

# TOMAWAC

Software for sea state modelling  
on unstructured grids over  
oceans and coastal seas

Release 6.0

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## 1. TOMAWAC– an overview

### 1.1. Introduction - Generals

TOMAWAC is a scientific software which models the changes, both in the time and in the spatial domain, of the power spectrum of wind-driven waves and wave agitation for applications in the oceanic domain, in the intracontinental seas as well as in the coastal zone. The model uses the finite elements formalism for discretizing the sea domain; it is based on the computational subroutines of the TELEMAC system as developed by the EDF R&D's Laboratoire National d'Hydraulique et Environnement (LNHE).

The acronym TOMAWAC being adopted for naming the software was derived from the following English denomination:

#### ***TELEMAC-based Operational Model Addressing Wave Action Computation***

(in French: *Modèle opérationnel basé sur le système TELEMAC concernant le calcul de l'action d'onde pour les vagues*)

TOMAWAC is one of the models making up the TELEMAC system [Hervouet, 2007], which addresses the various issues that are related to both free surface (either river- or sea-typed) and underground flows, as well as the associated physical processes: bed-load transport, water quality, etc.

### 1.2. Implementing TOMAWAC

TOMAWAC models the sea states by solving the balance equation of the action density directional spectrum. To serve that purpose, the model should reproduce the evolution of the action density directional spectrum at each node of a spatial computational grid.

In TOMAWAC the wave directional spectrum is split into a finite number of propagation frequencies  $f_i$  and directions  $\theta_i$ . The balance equation of wave action density is solved for each component  $(f_i, \theta_i)$ . The model is said to be a third generation model (e.g. like the WAM model [WAMDI, 1988] [Komen et al., 1994]), since it does not require any parameterization on the spectral or directional distribution of power (or action density). Each component of the action density spectrum changes in time under the effects of the software-modelled processes.

### 1.3. TOMAWAC general purposes

TOMAWAC can be used for three types of applications:

1. **Wave climate forecasting** a few days ahead, from wind field forecasts. This real time type of application is rather directed to weather-forecasting institutes such as Météo-France, whose one mission consists of predicting continuously the weather developments and, as the case may be, publishing storm warnings.
2. **Hindcasting** of exceptional events having severely damaged maritime structures and for which field records are either incomplete or unavailable.
3. **Study of wave climatology and maritime or coastal site features**, through the application of various, medium or extreme, weather conditions in order to obtain the conditions necessary to carry out projects and studies (harbour constructions, morphodynamic coastal evolutions, ...).

During the development of the TOMAWAC model, the LNHE laboratory has been interested mainly on the last two types of applications. It considered also the possibility to carry out research activities focused on the following topics:

- wave-currents and wave-overelevations interactions, especially in those places where tide plays a significant role,
- coastal morphodynamics,
- probability of floods in coastal zone,
- coastal structure stability and coast protection,
- assimilation of wind or wave satellite data during computation...

## 2. Representing waves in TOMAWAC

### 2.1. General definition of waves

As stated in paragraph 1.1, the purpose of the TOMAWAC software consists of modelling the generation and the spatio-temporal evolution of waves at the surface of the seas or of the oceans. Then, the main physical process of interest is **the wave** or **the sea states**, these two terms being used interchangeably in this document.

The word waves, generally means all the wind driven free surface waves propagating at the surface of the ocean and the period of which (denoted as  $T$ ) typically ranges from 2.5 to 25 s, or even, equivalently, whose frequency  $f=1/T$  ranges from 0.04 to 0.4 Hz.

The sea state may take various forms, depending on whether the sea is still and quiet or, on the contrary, in a stormy phase, whether the waves are being formed (the so-called wind sea) or, on the contrary, are coming from the ocean after travelling several hundreds or thousand kilometres (the so-called “swell”).

### 2.2. Plane monochromatic waves

The most commonly used way to introduce wave modelling consists of considering simple sinusoidal waves (they are often called regular waves). It is a monochromatic (one period or frequency) and plane (one propagation direction) wave. The free surface elevation, which is denoted as  $\eta$ , depends on the position  $(x, y)$  of the point being considered in space, as well as on time  $t$ . It is written as:

$$\eta(x, y, t) = a \cos [k(x \sin \theta + y \cos \theta) - \omega t + \varphi] \quad (2.1)$$

wherein:

- $a$  is the wave amplitude (in meters) and corresponds to the distance from the wave crest and the mean level at rest. The wave height, being measured from the crest to the trough of the wave, is used as well:  $H=2a$ .
- $\omega$  is the wave frequency (in rad/s). The period (in seconds)  $T = 2\pi/\omega$  or the frequency  $f$  (in hertz)  $= 1/T = \omega/(2\pi)$  is used as well.
- $k$  is the wave number (in rad/m). The wavelength (in meters):  $L = 2\pi/k$  is used as well. The wave number  $k$  is given by the free surface wave linear dispersion relation, according to frequency  $\omega$  and depth  $d$ :

$$\omega^2 = g.k.\tanh(k.d) \quad (2.2)$$

- $\theta$  is the wave propagation direction (in radians). Conventionally, this direction is measured herein clockwise with respect to  $Y$  axis.

- $\varphi$  is the wave phase (in radians).

The energy per unit area of these progressive waves (which consists of kinetic energy and potential energy in halves) amounts to:

$$E = 1/2 \rho g a^2 = 1/8 \rho g H^2 \quad (2.3)$$

wherein:

- $g$  is the gravity acceleration ( $g \approx 9.81 \text{ m/s}^2$ )
- $\rho$  is the water density (in  $\text{kg/m}^3$ ) ( $\rho \approx 1025 \text{ kg/m}^3$  for seawater).

### 2.3. Random multidirectional waves

A first representation of waves at the surface of the ocean is possible through the sinusoidal expression being used in the preceding paragraph. When watching an actual sea state, however, not all the waves have the same features, whether it is in terms of height, period or propagation direction. As a matter of fact, the free surface wave energy is distributed over a range of frequencies (waves are then said to be irregular or random) and over a range of propagation directions (waves are then called multidirectional). Mathematically, that irregularity is expressed by writing that a real sea state results from the superposition of an infinite (or large) number of elementary sinusoidal components (i.e. monochromatic and uni-directional components).

Thus, a random multidirectional wave field can be modelled through a superposition method, considering  $M$  plane monochromatic components:

$$\eta(x, y, t) = \sum_{m=1}^M \eta_m(x, y, t) = \sum_{m=1}^M a_m \cos [k_m(x \sin \theta_m + y \cos \theta_m) - \omega_m t + \varphi_m] \quad (2.4)$$

A major point in the above expression concerns the phase distribution  $\varphi_m$  of elementary wave components. The approach used in the TOMAWAC model assumes that these phases are randomly distributed over the  $[0; 2\pi]$  range with a uniform probability density. The various wave components are then independent, i.e. a linear or phase averaged representation is used.

With the linear representation featuring TOMAWAC and using the random phase hypothesis, the energy per unit area of random multidirectional waves can then be expressed as:

$$E = \sum_{m=1}^M \frac{1}{2} \rho g a_m^2 \quad (2.5)$$

It is noteworthy, however, that the distortions of shallow water wave profiles cannot be modelled with such a representation. This is because, as the water depth decreases, the non-linear processes linked to wave propagation and wave interactions with the sea bottom get some importance. The waves become steeper and dissymmetrical: they depart from a sinusoidal profile. A fine modelling of these non-linear effects involves non-linear wave theories (3rd- or 5th-order Stokes waves, cnoidal waves, ...) and/or so-called "phase resolving" propagation models modelling the evolution of each wave from a train, with a spatial discretization of 20-50 points per wavelength (Boussinesq, Serre equations, ...).

TOMAWAC is a phase averaged model: it is therefore *a priori* hardly suitable for modelling these non-linear effects when the wave profile can no longer be considered as the superposition of a number of independent sinusoidal components. In Section 4, however, it will be explained how the non-linear effects can be processed and represented through source terms.

### 2.4. Sea state directional power spectrum

Real waves were introduced in the previous chapter as a discrete sum of elementary components. Actually, the power spectrum over both frequencies and propagation directions is a continuous function. The relevant variable for describing that sea state power spectrum is the **directional spectrum of wave energy** which is also known as wave **directional spectrum of energy** and will henceforth be denoted as  $E(f, \theta)$ .

It is a function (in  $\text{Joule} \cdot \text{Hz}^{-1} \cdot \text{rad}^{-1}$ ) that depends on:



- wave frequency  $f$  (in Hertz), conventionally only positive (ranging from 0 to  $+\infty$ )
- propagation direction  $\theta$ , ranging within a  $2\pi$  length interval.

Correspondence with the discrete case of the previous section is set considering the following equivalence:

$$\sum_f^{f+df} \sum_\theta^{\theta+d\theta} \frac{1}{2} \rho g a_m^2 = E(f, \theta) df d\theta \quad (2.6)$$

In case of a wave propagation in a zero-current medium, a balance equation of the wave energy directional spectrum can be written taking into account some source and sink terms for energy generation or energy dissipation.

### 2.5. Directional spectrum of sea state variance

The preferred variable for sea state representation and modelling is rather the **variance density directional spectrum**.

This function, noted as  $F(f, \theta)$  and expressed in  $\text{m}^2 \text{Hz}^{-1} \text{rad}^{-1}$  is simply derived from the directional spectrum of wave energy by the relation:

$$F(f, \theta) = E(f, \theta) / (\rho g) \quad (2.7)$$

Then, in particular, we have: 
$$\sum_f^{f+df} \sum_\theta^{\theta+d\theta} \frac{1}{2} \rho g a_m^2 = E(f, \theta) df d\theta \quad (2.8)$$

The relation linking the variance density directional spectrum and the free surface elevation is then written in the following pseudo-integral form:

$$\eta(x, y, t) = \int_{f=0}^{\infty} \int_{\theta=0}^{2\pi} \sqrt{2F(f, \theta)} df d\theta \cos[k(x \cos \theta + y \sin \theta) - \omega t + \varphi] \quad (2.9)$$

It should be reminded that the phases are randomly distributed in that expression over the range  $[0; 2\pi]$  with a uniform probability density. As regards the amplitude of each elementary component, it is related to the variance density directional spectrum by:

$$a_m = \sqrt{2F(f, \theta) df d\theta} \quad (2.10)$$

The  $n$ -order ( $n = 0, 1, 2, \dots$ ) moments  $m_n$  of the variance density directional spectrum are defined as:

$$m_n = \int_{f=0}^{\infty} \int_{\theta=0}^{2\pi} f^n F(f, \theta) df d\theta \quad (2.11)$$

Among these moments, the 0-order moment is equal to the variance of the free surface elevation:

$$\langle \eta^2 \rangle = \lim_{t_o \rightarrow \infty} \frac{1}{t_o} \int_0^{t_o} \eta^2(t) dt = m_0 = \int_{f=0}^{\infty} \int_{\theta=0}^{2\pi} F(f, \theta) df d\theta \quad (2.12)$$

In particular, that moment  $m_0$  affects the determination of the significant spectral wave height  $H_{m0}$  (equal to the significant height  $H_{1/3}$  assuming that the wave heights are distributed according to a Rayleigh's law) by the relation:

$$H_{m0} = 4\sqrt{m_0} \quad (2.13)$$

The average frequencies  $f_{01}$  and  $f_{02}$  and  $f_{10}=f_e$  are also used and computed as follows:

$$f_{01} = \frac{m_1}{m_0} \quad f_{02} = \sqrt{\frac{m_2}{m_0}} \quad f_e = \frac{m_0}{m_{-1}} \quad (2.14)$$

Further derived parameters can be computed from the variance density directional spectrum (see e.g. in [AIRH, 1986]).

## 2.6. Sea state directional spectrum of wave action

In the general case of wave propagation in an unsteady medium (sea currents and/or levels varying in time and space), the directional spectrum of the variance density is no longer kept and a new quantity should be introduced, namely the **directional spectrum of wave action**.

That quantity, noted as  $N(f, \theta)$ , will remain constant (without considering the source and sink terms) even though the propagation medium is neither homogeneous nor steady [Komen et al., 1994] [Willebrand, 1975] [Phillips, 1977] [Bretherton, 1969].

The action density spectrum is related to the directional spectrum of variance density by the relation:

$$N = F/\sigma \quad (2.15)$$

wherein  $\sigma$  denotes the relative or intrinsic angular frequency, i.e. the angular frequency being observed in a coordinate system moving at the velocity of current. Such a frequency is different from the absolute angular frequency  $\omega$  observed in a fixed system of coordinates. The two frequencies are linked by the Doppler effect relation in the presence of a current  $\vec{U}$  :

$$\Omega(\vec{k}, \vec{x}, t) = \omega = \sigma + \vec{k} \cdot \vec{U} \quad (2.16)$$

## 2.7. Selecting the directional spectrum discretization variables

The directional spectra of wave energy, variance or action shall generally be considered as functions depending on five variables:

- time  $t$ ;
- the pair of coordinates proving the spatial position of the point being considered. In TOMAWAC, these coordinates can be expressed either in a Cartesian coordinate system (x, y) or in a spherical coordinate system (latitude, longitude) according to the dimension of the computational domain;
- the pair of variables applied for directional spectrum discretization, for which several solutions are theoretically possible:
  - $(f_a, \theta)$  = (absolute frequency; propagation direction)
  - $(f_r, \theta)$  = (relative frequency; propagation direction)
  - $(k, \theta)$  = (wave number; propagation direction)
  - $(k_x, k_y) = (k \cdot \sin \theta; k \cdot \cos \theta)$  = (wave number vector)

For the numerical resolution of equations, the model TOMAWAC uses the pair  $(f_r, \theta)$  = (relative frequency; propagation direction).

The directional spectra output by TOMAWAC, however, are always expressed in  $(f_a, \theta)$ . The equations solved by TOMAWAC are thoroughly reviewed in section 4.

### 3. Hypotheses and application domain of TOMAWAC

#### 3.1. Application domain of the model TOMAWAC

TOMAWAC is designed to be applied from the ocean domain up to the coastal zone. The limits of the application range can be determined by the value of the relative depth  $d/L$ , wherein  $d$  denotes the water height (in metres) and  $L$  denotes the wave length (in metres) corresponding to the peak spectral frequency for irregular waves.

The application domain of TOMAWAC includes:

- **the oceanic domain**, characterized by large water depths, i.e. by relative water depths of over 0.5. The dominant physical processes are: wind-driven wave generation, whitecapping dissipation and non-linear quadruplet interactions;
- **the continental seas and the medium depths**, characterized by a relative water depth ranging from 0.05 to 0.5. In addition to the above processes, the bottom friction, the shoaling (wave growth due to a bottom rise) and the effects of refraction due to the bathymetry and/or to the currents are to be taken into account;
- **The coastal domain**, including shoals or near-shore areas (relative water depth lower than 0.05). For these shallow water areas, such physical processes as bottom friction, bathymetric breaking, non-linear triad interactions between waves should be included. Furthermore, it could be useful to take into account the effects related to unsteady sea level and currents due to the tide and/or to the weather-dependent surges.

Through a so-called finite element spatial discretization, one computational grid may include mesh cells among which the ratio of the largest sizes to the smallest ones may reach or even exceed 100. That is why TOMAWAC can be applied to a sea domain that is featured by highly variable relative water depths; in particular, the coastal areas can be finely represented.

The application domain of TOMAWAC does not include the harbour areas and, more generally, all those cases in which the effects of reflection on structures and/or diffraction may not be ignored.

#### 3.2. Wave interactions with other physical factors

Several factors are involved in the wave physics and interact to various extents with the waves changing their characteristics. The following main factors should be mentioned:

- bathymetry and sea bottom geometry (bottom friction, refraction, surf-breaking, non-linear effects of interactions with the bottom, sand rippling...);
- atmospheric circulation (wind and pressure effects);
- tide pattern (variation of currents and water heights);
- three-dimensional oceanic circulation currents;
- over/under elevations caused by exceptional weather events, resulting in sea levels variations up to several meters (storm, surges).

The fine modelling of the interactions between these various physical factors and the waves is generally rather complex and several research projects are currently focused on it. Within the application domain as defined in the previous paragraph, TOMAWAC models the following interactions:

- **wave-bathymetry interaction:** the submarine relief data input into TOMAWAC are constant in time, but the sea level can change in time. In addition to the effects of the

sea level variations in time, TOMAWAC allows to take into account refraction, shoaling, bottom friction and bathymetric breaking;

- **wave-atmosphere interaction:** this interaction is the driving phenomenon in the wave generation, takes part in energy dissipation processes (whitecapping, wave propagation against the wind...) and is involved in the energy transfer. To represent the unsteady behaviour of this interaction, TOMAWAC requires 10 m wind fields (specification of the couple of horizontal velocity components) with a time step matched to the weather conditions being modelled. These wind fields can be provided either by a meteorological model or from satellite measurements;
- **wave-current interaction:** the sea currents (as generated either by the tide or by oceanic circulations) may significantly affect the waves according to their intensity. They modify the refractive wave propagation direction, they reduce or increase the wave height according to their propagation direction in relation to the waves and may influence the wave periods if exhibiting a marked unsteady behaviour. In TOMAWAC, the current field is provided by the couple of horizontal components of its average (or depth-integrated) velocity at the nodes of the computational grid. TOMAWAC allows to model the frequency changes caused either by the Doppler effect or by the unsteady currents, as well as by a non-homogeneous current field.

### 3.3. The physical processes modelled in TOMAWAC

Those interactions being taken into account by TOMAWAC have been reviewed and a number of physical events or processes have been mentioned in the previous paragraph. These processes modify the total wave energy as well as the directional spectrum distribution of that energy (i.e. the shape of the directional spectrum of energy). So far, the numerical modelling of these various processes, although some of them are now very well known, is not yet mature and keep on providing many investigation subjects. Considering the brief review of physical interactions given in the previous paragraph, the following physical processes are taken into account and digitally modelled in TOMAWAC:

#### —> *Energy source/dissipation processes:*

- wind-driven interactions with atmosphere. Those interactions imply the modelling of the wind energy input into the waves. It is the prevailing source term for the wave energy directional spectrum. The way that spectrum evolves primarily depends on wind velocity, direction, time of action and fetch (distance over which the wind is active). It must be pointed out that the energy that is dissipated when the wind blocks the waves is not taken into account in TOMAWAC;
- whitecapping dissipation or wave breaking, due to an excessive wave steepness during wave generation and propagation;
- bottom friction-induced dissipation, mainly occurring in shallow water (bottom grain size distribution, ripples, percolation...);
- dissipation through bathymetric breaking. As the waves come near the coast, they swell due to shoaling until they break when they become too steep;
- dissipation through wave blocking due to strong opposing currents.

#### —> *Non-linear energy transfer conservative processes:*

- non-linear resonant quadruplet interactions, which is the exchange process prevailing at great depths;

- non-linear triad interactions, which become the prevailing process at small depths.

—> **Wave propagation-related processes:**

- wave propagation due to the wave group velocity and, in case, to the velocity of the medium in which it propagates (sea currents);
- depth-induced refraction which, at small depths, modifies the directions of the wave-ray and then implies an energy transfer over the propagation directions;
- shoaling: wave height variation process as the water depth decreases, due to the reduced wavelength and variation of energy propagation velocity;
- current-induced refraction which also causes a deviation of the wave-ray and an energy transfer over the propagation directions;
- interactions with unsteady currents, inducing frequency transfers (e.g. as regards tidal seas).

These various processes are numerically modelled as presented in chapter 4.

It should be remembered that, due to the hypothesis adopted in paragraph 3.1 about the TOMAWAC application domain, the following physical processes are not addressed by the model (non-exhaustive list):

- diffraction by a coastal structure (breakwater, pier, etc...) or a shoal, resulting in an energy transfer towards the shadow areas beyond the obstacles blocking the wave propagation.
- reflection (partial or total) from a structure or a pronounced depth irregularity.

## 4. Mathematical modelling procedures used by TOMAWAC

### 4.1. Scope of sea state modelling

The directional spectrum of wave action density, as defined in paragraph 2.6, is considered as a function of five variables:

$$N(\vec{x}, \vec{k}, t) = N(x, y, k_x, k_y, t)$$

using, as discretization variables:

- the position vector  $\vec{x} = (x, y)$  for spatial location in a Cartesian coordinate system;
- the wave number vector  $\vec{k} = (k_x, k_y) = (k \cdot \sin \theta, k \cdot \cos \theta)$  for directional spectrum discretization,  $\theta$  denoting the wave propagation direction (direction in which the waves travel);
- the time  $t$ .

Under the hypotheses made on the wave representation (see in paragraph 2.6) as well as on the model application domain and the modelled physical processes (see in paragraph 3.3), an equation of evolution of the directional spectrum of wave action can be written in the following form (see in [Willebrand, 1975] [Phillips, 1977] [Bretherton, 1969] for a detailed demonstration of the way that equation is arranged):

$$\frac{\partial N}{\partial t} + \frac{\partial(\dot{x}N)}{\partial x} + \frac{\partial(\dot{y}N)}{\partial y} + \frac{\partial(\dot{k}_x N)}{\partial k_x} + \frac{\partial(\dot{k}_y N)}{\partial k_y} = Q(k_x, k_y, x, y, t) \quad (4.1)$$

The equation expresses that, in the general case of waves propagating in a non-homogeneous, unsteady environment (currents and/or sea levels varying in time and space), the wave action is preserved to within the source and sink terms (designated by the term  $Q$ ).

The following notation is also used in (4.1):

$$\dot{g} = \frac{dg}{dt} = \frac{\partial g}{\partial t} + \frac{\partial x}{\partial t} \frac{\partial g}{\partial x} + \frac{\partial y}{\partial t} \frac{\partial g}{\partial y}$$

In that form (conservative writing in the form of a flux), equation (4.1) can be transposed to other coordinate systems and, for instance,  $(k, \theta)$ ,  $(f_a, \theta)$  or else  $(f_r, \theta)$  can be used for the discretization of directional spectrum [Komen et al., 1994] [Tolman, 1991].

Working in  $(x, y, k_x, k_y)$ , however, makes it possible to remain in the canonical coordinate system and to write, for the propagation equations (also named Hamilton's equations):

$$\dot{x} = \frac{\partial \Omega}{\partial k_x} \quad \text{and} \quad \dot{y} = \frac{\partial \Omega}{\partial k_y} \quad (4.2.a)$$

$$\dot{k}_x = -\frac{\partial \Omega}{\partial x} \quad \text{and} \quad \dot{k}_y = -\frac{\partial \Omega}{\partial y} \quad (4.2.b)$$

wherein  $\Omega$  results from the Doppler relation applied to the wave dispersion relation for the general case with current:

$$\Omega(\vec{k}, \vec{x}, t) = \omega = \sigma + \vec{k} \cdot \vec{U} \quad (4.3)$$

wherein:  $\omega$  is the absolute angular frequency observed in a fixed coordinate system.

$f_a = \omega/(2\pi)$  is named absolute frequency.

$\vec{U}$  denotes the current velocity (depth-integrated).

$\sigma$  denotes the intrinsic or relative angular frequency, which is observed in a coordinate system moving at the velocity  $\vec{U}$ . It is given by the dispersion relation in the zero-current case:

$$\sigma^2 = g.k.\tanh(k.d) \quad (4.4)$$

$f_r = \sigma/(2\pi)$  is named intrinsic or relative wave frequency;

$d$  denotes the water height.

Through the Hamilton's equations (4.2.a and 4.2.b), it can be demonstrated that we have:

$$\frac{\partial \dot{x}}{\partial x} + \frac{\partial \dot{y}}{\partial y} + \frac{\partial \dot{k}_x}{\partial k_x} + \frac{\partial \dot{k}_y}{\partial k_y} = 0 \quad (4.5.a)$$

$$\text{or } \text{div}(\vec{V}) = 0 \text{ when defining: } \vec{V} = (\dot{x}, \dot{y}, \dot{k}_x, \dot{k}_y) \quad (4.5.b)$$

The evolution equation (4.1) can then alternatively be written in the following form (the so-called transport form):

$$\frac{\partial N}{\partial t} + \dot{x} \frac{\partial N}{\partial x} + \dot{y} \frac{\partial N}{\partial y} + \dot{k}_x \frac{\partial N}{\partial k_x} + \dot{k}_y \frac{\partial N}{\partial k_y} = Q(k_x, k_y, x, y, t) \quad (4.6.a)$$

$$\frac{\partial N}{\partial t} + \vec{V} \cdot \text{grad}_{\vec{x}, \vec{k}}(N) = Q \quad (4.6.b)$$

The transfer rates are given by the linear wave theory [Chaloin, 1989] [Komen et al., 1994] [Mei, 1983] [Tolman, 1991]:

$$\dot{x} = C_g \frac{k_x}{k} + U_x \quad (4.7.a)$$

$$\dot{y} = C_g \frac{k_y}{k} + U_y \quad (4.7.b)$$

$$\dot{k}_x = -\frac{\partial \sigma}{\partial d} \frac{\partial d}{\partial x} - \vec{k} \cdot \frac{\partial \vec{U}}{\partial x} \quad (4.7.c)$$

$$\dot{k}_y = -\frac{\partial \sigma}{\partial d} \frac{\partial d}{\partial y} - \vec{k} \cdot \frac{\partial \vec{U}}{\partial y} \quad (4.7.d)$$

$C_g$  is the relative (or intrinsic) group velocity of waves, i.e. as is observed in a coordinate system moving at the velocity of the current:

$$C_g = \frac{\partial \sigma}{\partial k} = n \frac{\sigma}{k} \text{ with } n = \frac{1}{2} \left( 1 + \frac{2kd}{\sinh(2kd)} \right) \quad (4.8)$$

The relative (or intrinsic) phase velocity  $C$  of waves is also introduced:  $C = \frac{\sigma}{k}$

The sea state spectral modelling will then consist of solving the evolution equations (4.1) or (4.6.a), using the kinematic equations (4.7.a – 4.7.d).

The transport equation formulation (4.6.a) or (4.6.b) has been adopted in TOMAWAC, since it is closely related to other equations applied in hydraulics, which have already been treated at the LNHE and for which methods and a know-how have been developed long ago.

As regards the discretization variables being used in TOMAWAC, we have already mentioned in paragraph 2.7 that:

- spatial discretization can be based either on a Cartesian coordinate system in  $(x, y)$  or on a spherical coordinate system at the Earth's surface in  $(\lambda, \varphi) = (\text{longitude}, \text{latitude})$ .
- Discretization of angular spectrum uses the pair  $(f_r, \theta) = (\text{relative frequency} ; \text{propagation direction})$ .

The following conventions are adopted for writing the equations:

- the x-axis (in the Cartesian coordinate system) or the  $\lambda$ -axis of longitudes (in the spherical coordinate system) is assumed to be horizontal, directed to the right, whereas the y-axis (in the Cartesian coordinate system) or the  $\varphi$ -axis of latitudes (in the spherical coordinate system) is assumed to be vertical, upwardly directed. Then, in spherical coordinates, the vertical axis points at the north, whereas the horizontal axis points to the East.
- In either case, the wave propagation directions  $\theta$  are defined with respect to the vertical axis in the clockwise direction.

These conventions are illustrated below in Figure 4.1. Those equations that correspond to the two spatial discretizations options are developed in the next paragraphs.

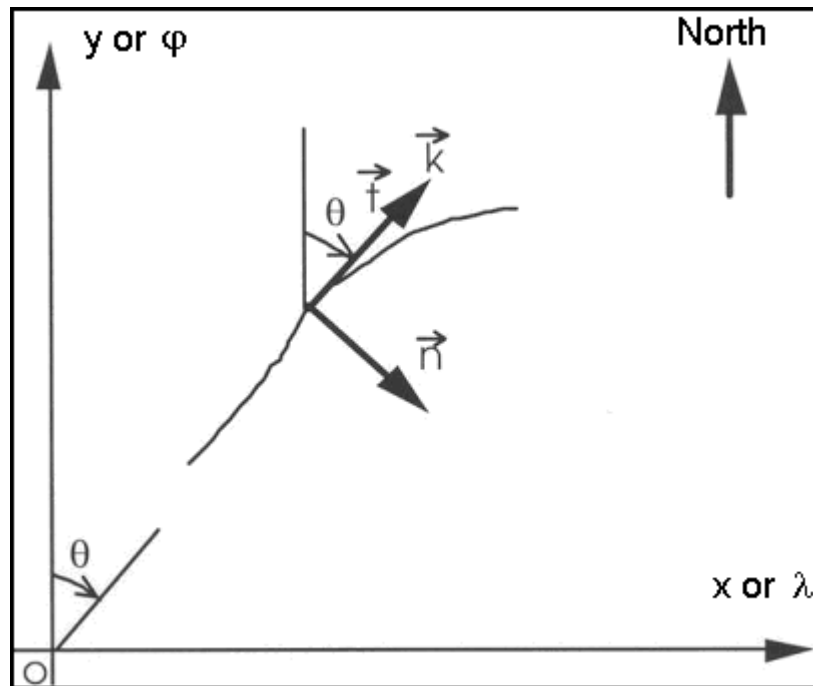


Figure 4.1: definition of location conventions as used in TOMAWAC



## 4.2. Equations solved

### 4.2.1. Equations solved in a Cartesian spatial coordinate system

By switching the variable from  $(x, y, k_x, k_y)$  to  $(x, y, f_r, \theta)$ , it can be shown that the following relation exists for the directional spectrum of wave action as expressed in both coordinate systems:

$$N(x, y, k_x, k_y, t) = \frac{CCg}{2\pi\sigma} \tilde{N}(x, y, f_r, \theta, t) = \tilde{B} \cdot \tilde{F}(x, y, f_r, \theta, t) \quad (4.9)$$

$$\text{putting: } \tilde{B} = \frac{C Cg}{2\pi\sigma^2} = \frac{Cg}{(2\pi)^2 k f_r} \quad (4.10)$$

The evolution equation (4.6.b) is then written as:

$$\frac{\partial(\tilde{B}\tilde{F})}{\partial t} + \dot{x} \frac{\partial(\tilde{B}\tilde{F})}{\partial x} + \dot{y} \frac{\partial(\tilde{B}\tilde{F})}{\partial y} + \dot{\theta} \frac{\partial(\tilde{B}\tilde{F})}{\partial \theta} + \dot{f}_r \frac{\partial(\tilde{B}\tilde{F})}{\partial f_r} = \tilde{B} \cdot \tilde{Q}(x, y, \theta, f_r, t) \quad (4.11)$$

with the following transfer rates, as computed from the linear wave theory:

$$\dot{x} = Cg \cdot \sin \theta + U_x \quad (4.12.a)$$

$$\dot{y} = Cg \cdot \cos \theta + U_y \quad (4.12.b)$$

$$\dot{\theta} = -\frac{1}{k} \frac{\partial \sigma}{\partial d} \tilde{G}_n(d) - \frac{\vec{k}}{k} \cdot \tilde{G}_n(\vec{U}) \quad (4.12.c)$$

$$\dot{f}_r = \frac{1}{2\pi} \left[ \frac{\partial \sigma}{\partial d} \left( \frac{\partial d}{\partial t} + \vec{U} \cdot \vec{\nabla} d \right) - Cg \vec{k} \cdot \tilde{G}_t(\vec{U}) \right] \quad (4.12.d)$$

The operators  $\tilde{G}_n$  and  $\tilde{G}_t$  refer to the computation of a function gradient in directions that are respectively normal and tangential to the characteristic curve with the direction  $\theta$ .

$$\tilde{G}_n(g) = \vec{n} \cdot \vec{\nabla} g = \cos \theta \frac{\partial g}{\partial x} - \sin \theta \frac{\partial g}{\partial y} \quad (4.13.a)$$

$$\tilde{G}_t(g) = \vec{t} \cdot \vec{\nabla} g = \sin \theta \frac{\partial g}{\partial x} + \cos \theta \frac{\partial g}{\partial y} \quad (4.13.b)$$

Besides, using the dispersion relation (4.4), it can be demonstrated that:

$$\frac{\partial \sigma}{\partial d} = \frac{\sigma k}{\sinh(2kd)} \quad (4.14)$$

The spatial transfer rates  $\dot{x}$  and  $\dot{y}$  (equations 4.12.a and 4.12.b) model the spatial wave propagation and the shoaling. The directional transfer rate  $\dot{\theta}$  (equation 4.12.c) models the refraction-induced change of wave propagation direction. Refraction is generated by the spatial variations of those properties of the environment in which the waves propagate and can result either from a bathymetric variation (first term in 4.12.c) or from current gradients (second term in 4.12.c). The relative frequency transfer rate  $\dot{f}_r$  (equation 4.12.d) models the relative frequency changes resulting from sea level variations both in space and time and/or from current variations in space.

It is noteworthy that this last term is zero in the case of zero-current and of no variation of sea level in time: the advection equation is then reduced to a three-dimensional equation.

Lastly, as regards the source terms, it should be mentioned that changing the coordinate system and using the factor  $\tilde{B}$  allows to switch from the term  $Q$  to a term  $\tilde{Q}$  that is directly expressed in terms of the directional variance spectrum with a variance  $\tilde{F}(f_r, \theta)$ . The content of that term is explained in paragraph 4.2.3.

#### 4.2.2. Equations solved in a spherical spatial coordinate system

By switching the variables from  $(x, y, k_x, k_y)$  to  $(\lambda, \varphi, f_r, \theta)$ , it can be shown that the following relation exists for the directional spectrum of wave action as expressed in both coordinate systems:

$$N(x, y, k_x, k_y, t) = \frac{CCg}{2\pi\sigma R^2 \cos\varphi} \hat{N}(\lambda, \varphi, f_r, \theta, t) = \hat{B} \cdot \hat{F}(\lambda, \varphi, f_r, \theta, t) \quad (4.15)$$

$$\text{putting: } \hat{B} = \frac{C Cg}{2\pi\sigma^2 R^2 \cos\varphi} = \frac{Cg}{(2\pi)^2 k f_r R^2 \cos\varphi} \quad (4.16)$$

$R$  denotes the Earth's radius ( $R \approx 6400$  km) and, once more,  $\lambda$  and  $\varphi$  are respectively the longitude and the latitude of the point being considered.

The evolution equation (4.6.b) is then written as:

$$\frac{\partial(\hat{B}\hat{F})}{\partial t} + \dot{\lambda} \frac{\partial(\hat{B}\hat{F})}{\partial \lambda} + \dot{\varphi} \frac{\partial(\hat{B}\hat{F})}{\partial \varphi} + \dot{\theta} \frac{\partial(\hat{B}\hat{F})}{\partial \theta} + \dot{f}_r \frac{\partial(\hat{B}\hat{F})}{\partial f_r} = \hat{B} \cdot \hat{Q}(\lambda, \varphi, \theta, f_r, t) \quad (4.17)$$

with the following transfer rates:

$$\dot{\lambda} = \frac{1}{R \cos\varphi} (Cg \cdot \sin\theta + U_\lambda) \quad (4.18.a)$$

$$\dot{\varphi} = \frac{1}{R} (Cg \cdot \cos\theta + U_\varphi) \quad (4.18.b)$$

$$\dot{\theta} = \frac{1}{R} \left[ Cg \sin\theta \tan\varphi - \frac{1}{k} \frac{\partial\sigma}{\partial d} \hat{G}_n(d) - \frac{\vec{k}}{k} \cdot \hat{G}_t(\vec{U}) \right] \quad (4.18.c)$$

$$\dot{f}_r = \frac{1}{2\pi R} \left[ \frac{\partial\sigma}{\partial d} \left( \frac{\partial d}{\partial t} + \frac{U_\lambda}{\cos\varphi} \frac{\partial d}{\partial \lambda} + U_\varphi \frac{\partial d}{\partial \varphi} \right) - Cg \cdot \vec{k} \cdot \hat{G}_t(\vec{U}) \right] \quad (4.18.d)$$

As in the previous case, the operators  $\hat{G}_n$  and  $\hat{G}_t$  refer to the computation of a function gradient in directions that are respectively normal and tangential to the characteristic curve with the direction  $\theta$ .

$$\hat{G}_n(g) = \frac{\cos\theta}{\cos\varphi} \frac{\partial g}{\partial \lambda} - \sin\theta \frac{\partial g}{\partial \varphi} \quad (4.19.a)$$

$$\hat{G}_t(g) = \frac{\sin\theta}{\cos\varphi} \frac{\partial g}{\partial \lambda} + \cos\theta \frac{\partial g}{\partial \varphi} \quad (4.19.b)$$

As previously, the spatial transfer rates  $\dot{\lambda}$  and  $\dot{\varphi}$  (equations 4.18.a and 4.18.b) model the wave propagation in space and the shoaling. In that coordinate system, the directional transfer rate  $\dot{\theta}$  has

an additional term (the first term in equation (4.18.c)) compared to the case in Cartesian coordinates. That term results from the propagation in spherical coordinates, in such a way that waves are located with respect to the North change during the propagation over a large circle arc at the Earth's surface [WAMDI, 1988] [Komen et al., 1994]. Both second and third terms  $\dot{\theta}$  (equation 4.18.c) model the refraction caused respectively by bathymetry and currents. The relative frequency transfer rate  $\dot{f}_r$  (equation 4.18.d) models the changes of relative frequency resulting from variations of the sea level or of the current in both space and time. It is noteworthy that this last term is zero in the case of zero current and of no variation of the sea level in time: the advection equation is then reduced to a three-dimensional equation.

### 4.2.3. TOMAWAC source and sink terms

#### 4.2.3.1. Generals

The source and sink terms that compose  $\tilde{Q}$  and  $\hat{Q}$  in the right-hand members of evolution equations (4.11) and (4.17) of directional spectrum of wave action gather the contributions from the physical processes listed in paragraph 3.3. for the application domain of TOMAWAC:

$$Q = Q_{in} + Q_{ds} + Q_{nl} + Q_{bf} + Q_{br} + Q_{tr}$$

wherein  $Q_{in}$ : wind-driven wave generation

$Q_{ds}$ : whitecapping-induced energy dissipation

$Q_{nl}$ : non-linear quadruplet interactions

$Q_{bf}$ : bottom friction-induced energy dissipation

$Q_{br}$ : bathymetric breaking-induced energy dissipation

$Q_{tr}$ : non-linear triad interactions

These source and sink terms are numerically modelled and parameterized as detailed in the next paragraphs. For most of these processes, several models or formulations are proposed and available in TOMAWAC.

#### 4.2.3.2. Wind input (term $Q_{in}$ )

Two models are available in TOMAWAC. The model to be activated is selected through the keyword *WIND GENERATION* in the steering file, which can take three values, namely:

- 0 no wind drift (*default value*)
- 1 Janssen's model [Janssen, 1989] [Janssen, 1991] (WAM cycle 4) (see in paragraph 4.2.3.2.1).
- 2 Snyder et al. model [Snyder et al., 1981] (see in paragraph 4.2.3.2.2).

##### 4.2.3.2.1. Option 1 for wind drift: Janssen's model

With that option, the model implemented for the wind drift term is based upon the Janssen's works [Janssen, 1989] [Janssen, 1991]; Janssen proposed a quasi-linear theory for modelling the ocean/atmosphere interactions. The linear growth term is ignored and only an exponential energy growth is taken into account, following Miles' results [Miles, 1957].

A quasi-linear source term is obtained as a function of the directional variance spectrum:

$$Q_{in} = \sigma \cdot \varepsilon \cdot \beta \cdot \left( \left[ \frac{u_*}{C} + z_\alpha \right] \max[\cos(\theta - \theta_w); 0] \right)^2 F \quad (4.20)$$

with the following notations:

$\varepsilon = \rho_{air}/\rho_{water}$  is the ratio of air and water specific gravities ( $\varepsilon \approx 1.25 \cdot 10^{-3}$ ).

$C = \sigma/k$  is the wave phase velocity

$\theta_w$  is the local wind direction (direction in which it blows)

$u_*$  is the friction velocity, being linked to the surface stress  $\tau_s$  by the following relation:

$$u_* = \sqrt{\frac{\tau_s}{\rho_{air}}} \quad (4.21)$$

$z_\alpha$  is a constant allowing to offset the growth curve.

The operator 'max' in the source term expression limits the wave generation for the propagation directions included within a  $\pm 90^\circ$  angular sector with respect to the local wind direction  $\theta_w$ . For the wave directions making an angle in excess of  $90^\circ$  with respect to the wind direction  $\theta_w$ , the wind drift term is void.

In the Janssen's model [Janssen, 1991], the Miles' parameter  $\beta$  is a function of two non-dimensional variables:

- the wave age:

$$A = \frac{u_*}{C}$$

- the wind profile parameter:

$$\Omega = \frac{g \cdot z_0}{u_*^2}$$

$$\text{It is written as } \beta = \frac{\beta_m}{\kappa^2} \mu \ln^4 \mu \quad (4.22)$$

where  $\kappa$  is the Von Karman's constant

$\beta_m$  denotes a coefficient set to 1.2 by Janssen [Janssen, 1991].

$z_0$  denotes the roughness length

$\mu$  denotes the non-dimensional critical height:

$$\mu = \min \left[ \frac{g \cdot z_0}{C^2} \exp \left( \frac{\kappa}{\left[ \frac{u_*}{C} + z_\alpha \right] \cos(\theta - \theta_w)} \right); 1 \right] = \min \left[ \Omega \cdot A^2 \exp \left( \frac{\kappa}{[A + z_\alpha] \cos(\theta - \theta_w)} \right); 1 \right] \quad (4.23)$$

The Janssen's model [Janssen, 1989] [Janssen, 1991] is characterized by the method it uses for computing  $u_*$  and  $z_0$ . The surface stress  $\tau_s$  is a function depending, on the one hand, on the wind velocity  $U_{10}$  at 10 m and, on the other hand, on the sea state roughness through the wave stress  $\tau_w$ . It is obtained by solving the following system of equations:

$$U_{10} = \frac{u_*}{\kappa} \ln \left( \frac{10 + z_0 + \tilde{z}_0}{z_0} \right) \approx \frac{u_*}{\kappa} \ln \left( \frac{10}{z_0} \right) \quad (4.24.a)$$

$$z_0 = \frac{\tilde{z}_0}{\sqrt{1 - \tau_w / \tau_s}} \quad (4.24.b)$$

$$\tilde{z}_0 = \alpha \frac{u_*^2}{g} \quad (4.24.c)$$

$$u_* = \sqrt{\frac{\tau_s}{\rho_{air}}} \quad (4.24.c)$$

The solution of the system of equations through a Newton-Raphson's iterative method yields the surface stress  $\tau_s$ , the friction velocity  $u_*$  and the roughness length  $z_0$ .

The initial value of friction velocity  $u_*$  being used in the iterative algorithm is obtained considering a constant drag coefficient:

$$u_* = \sqrt{C_D} U_{10} \quad \text{where: } C_D = 1.2875 \cdot 10^{-3} \text{ by default.}$$

The wave stress  $\tau_w$  itself is computed from the variance spectrum  $F$  (via the source term  $Q_{in}$ ) using the following relation:

$$\tau_w = \left| \iint \rho_{water} \sigma Q_{in}(f_r, \theta) (\cos \theta, \sin \theta) df_r d\theta \right| \quad (4.25)$$

That integral is numerically computed over the discretized portion of the spectrum and a parameterization, based upon a decrement of variance in  $f^{-n}$ , is used for the high frequencies portion of the spectrum.

In fact, that source term has eight parameters, namely:

- coefficient  $\beta_m$  (corresponding to the keyword *WIND GENERATION COEFFICIENT* in the steering file). Its default value is taken as 1.2, in accordance with the Janssen's proposal [Janssen, 1991] and the value adopted in the model WAM-Cycle 4;
- air specific gravity  $\rho_{air}$  (corresponding to the keyword *AIR DENSITY* in the steering file). Its default value is taken as 1.225 kg/m<sup>3</sup>;
- water specific gravity  $\rho_{water}$  (corresponding to the keyword *WATER DENSITY* in the steering file). Its default value is taken as 1,000 kg/m<sup>3</sup>;
- constant  $\alpha$  (corresponding to the keyword *CHARNOCK CONSTANT* in the steering file). Its default value is taken as 0.01, in accordance with the Janssen's proposal [Janssen, 1991] and the standard value adopted in the model WAM-Cycle 4;
- constant  $\kappa$  (corresponding to the keyword *VON KARMAN CONSTANT* in the steering file). Its default value is taken as 0.41, i.e. the typical value;
- initial drag coefficient  $C_D$  (corresponding to the keyword *WIND DRAG COEFFICIENT* in the steering file). This drag coefficient is provided for initializing the iterative computation of friction velocity  $u_*$ . Its default value is taken as 1.2875  $\cdot 10^{-3}$ ;
- offset constant  $z_\alpha$  (corresponding to the keyword *SHIFT GROWING CURVE DUE TO WIND* in the steering file). Its default value is taken as 0.011, in accordance with the value adopted in the model WAM-Cycle 4;
- elevation at which the wind is recorded (corresponding to the keyword *WIND MEASUREMENTS LEVEL* in the steering file). Its default value is taken as 10 m: it corresponds to the typical value and to the value being adopted in the above explanations.

#### 4.2.3.2.2. Option 2 for wind drift: Snyder et al. model

In that option, the model implemented for the wind drift term is based upon the works conducted by Snyder *et al.* [Snyder et al., 1981], as amended by Komen et al. [Komen et al., 1984] to take into account the friction velocity  $u_*$  instead of the wind velocity at 5 m. It corresponds to the formulation being used in the cycle 3 release of WAM model. The formulation is simpler than the Janssen's theory, which Option 1 is based upon (see in preceding paragraph).

As in Option 1, the linear growth term is ignored and only an exponential energy growth is taken into account, following the Miles' results [Miles, 1957]:

$$Q_{in} = \beta F \quad \text{where: } \beta = \max \left[ 0 ; 0.25 \frac{\rho_{air}}{\rho_{water}} \left( 28 \frac{u_*}{C} \cos(\theta - \theta_w) - 1 \right) \right] \sigma \quad (4.26)$$

The shear velocity value  $u_*$  used is obtained considering a drag coefficient linearly depending on the wind velocity:

$$u_* = \sqrt{C_D} U_{10} \quad \text{where: } \begin{aligned} C_D &= 6.5 \cdot 10^{-5} U_{10} + 8 \cdot 10^{-4} & \text{if } U_{10} > 7.5 \text{ m/s.} \\ C_D &= 1.2875 \cdot 10^{-3} & \text{if } U_{10} < 7.5 \text{ m/s.} \end{aligned}$$

That source term only uses two parameters, namely:

- air density  $\rho_{air}$  (corresponding to the keyword *AIR DENSITY* in the steering file). Its default value is taken as 1.225 kg/m<sup>3</sup>.
- water density  $\rho_{water}$  (corresponding to the keyword *WATER DENSITY* in the steering file). Its default value is taken as 1,000 kg/m<sup>3</sup>.

#### 4.2.3.3. Whitecapping-induced dissipations (term $Q_{ds}$ )

A single model is available in TOMAWAC. The whitecapping or the free surface slope-induced breaking is activated through the keyword *WHITE CAPPING DISSIPATION* in the steering file; the keyword can take two values, namely:

- 0 no whitecapping-induced dissipation (*default value*)
- 1 Komen et al. [Komen et al., 1984] and Janssen's [Janssen, 1991] dissipation model.

In deep water, that term is written as follows in TOMAWAC:

$$Q_{ds} = -\frac{1}{g^4} C_{dis} \bar{\sigma}^9 m_0^2 \left( \delta \left( \frac{\sigma}{\bar{\sigma}} \right)^2 + (1 - \delta) \left( \frac{\sigma}{\bar{\sigma}} \right)^4 \right) F \quad (4.27)$$

With a finite water height, TOMAWAC uses the following formulation:

$$Q_{ds} = -C_{dis} \bar{\sigma} \bar{k}^4 m_0^2 \left( \delta \frac{k}{\bar{k}} + (1 - \delta) \left( \frac{k}{\bar{k}} \right)^2 \right) F \quad (4.28)$$

$m_0$  denotes the total variance,  $\bar{\sigma}$  denotes the average intrinsic frequency and  $\bar{k}$  denotes the average wave number; they are respectively computed as followings:

$$m_0 = \int_{f_r=0}^{\infty} \int_{\theta=0}^{2\pi} F(f_r, \theta) df_r d\theta \quad (4.29.a)$$

$$\bar{\sigma} = \left( \frac{1}{m_0} \int_{f_r=0}^{\infty} \int_{\theta=0}^{2\pi} \frac{1}{\sigma} F(f_r, \theta) df_r d\theta \right)^{-1} \quad (4.29.b)$$

$$\bar{k} = \left( \frac{1}{m_0} \int_{f_r=0}^{\infty} \int_{\theta=0}^{2\pi} \frac{1}{\sqrt{k}} F(f_r, \theta) df_r d\theta \right)^{-2} \quad (4.29.c)$$

The formulas for computing the average frequency and the average wave number are derived from those in use in WAM-cycle 4 [Komen et al., 1994]. These averages are not directly weighted by the variance spectrum, since it was found, when WAM-cycle 3 [WAMDI, 1988] was being developed, that the above expressions yielded more stable results than the conventional weighted averages. Lastly, it should be pointed out that in TOMAWAC the above average quantities are computed not only on the discretized portion of the variance spectrum, but also analytically on the high frequency portion (up to  $+\infty$ ) considering a decreasing variance in  $f^{-n}$ .

That source term has two parameters:

- constant  $C_{dis}$  (corresponding to the keyword *WHITE CAPPING DISSIPATION COEFFICIENT* in the steering file). Its default value is taken as 4.5, in accordance with the proposal made by Komen et al. [Komen et al., 1984] and the standard value adopted in the model WAM-Cycle 4.
- weighting parameter  $\delta$  (corresponding to the keyword *WHITE CAPPING WEIGHTING COEFFICIENT* in the steering file). Its default value is taken as the 0.5 average value.

#### 4.2.3.4. Bottom friction-induced dissipations (term $Q_{bf}$ )

A single model is available in TOMAWAC. The bottom friction-induced dissipation is activated through the keyword *BOTTOM FRICTION DISSIPATION* in the steering file; the keyword can take two values, namely:

1. no bottom friction-induced dissipation (*default value*)
2. expression obtained during the JONSWAP campaign (Hasselmann et al. [Hasselmann et al., 1973]) and taken up by Bouws and Komen [Bouws, 1983].

The model used for the bottom friction-induced energy losses is an empirical expression globally representing the various contributions from the wave-bottom interaction (percolation, friction...):

$$Q_{bf} = -\Gamma \left( \frac{\sigma}{g \cdot \sinh(k \cdot d)} \right)^2 F \quad (4.35)$$

That (linear) expression is programmed in TOMAWAC using the following alternative form, which involves the dispersion relation:

$$Q_{bf} = -\Gamma \frac{2k}{g \cdot \sinh(2 \cdot k \cdot d)} F \quad (4.36)$$

That source term has a single parameter:

- constant  $\Gamma$  (corresponding to the keyword *BOTTOM FRICTION COEFFICIENT* in the steering file). Its default value is taken as  $0.038 \text{ m}^2 \text{ s}^{-3}$ , in accordance with what had been obtained during the JONSWAP campaign [Hasselmann et al., 1973] and with the standard value being used in the model WAM-Cycle 4.

#### 4.2.3.5. Bathymetric breaking-induced dissipations (term $Q_{br}$ )

In TOMAWAC, four parametric formulas are proposed for reproducing the effects of the bathymetric breaking-induced energy dissipation on the spectrum. The bathymetric breaking-

induced dissipation is activated through the keyword *DEPTH-INDUCED BREAKING DISSIPATION* in the steering file; the keyword can take five values:

- 0 No breaking-induced dissipation (*default value*)
- 1 Battjes and Janssen's model [Battjes, 1978]
- 2 Thornton and Guza's model [Thornton, 1983]
- 3 Roelvink's model [Roelvink, 1993]
- 4 Izumiya and Horikawa's model [Izumiya, 1984]

The first three models are parametric spectral models developed for studying the random waves, whereas the fourth one is a turbulence model initially developed for studying the regular waves.

The general principle of the parametric spectral models consists in developing an expression for the total dissipation of wave energy by combining a rate of breaker-induced dissipation with a breaking probability.

Whatever model is adopted, the directional spectrum version of the bathymetric breaking-induced dissipation term is based on the assumption that breaking does not affect the energy frequency and direction distributions.

#### 4.2.3.5.1. Battjes and Janssen's model (1978)

The Battjes and Janssen's breaking model [Battjes, 1978] is based on the analogy with a hydraulic jump. Besides, it assumes that all the breaking waves have a height  $H_m$ , which is of the same order of magnitude as the water depth. The total energy dissipation term  $D_{br}$  is expressed as follows

$$D_{br} = -\frac{\alpha Q_b f_c H_m^2}{4} \quad (4.37)$$

where  $H_m$  denotes the maximum wave height being compatible with the water depth,  $Q_b$  is the fraction of breaking wave,  $f_c$  is a characteristic wave frequency and  $\alpha$  is a numerical constant of order 1.

$H_m$  can be computed either through the relation:

$$H_m = \gamma_2 d \quad (4.38)$$

or through a relation derived from the Miche's criterion

$$H_m = \frac{\gamma_1}{k_c} \tanh\left(\frac{\gamma_2 k_c d}{\gamma_1}\right) \quad (4.39)$$

where  $k_c$  is linked to  $f_c$  by the linear wave dispersion relation.

$Q_b$  is estimated, according to the Battjes and Janssen's theory, as a solution of the implicit equation:

$$\frac{1 - Q_b}{\ln Q_b} = -\frac{H_{m0}^2}{2H_m^2} \quad (4.40)$$

In TOMAWAC, that equation can be solved either in a dichotomous way or through explicit approximations as proposed by Dingemans [Dingemans, 1983]. The latter are expressed as follows when putting:

$$b = \frac{H_{m0}}{\sqrt{2}H_m}$$

- version 1:  $Q_b = 0$  if  $b < C_b$ , ( $C_b = 0.5$ )



$$Q_b = \left( \frac{b - C_b}{1 - C_b} \right)^2 \quad \text{if } b \geq C_b$$

- version 2:

$$q_0 = (2b - 1)^2 \quad \text{if } 0.5 < b < 1$$

$$q_0 = 0 \quad \text{if } b \leq 0.5$$

$$q_1 = q_0 - b^2 \frac{q_0 - e^{\lfloor (q_0 - 1)/b^2 \rfloor}}{b^2 - e^{\lfloor (q_0 - 1)/b^2 \rfloor}}$$

$$Q_b = 0 \quad \text{if } b \leq C_b, (C_b = 0.3)$$

$$Q_b = q_1 \quad \text{if } C_b < b < 0.9$$

$$Q_b = q_0 \quad \text{if } 0.9 \leq b \leq 1.0$$

- version 3:

$$Q_b = 2.4 * b^7$$

The directional spectrum version of the sink term is based on the assumption that breaking does not modify the frequency and directional distribution of energy. The source term  $Q_{br}$  is then written as:

$$Q_{br}(f, \theta) = - \frac{\alpha Q_b f_c H_m^2}{4} \frac{F(f, \theta)}{m_0} \quad (4.41)$$

Three constants can be modified using keywords:

- constant  $\alpha$  corresponds to the keyword *DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT ALPHA* in the steering file. Its default value is taken as 1, in accordance with the value as recommended by Battjes and Janssen [Battjes, 1978].
- constant  $\gamma_1$  corresponds to the keyword *DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA1* in the steering file. Its default value is taken as 0.88, in accordance with the value as recommended by Battjes and Janssen [Battjes, 1978].
- constant  $\gamma_2$  corresponds to the keyword *DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA2* in the steering file. Its default value is taken as 0.8, in accordance to the value as recommended by Battjes and Janssen [Battjes, 1978].

The following keywords are for selecting the model options:

- The characteristic wave frequency is selected through the keyword *DEPTH-INDUCED BREAKING 1 (BJ) CHARACTERISTIC FREQUENCY*. Six values are possible:
  1. average frequency:  $\bar{f} = \frac{\bar{\sigma}}{2\pi}$  (refer to equation (4.29.b));
  2. average frequency:  $f_{01}$ , computed from the spectrum moments  $m_0$  and  $m_1$  (default value);
  3. average frequency:  $f_{02}$ , computed from the spectrum moments  $m_0$  and  $m_2$ ;
  4. discrete peak frequency:  $f_p$ ;
  5. peak frequency computed through the Read's method to order 5:  $f_{R5}$ ;
  6. peak frequency computed through the Read's method to order 8:  $f_{R8}$ .
- The computation mode for breaking probability  $Q_b$  (exact computation or utilization of an explicit approximation as proposed by Dingemans [Dingemans, 1983]) is selected through the keyword *DEPTH-INDUCED BREAKING 1 (BJ) QB COMPUTATION METHOD*. By default, version 2 of the explicit formulations as proposed by Dingemans [Dingemans, 1983] is used (see above). For applications, it is recommended **not** to modify the value of that keyword.

- The computation mode for the maximum height compatible with the local water depth,  $H_m$ , is selected through the keyword *DEPTH-INDUCED BREAKING 1 (BJ) HM COMPUTATION METHOD*. Two values are possible:
  1. Relation:  $H_m = \gamma_2 d$  (default value);
  2. Miches' relation (see in (4.39) above)

#### 4.2.3.5.2. Thornton and Guza's model (1983)

The Thornton and Guza's breaking model [Thornton, 1983] is based on the analogy with a hydraulic jump and on two types of breaking wave height distribution. The energy sink term is written according to the breaking wave height distribution being retained:

$$\text{function 1: } Q_{br1}(f, \theta) = -48\sqrt{\pi} B^3 f_c \frac{(2m_0)^{5/2}}{H_m^4 d} F(f, \theta) \quad (4.42.a)$$

$$\text{function 2: } Q_{br2}(f, \theta) = -12\sqrt{\pi} B^3 f_c \frac{(2m_0)^{3/2}}{H_m^2 d} \left[ 1 - \left( 1 + \left( \frac{8m_0}{H_m^2} \right) \right)^{-5/2} \right] F(f, \theta) \quad (4.42.b)$$

$f_c$  is the characteristic wave frequency (average frequency,  $f_{01}$ ,  $f_{02}$  or peak frequency) and  $B$  is a parameter ranging from 0.8 to 1.5 (its default value in TOMAWAC is  $B = 1.0$ ). The maximum wave height compatible with the water depth,  $H_m$ , is governed by the parameter  $\gamma$  ( $H_m = \gamma d$ ).

The breaking model as proposed by Thornton and Guza can then be parameterized by the user via the following 4 keywords:

- « *DEPTH-INDUCED BREAKING 2 (TG) WEIGHTING FUNCTION* Two values are possible:
  1. weighting function 1 (see in (4.42.a));
  2. weighting function 2 (see in (4.42.b)) (default value).
- « *DEPTH-INDUCED BREAKING 2 (TG) CHARACTERISTIC FREQUENCY*. Six values are possible:
  1. average frequency:  $\bar{f} = \frac{\bar{\sigma}}{2\pi}$  (refer to equation (4.29.b));
  2. average frequency:  $f_{01}$ , computed from the spectrum moments  $m_0$  et  $m_2$ ;
  3. average frequency:  $f_{02}$ , computed from the spectrum moments  $m_0$  et  $m_2$ ;
  4. discrete peak frequency:  $f_p$ ;
  5. peak frequency computed through the Read's method to order 5:  $f_{R5}$  (default value);
  6. peak frequency computed through the Read's method to order 8:  $f_{R8}$ ;
- *DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT B*, corresponding to the  $B$  variable. Its default value in the model is taken as 1.
- « *DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT GAMMA*, corresponding to the  $\gamma$  variable. Its default value in the model is taken as 0.42.

#### 4.2.3.5.3. Roelvink's model (1993)

The Roelvink's breaking model [Roelvink, 1993] is based on the analogy with a hydraulic jump and on two types of wave height distribution in the breaking zone (Weibull or Rayleigh). The energy sink term is written according to the wave height distribution in the breaking zone:

- Weibull's distribution:

$$Q_{br1}(f, \theta) = -\alpha f_c m A \sqrt{\frac{2}{m_0}} F(f, \theta) \int_0^{\infty} \left( \frac{H}{\sqrt{8m_0}} \right)^{2m+1} \exp \left[ -A \left( \frac{H}{\sqrt{8m_0}} \right)^{2m} \right] \left[ 1 - \exp \left( - \left( \frac{H}{\gamma d} \right)^N \right) \right] dH \quad (4.43)$$

$$A = \left[ \Gamma \left( 1 + \frac{1}{m} \right) \right]^m \quad \text{with} \quad m = 1 + 0.7 \tan^2 \left( \frac{\pi}{2} \frac{1}{\gamma_2} \frac{\sqrt{8m_0}}{d} \right) \quad (4.44)$$

The coefficient  $\gamma_2$  is usually set to 0.65.

- Rayleigh's distribution:

$$Q_{br2}(f, \theta) = -\alpha f_c \sqrt{\frac{2}{m_0}} F(f, \theta) \int_0^{\infty} \left( \frac{H}{\sqrt{8m_0}} \right)^3 \exp \left[ - \left( \frac{H}{\sqrt{8m_0}} \right)^2 \right] \left[ 1 - \exp \left( - \left( \frac{H}{\gamma d} \right)^N \right) \right] dH \quad (4.45)$$

$f_c$  denotes the characteristic wave frequency (average frequency,  $f_{01}$ ,  $f_{02}$  or peak frequency),  $\alpha$  is a numerical constant of order 1,  $\gamma$  is the proportional control factor between the allowable wave height and the water depth (by default,  $\gamma = 0.54$ ) and  $N$  is an exponent in the wake breaking weighting function (typically  $N=10$ ).

Thus, the Roelvink's breaking model can be parameterized by the user via the following 5 keywords:

- « *DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT ALPHA*, corresponding to the  $\alpha$  variable. Its default value in the model is taken as 1.0.
- « *DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA*, corresponding to the  $\gamma$  variable. Its default value in the model is taken as 0.54.
- « *DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA2*, corresponding to the  $\gamma_2$  variable. Its default value in the model is taken as 0.65.
- « *DEPTH-INDUCED BREAKING 3 (RO) WAVE HEIGHT DISTRIBUTION* provided for retaining either a Weibull distribution (4.43) if the (default) value of the parameter is 1 or a Rayleigh distribution (4.45) if the parameter value is 2.
- « *DEPTH-INDUCED BREAKING 3 (RO) EXPONENT WEIGHTING FUNCTION*, corresponding to the  $N$  variable. Its default value in the model is 10.
- « *DEPTH-INDUCED BREAKING 3 (RO) CHARACTERISTIC FREQUENCY* Six values are possible:

1. average frequency:  $\bar{f} = \frac{\bar{\sigma}}{2\pi}$  (refer to equation (4.29.b));
2. average frequency:  $f_{01}$ , computed from the spectrum moments  $m_0$  et  $m_2$ ;
3. average frequency:  $f_{02}$ , computed from the spectrum moments  $m_0$  et  $m_2$ ;
4. discrete peak frequency:  $f_p$ ;
5. peak frequency computed through the Read's method to order 5:  $f_{R5}$  (default value);
6. peak frequency computed through the Read's method to order 8:  $f_{R8}$ .

#### 4.2.3.5.4. Izumiya and Horikawa's turbulence model (1984)

Izumiya and Horikawa [Izumiya, 1984] sought an estimate of the dissipation by breaking-induced turbulence in the case of regular waves. From the Reynolds' equations and only considering a one-

dimensional condition, they obtained an expression of the breaking-induced dissipation of wave energy in the following form:

$$\frac{d}{dx}(EC_g) = -\alpha \frac{E^{3/2}}{\rho^{1/2} d^{3/2}} \left( \frac{2C_g}{c} - 1 \right)^{1/2} \quad (4.46)$$

$E$  denotes the total wave energy,  $C_g$  and  $c$  are respectively group and phase velocities associated to the characteristic wave frequency  $f_c$  (average frequency  $f_{01}$ ,  $f_{02}$  or peak frequency),  $\alpha$  is a parameter governing the magnitude of the energy dissipation to be determined. For any profile, a shoal may induce the wave reforming. In order to take that process into account, Izumiya and Horikawa express the factor  $\alpha$  in terms of a deviation from a steady state:

$$\alpha = \beta_0 (M_*^2 - M_{*s}^2)^{1/2}$$

where  $M_*$  is a dimensionless quantity in the form:  $M_*^2 = \frac{C_g}{c} \cdot \frac{E}{\rho g d^2}$

From laboratory data, Izumiya and Horikawa set  $M_{*s}^2$  to  $9 \cdot 10^{-3}$  and  $\beta_0$  to 1.8.

Assuming that the breaking does not affect the frequency and direction distribution of energy, the dissipation term is lastly written as:

$$Q_{br}(f, \theta) = -\beta_0 \left( \frac{C_g}{c} \cdot \frac{m_0}{d^2} - M_{*s}^2 \right)^{1/2} \frac{g^{1/2} m_0^{1/2}}{d^{3/2}} \left( \frac{2C_g}{c} - 1 \right)^{1/2} F(f, \theta) \quad (4.47)$$

Thus, the breaking model as proposed by Izumiya and Horikawa can be parameterized by the user through the three following keywords:

- « *DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT BETA0*, corresponding to the  $\beta_0$  variable. The default value in the model is 1.8.
- « *DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT M2STAR*, corresponding to the  $M_{*s}^2$  variable. The default value in the model is 0.009.
- « *DEPTH-INDUCED BREAKING 4 (IH) CHARACTERISTIC FREQUENCY*. Six values are possible:

1. average frequency:  $\bar{f} = \frac{\bar{\sigma}}{2\pi}$  (refer to equation (4.29.b));
2. average frequency:  $f_{01}$ , computed from the spectrum moments  $m_0$  et  $m_2$ ;
3. average frequency:  $f_{02}$ , computed from the spectrum moments  $m_0$  et  $m_2$ ;
4. discrete peak frequency:  $f_p$ ;
5. peak frequency computed through the Read's method to order 5:  $f_{R5}$  (default value);
6. peak frequency as computed through the Read's method to order 8:  $f_{R8}$ .

#### 4.2.3.6. Non-linear quadruplet interactions (term $Q_{nl}$ )

A single model is available in TOMAWAC. The non-linear quadruplet interactions are through the keyword *NON-LINEAR TRANSFERTS BETWEEN FREQUENCIES* in the steering file; the keyword can take two values, namely:

- 0 no non-linear quadruplet interaction (default value)
- 1 Hasselmann et al. [Hasselmann et al., 1985] DIA method (Discrete Interaction Approximation) which is a discrete parameterization of the exact computation operator as proposed by Hasselmann [Hasselmann, 1962] [Hasselmann, 1962].

The method and its implementation in TOMAWAC have been the subject of a specific report [Benoit, 1997] which the reader is invited to refer to for further information. The major teachings of the DIA method are summarized below.

The exact expression of the deep water interactions term as set by Hasselmann [Hasselmann, 1962] [Hasselmann, 1962], expressed herein for convenience as a function of the wave number vector, is analogous to a Boltzmann integral:

$$Q_{nl}^{exact} = \iiint \sigma_4 G \delta(\vec{k}_1 + \vec{k}_2 - \vec{k}_3 - \vec{k}_4) \delta(\sigma_1 + \sigma_2 - \sigma_3 - \sigma_4) \left[ \frac{F(\vec{k}_1)}{\sigma_1} \frac{F(\vec{k}_2)}{\sigma_2} \left( \frac{F(\vec{k}_3)}{\sigma_3} + \frac{F(\vec{k}_4)}{\sigma_4} \right) - \frac{F(\vec{k}_3)}{\sigma_3} \frac{F(\vec{k}_4)}{\sigma_4} \left( \frac{F(\vec{k}_1)}{\sigma_1} + \frac{F(\vec{k}_2)}{\sigma_2} \right) \right] d\vec{k}_1 d\vec{k}_2 d\vec{k}_3 \quad (4.30)$$

The energy exchanges, in that integral (*a priori* rather uneasily computable), take place between quadruplets meeting the resonance conditions:

$$\sigma_1 + \sigma_2 = \sigma_3 + \sigma_4 \quad \text{and} \quad \vec{k}_1 + \vec{k}_2 = \vec{k}_3 + \vec{k}_4 \quad (4.31)$$

as evidenced by the two Dirac functions  $\delta$  in the integral.

$G$  denotes the value of the coupling term for the resonant quadruplet interactions  $(\vec{k}_1, \vec{k}_2, \vec{k}_3, \vec{k}_4)$ . Establishing and computing its expression is also an awkward task. Hasselmann [Hasselmann, 1962] proposed a computation mode that was also taken up and given a more concise form by such other authors as Webb [Webb, 1978].

The exact computation of the above Boltzmann integral is too complex and time-consuming for such a sea state operational model as TOMAWAC (see e.g. [Hasselmann, 1985]). That is why, starting from the experiment as developed in WAM [WAMDI, 1988] [Komen et al., 1994], TOMAWAC uses the DIA (« Discrete Interaction Approximation ») approximate computation method as proposed by Hasselmann et al. [Hasselmann et al., 1985]. Whereas the exact computation requires the summation of the contributions from a great number of quadruplets, the approximate computation implements only a small number of quadruplet configurations that are all similar.

That standard interaction configuration is defined as follows:

- two of the wave numbers are alike:  $\vec{k}_1 = \vec{k}_2 = \vec{k}$ , which also involves that the two related frequencies are identical:  $\sigma_1 = \sigma_2 = \sigma$
- the other two frequencies  $\sigma_3$  and  $\sigma_4$  are defined by:

$$\sigma_3 = (1 + \lambda) \sigma = \sigma^+$$

$$\sigma_4 = (1 - \lambda) \sigma = \sigma^-$$

Through the value  $\lambda = 0.25$ , a good correlation with the exact computation of the integral [Hasselmann et al., 1985] could be achieved. That value is used in the model WAM [WAMDI, 1988] [Komen et al., 1994] and is taken up in TOMAWAC.

- since the wave vectors  $\vec{k}_3 = \vec{k}^+$  and  $\vec{k}_4 = \vec{k}^-$  should observe the resonance condition, it can be shown they are featured by angles  $\theta_3 = 11.5^\circ$  and  $\theta_4 = -33.6^\circ$  with respect to the common direction of  $\vec{k}_1 = \vec{k}_2 = \vec{k}$  (refer to [Hasselmann et al., 1985]).
- Furthermore, the mirror image is taken into account by considering the vectors as symmetrical with respect to the direction of  $\vec{k}_1 = \vec{k}_2 = \vec{k}$ .

The standard interaction configuration (in full line) and its mirror image (in dotted line) are shown schematically in Figure 4.2.

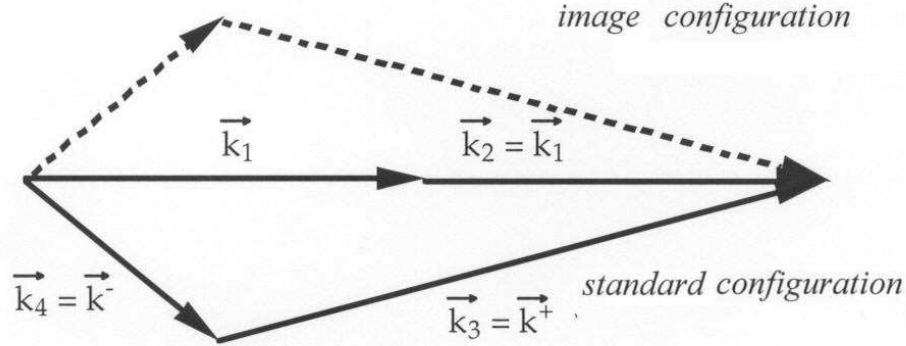


Figure 4.2: Schematic standard interaction configuration for the DIA method

With this standard configuration, the non-linear interaction term for all four resonant wave numbers is written as [Hasselmann et al., 1985]:

$$\begin{bmatrix} Q_{nl} \\ Q_{nl}^- \\ Q_{nl}^+ \end{bmatrix} = \begin{bmatrix} -2 \\ 1 \\ 1 \end{bmatrix} \Pi g^{-4} f_r^{11} \left( F^2 \left( \frac{F^+}{(1+\lambda)^4} + \frac{F^-}{(1-\lambda)^4} \right) - \frac{2FF^+F^-}{(1-\lambda^2)^4} \right) \quad (4.32)$$

With such a computation method, the vector  $\vec{k}$  scans all the discretization nodes of the directional spectrum mesh. The number of configurations being considered is then twice as large as the number of points in that mesh. In relation to the full computation, the 5-dimensional space (three integration dimensions and two dimensions for  $\vec{k}_4$ ) of all the possible resonant quadruples is reduced to a 2-dimensional space.

In a finite water depth, from exact computations of the Boltzmann integral, Herterich and Hasselmann [Herterich, 1980] suggested to make a deep water computation based on the previous method, then to multiply it by a coefficient  $R$  representing the effect of the finite water height:

$$Q_{nl}(d) = R \cdot Q_{nl}(d = \infty) \quad (4.33)$$

Coefficient  $R$  is a function of the normalized water height  $\bar{k} \cdot d$  and is expressed as follows:

$$R(\chi) = 1 + \frac{5.5}{\chi} \left( 1 - \frac{5}{6} \chi \right) \exp\left(-\frac{5}{4} \chi\right) \quad \text{where: } \chi = \frac{3}{4} \bar{k} \cdot d \quad (4.34)$$

The average wave number  $\bar{k}$  was defined in the previous paragraph (see in (4.29.c)).

In its authors' opinion, that relation remains valid as long as  $\bar{k} \cdot d > 1$ . It is used as such in TOMAWAC for the finite water depth computations.

That source-term has a single parameter:

- constant  $\lambda$  (corresponding to the keyword *STANDARD CONFIGURATION PARAMETER* of the steering file). Its default value is taken as 0.25, in accordance with the proposal made by Hasselmann et al. [Hasselmann et al., 1985] and with the standard value in the model WAM-Cycle 4.

#### 4.2.3.7. Non-linear transfers between triads (*Qtr* term)

##### 4.2.3.7.1. LTA (Lumped Triad Approximation) model

A parametric model allowing to take into account the non-linear triad interactions in the averaged-phase models has been proposed by Eldeberky and Battjes [Eldeberky, 1995]. The LTA model is a parametric approach that is based on the Madsen and Sorensen's deterministic spectral model [Madsen, 1993]. Simplifying hypotheses are introduced for reducing the computation cost. Thus, a parametric formulation is given for the biphase as a function of the Ursell's number and the model is restricted to the self-interactions.

The source term is written as:

$$Q_{LTA}(f, \theta) = Q_{LTA}^+(f, \theta) + Q_{LTA}^-(f, \theta)$$

$$Q_{LTA}^+(f, \theta) = \alpha_{LTA} c C_g g^2 \frac{R_{(f/2, f/2)}^2}{S_f^2} \sin|\beta_{f/2, f/2}| [F^2(f/2, \theta) - 2F(f, \theta)F(f/2, \theta)] \quad (4.48)$$

$$Q_{LTA}^-(f, \theta) = -2Q_{LTA}^+(2f, \theta)$$

$\alpha_{LTA}$  is the model adjustment coefficient;  $c$  and  $C_g$  denote the phase and group velocities, respectively.

$$R \text{ is the self-interaction coefficient: } R_{f,f} = (2k)^2 \left[ \frac{1}{2} + \frac{(2\pi f)^2}{gdk^2} \right] \quad (4.49)$$

$$S \text{ is given by the relation: } S_f = -2k(gd + 2Bgd^3k^2 - (B + 1/3)d^2(2\pi f)^2) \quad (4.50)$$

$$\text{The biphase } \beta \text{ is given by the relation: } \beta(f, f) = -\frac{\pi}{2} + \frac{\pi}{2} \tanh\left(\frac{0.2}{Ur}\right) \quad (4.51)$$

$$\text{where } Ur \text{ denotes the Ursell's number: } Ur = \frac{g}{8\pi^2 \sqrt{2}} \frac{H_{m0} T_m^2}{d^2} \quad (4.52)$$

with  $H_{m0}$  being the significant spectral height and  $T_m$  being the average wave time.

$Q_{LTA}^\pm$  denotes the negative and positive contributions of the self-interactions. Since  $Q_{LTA}^+$  denotes the positive contributions to the first upper harmonic, it should be positive. The negative values of  $Q_{LTA}^+$  are replaced by the zero value. In the numerical integration of the energy equation, the source term for the triad interactions is generally only computed for frequencies that are lower than  $R_{fm}f_m$  (Ris [Ris, 1997]) where  $R_{fm} = 2.5$ .

Two constants can be modified through keywords:

- constant  $\alpha_{LTA}$  corresponding to the keyword *TRIADS 1 (LTA) COEFFICIENT ALPHA*. Its default value is  $\alpha_{LTA} = 0.5$
- constant  $R_{fm}$  corresponding to the keyword *TRIADS 1 (LTA) COEFFICIENT RFMLTA*. Its default value is  $R_{fm} = 2.5$

##### 4.2.3.7.2. SPB model

The SPB model was developed by Becq [Becq, 1998] from the extended Boussinesq equations as proposed by Madsen and Sorensen [Madsen, 1992]. The model is for simulating the

effects induced by the collinear and non-collinear interactions of spectral components. The source term is written as:

$$Q(f, \theta) = \frac{B'g}{2S_{1,f}} \int_0^f \int_0^{2\pi} \int_0^f \int_0^{2\pi} df_1 df_2 d\theta_1 d\theta_2 T_{f_1, f_2} \delta(\theta_{\vec{k}} - \theta_{\vec{k}_1 + \vec{k}_2}) \delta(f - f_1 - f_2) \\ + \frac{B'g}{S_{1,f}} \int_0^\infty \int_0^{2\pi} \int_0^\infty \int_0^{2\pi} df_1 df_2 d\theta_1 d\theta_2 T_{-f_2, f_1} \delta(\theta_{\vec{k}_1} - \theta_{\vec{k} + \vec{k}_2}) \delta(f_1 - f - f_2) \quad (4.53)$$

$$\text{with: } T_{f_1, f_2} = \frac{gK}{K^2 + \Delta k^2} R_{f_1, f_2} \left[ -\frac{R_{-f_2, f}}{S_{2, f_1} k_1} F F_2 - \frac{R_{-f_1, f}}{S_{2, f_2} k_2} F F_1 + \frac{R_{f_1, f_2}}{S_{2, f} k} F_1 F_2 \right] \quad (4.54.a)$$

$$B' = \frac{Cg}{2\pi k} \quad (4.54.b)$$

$$R_{f_1, f_2} = (k_1 + k_2)^2 \left[ \frac{1}{2} + \frac{(2\pi)^2 f_1 f_2}{gdk_1 k_2} \right] \quad (4.54.c)$$

$$S_f = -2k(gd + 2Bgd^3 k^2 - (B + 1/3)d^2(2\pi f)^2) \quad (4.54.d)$$

$F$  denotes the variance spectrum in terms of frequencies and directions,  $F(f, \theta)$ .  $T_{f_1, f_2}$  and  $T_{-f_2, f_1}$  respectively correspond to the sum and difference interactions.  $K$  is the model adjustment parameter.

Since the model was designed for taking into account the energy transfers for all the possible triad configurations within the spectrum, the computation times are very long. In order to shorten these computation times, the interactions can be restricted over a range of spectral components that are included within a given angular sector. Thus, directional limits can be user-prescribed.

Three constants can be modified through keywords:

- constant  $K$  corresponding to the keyword *TRIADS 2 (SPB) COEFFICIENT K*. Its default value is  $K = 0.34$
- the lower and upper directional markers corresponding to the keywords *TRIADS 2 (SPB) LOWER DIRECTIONAL BOUNDARY* and *TRIADS 2 (SPB) UPPER DIRECTIONAL BOUNDARY*. Their respective default values are 0 and 360.



## 5. Discretizations used in TOMAWAC

The main aspects concerning the numerical discretization in TOMAWAC are presented and discussed herein for the two spatial variables (paragraph 5.1), for the two spectro-angular variables (paragraph 5.2) and for the time domain (paragraph 5.3).

### 5.1. Spatial discretization

The spatial coordinate system, whether it is Cartesian or spherical, is a planar two-dimensional domain that is meshed by means of triangular finite elements. Only the maritime portion of the computational domain is meshed, so that all the computational points of the spatial grid are provided with a water depth that is strictly above zero. Through this discretization technique, the mesh size may naturally be variable over the spatial domain, particularly enabling to get a fine grid in the areas of specific interest, featured either by complex geometries (straits, intracontinental seas, bays...) or by high bathymetric gradients. Furthermore, that spatial grid may include one or more islands.

The number of discretization points is only limited by the RAM capacities of the computing machine. The equation solved by TOMAWAC does not prescribe *a priori* any conditions about the number of grid points per wave length. The density of spatial discretization points is left at the user's will. It should match, however, both spatial and temporal scales of variation of the physical characteristics of the domain being studied, in particular bathymetry and wind field.

In the general case, this spatial grid is realised on a workstation using one of the mesh generators associated to the TELEMAC system (refer to the 7.2.2 for further details about the preparation of the grid). Two examples of spatial grids developed for TOMAWAC for simulated storms in the North Atlantic Ocean, the Channel and the North Sea are illustrated in Figure 5.1.

### 5.2. Spectro-angular discretization

#### 5.2.1. Frequency discretization

In TOMAWAC, the frequency domain is discretized considering a series of  $NF$  frequencies in a geometric progression:

$$f_n = f_{l,q}^{n-1} \text{ with } n \text{ ranging from } 1 \text{ to } NF$$

The minimum frequency is then  $f_l$  and the maximum frequency is  $f_{l,q}^{NF-1}$ .

In order to define the frequency discretization, the user should specify as an input into the steering file:

- the frequency number:  $NF$  (corresponding to the keyword *NUMBER OF FREQUENCIES* in the steering file)
- the minimum frequency:  $f_l$  (in Hertz) (corresponding to the keyword *MINIMAL FREQUENCY* in the steering file)
- the frequential ratio:  $q$  (corresponding to the keyword *FREQUENTIAL RATIO* in the steering file)

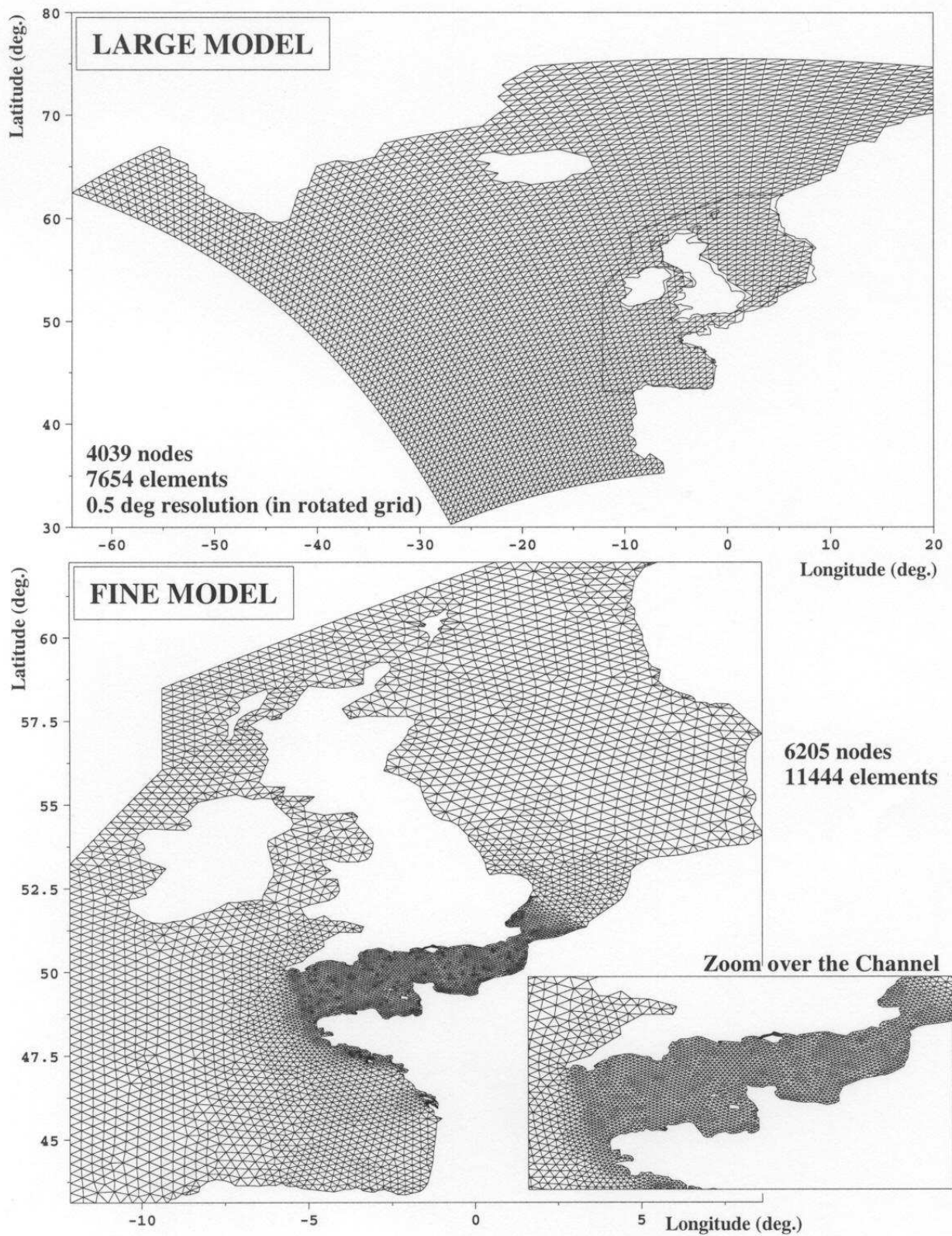


Figure 5.1: Examples of spatial grids in the Atlantic Ocean, the Channel and the North Sea

### 5.2.2. Directional discretization:

The interval of propagation direction  $[0, 360^\circ]$  is discretized into  $ND$  evenly distributed directions, so that these directions are:

$$\theta_m = (m-1) \cdot 360/ND \quad \text{with } m \text{ ranging from 1 to } ND$$

In order to define the directional discretization, the user should specify as an input into the steering file:

- the direction number:  $ND$  (corresponding to the keyword *NUMBER OF DIRECTIONS* in the steering file).
- The direction convention selected for the input/output directional variables: either nautical or counterclockwise (corresponding to the keyword *TRIGONOMETRICAL CONVENTION* in the steering file, the default value of which is NO). The nautical convention sets the wave propagation directions (towards which the waves are propagating) in relation to the true North or the vertical axis and opposite to the counterclockwise direction. The counterclockwise convention sets the wave propagation directions in relation to the horizontal axis.
- Note that the convention selected for computing the directions within the FORTRAN code always defines the propagation directions in the clockwise direction from the true North, even though the keyword *TRIGONOMETRICAL CONVENTION* = YES !

### 5.2.3. Spectro-angular grid:

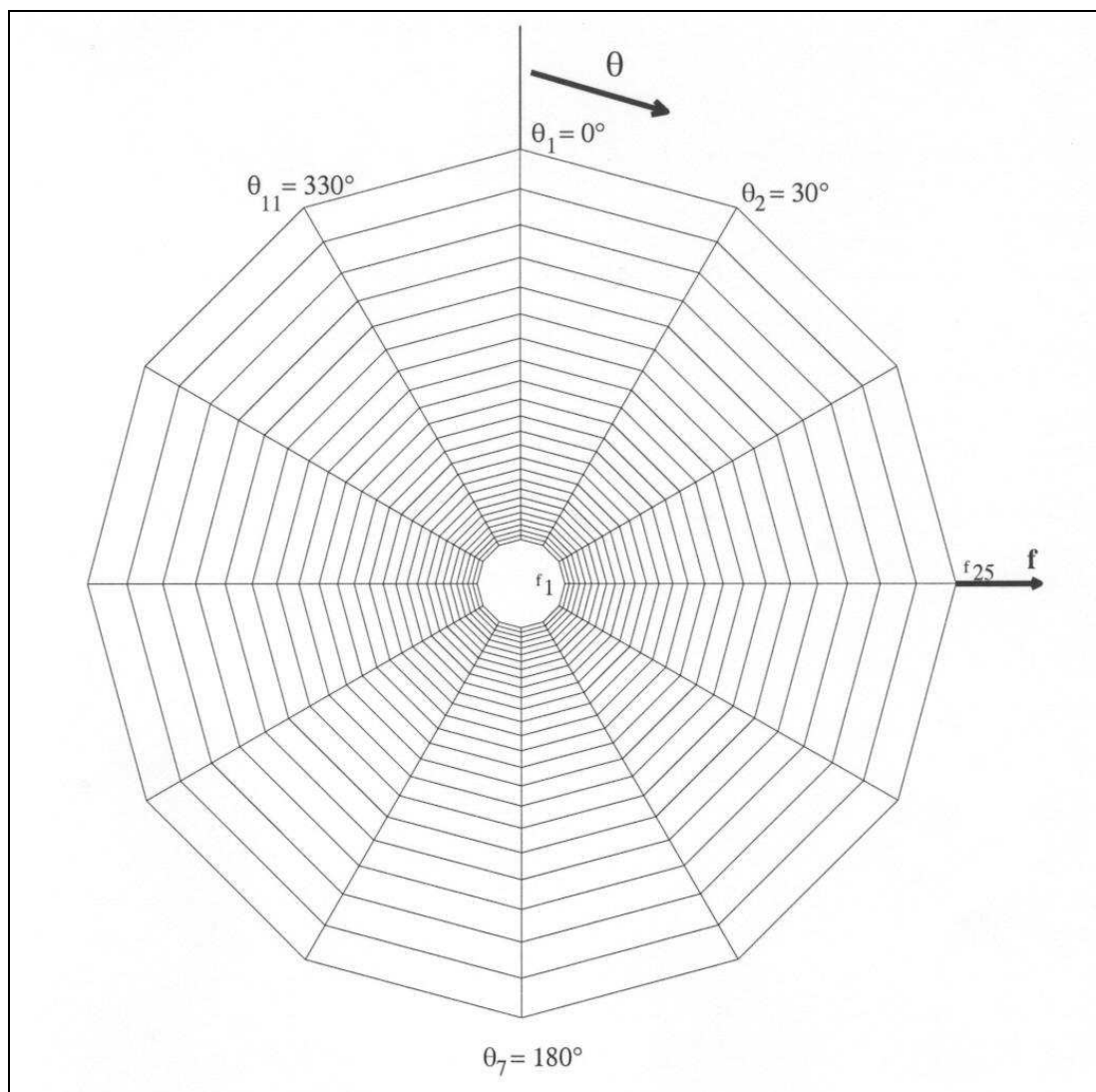
A two-dimensional grid for spectro-angular discretization is achieved by combining the above defined frequency and directional discretizations. That grid has  $NF \cdot ND$  points.

A polar representation is used in TOMAWAC, where the wave frequencies are measured radially and where the propagation direction corresponds to the value of the angle in relation to the axis selected by the user as (vertical or horizontal) origin. An example of a spectro-angular grid having 25 frequencies and 12 directions is illustrated in Figure 5.2.

## 5.3. Temporal discretization

In TOMAWAC, each computation begins at the internal date 0, to which an actual date being defined by the keyword *DATE OF COMPUTATION BEGINNING* in the steering file can be associated. That date is specified as per the yymmddhhmm format which corresponds to the moment dd/mm/yy at hh:mm (for example, 9505120345 corresponds to May 12, 1995 at 3.45).

The evolution equation of the directional spectrum of wave action density is integrated with a constant time step, that is expressed in seconds through the keyword *TIME STEP* in the steering file. Sub-iterations of that time step can also be made for computing the source terms (refer to paragraph 6.3). That number of sub-time steps per time step is defined in the steering file through the keyword *NUMBER OF ITERATIONS FOR THE SOURCE TERMS*.



*Figure 5.2: Example of a spectro-angular grid as used by TOMAWAC  
(25 frequencies and 12 directions in this case)*

## 6. Numerical methods used in TOMAWAC

### 6.1. General solution algorithm

As stated in Section 4, the equation to be solved by the TOMAWAC software is a transport (convection) equation with source terms that can be written in the following general form:

$$\frac{\partial(B F)}{\partial t} + \vec{V} \cdot \vec{\nabla}(B F) = B Q \quad (6.1)$$

Both functions  $F$  and  $Q$  are functions of five variables and depend, e.g. in Cartesian coordinates, on  $x$ ,  $y$ ,  $\theta$ ,  $f_r$  and  $t$ . The above equation is then to be solved on a four-dimensional grid in  $(x, y, \theta, f_r)$  and  $\vec{V}$  is a transport vector, which is a dimension-4 vector in the general case. It is reduced, however, to a three-dimensional vector ( $\dot{f}_r$  is zero) when there is neither a current nor a variation of water depth in time.

$$\vec{V} = \begin{pmatrix} \dot{x} \\ \dot{y} \\ \dot{\theta} \\ \dot{f}_r \end{pmatrix} \quad (6.2)$$

Equation (6.1) is solved in TOMAWAC through a fractional step method, i.e. the convection and the source term integration steps are solved successively and separately. Thus, the following steps are successively solved from a current state at the date  $t = n.\Delta t$ , in which the variance spectrum  $F^n$  is known in all points:

- a **convection step** without source terms (refer to paragraph 6.1.2):

$$\frac{\partial(B F)}{\partial t} + \vec{V} \cdot \vec{\nabla}(B F) = 0 \quad (6.3)$$

discretized as follows:

$$\frac{(B.F)^* - (B.F)^n}{\Delta t} = [\vec{V} \cdot \text{grad}(B.F)]^n \quad (6.4)$$

from which a value of  $(B.F)^*$ , then of  $F^*$ , intermediate after the convection step, is derived

- a **source term integration step** (refer to paragraph 6.1.3):

$$\frac{\partial F}{\partial t} = Q \quad (6.5)$$

discretized as follows:

$$\frac{F^{n+1} - F^*}{\Delta t} = \frac{Q^{n+1} + Q^*}{2} \quad (6.6)$$

since coefficient  $B$  is time independent.

The variance density spectrum  $F^{n+1}$  for a time step (time  $t = (n+1).\Delta t$ ) is then obtained. That operation is then repeated for the next time step and as many times as necessary for covering the simulation period being considered.

## 6.2. Processing the propagation step

The propagation step is solved in TOMAWAC by means of the method of characteristics, which is largely used at the LNHE for processing various convection equations (refer for example to [Esposito, 1981]). The application of that method to TOMAWAC has a specific feature: the method should be applied to a dimension-4 space in the general case and to a dimension-3 space when there is no current and the depth is constant over time; furthermore the domain in propagation directions is periodic.

It should be reminded that equation (6.3) without source terms is processed in that step, being discretized as follows for a time step  $\Delta t_p$ :

$$\frac{(B.F)^* - (B.F)^n}{\Delta t_p} = [\vec{V} \cdot \text{grad}(B.F)]^n \quad (6.7)$$

The convector field  $\vec{V}$ , whose expression was given in Section 4, is not time dependent when there is no tide, just like factor  $B$  (refer to paragraph 4). The equation to be processed can be simplified as follows in that case:

$$\frac{B.F^* - B.F^n}{\Delta t_p} = \vec{V} \cdot [\text{grad}(B.F)]^n \quad (6.8)$$

This is a major advantage, since the characteristics can be traced back only once, at the beginning of the simulation. It is sufficient to store the origin of the characteristic pathlines and to retrieve them whenever the convection step is called. For each quadruplet  $(x_Q, y_Q, \theta_Q, f_{rQ})$  of the discretized spatial and spectro-angular variables, the characteristic curve is traced back to the time step  $\Delta t_p$  and the “arrival” point  $(x_P, y_P, \theta_P, f_{rP})$ , which is called foot of the characteristic pathline, is stored. Actually, the numbers of the discretization elements (triangular elements for the spatial grid and quadrangular elements for the spectro-angular grid) including that foot of the characteristic pathline, as well as the linear interpolation coefficients allowing to obtain the values in that point from the values at the apices of the elements (barycentric coordinates), are kept. Thus, the convection step can be reduced in the form:

$$(B.F)^*(x_Q, y_Q, \theta_Q, f_{rQ}) = (B.F)^n(x_P, y_P, \theta_P, f_{rP}) \quad (6.9)$$

That step requires a short computation time since it only consists of an interpolation operation over each time step, once the characteristics have been traced back at the beginning of a computation.

When there is a tide, the principle remains unchanged, but the characteristics should be traced back after every depth and current update.

Such a method has the advantage of being unconditionally stable, enabling to revoke the condition that requires a Courant number below 1 and which is implemented, for example, in the upstream off-centred first-order propagation scheme being used in the WAM-cycle 4 model [WAMDI, 1988] [Komen et al., 1994]. The finite element grid generation technique is provided for achieving a locally finer computational grid in order to represent irregular bathymetric features or an irregular coastline. Thanks to the applied propagation scheme, the time step does not necessarily have to be much reduced, so that reasonable computation times can be kept. It should actually be clear that, rather than the propagation step, the source term integration step (particularly the computation of non-linear interactions) does consume most of the computation time. As regards the numerical schemes in which the propagation step implies a shorter time step when making the grid finer (e.g. as in the case of the WAM model), the overall computation time happens to become much longer because of the source terms and the model becomes less attractive for the practical applications.

Owing to the method of characteristic, on the contrary, the TOMAWAC model allows to overcome that restriction and is therefore attractive even for grids with a rather fine spatial resolution. The method of characteristic, however, has some drawbacks due to the fact that, in the general case, it has a significant level of numerical diffusion and is not conservative.

### 6.3. Processing the source term integration step

#### 6.3.1. Source term integration numerical scheme

The source and sink terms in the equation of variance density spectrum evolution are integrated using the following scheme, which can be changed by the user from fully explicit to fully implicit:

$$\frac{F^{n+1} - F^*}{\Delta t} = (1 - \chi)Q^* + \chi Q^{n+1} \quad (6.10)$$

where the exponent \* denotes the values of the variables after the propagation step (but before the source term integration step) and the exponent  $n+1$  denotes the values of the variables after the source term integration step. The parameter  $\chi$ , set by the user through the keyword *IMPLICITATION COEFFICIENT FOR SOURCE TERMS* in the steering file, should lie in the range [0 ; 1]:

- $\chi = 0$  corresponds to the fully explicit scheme (only the value of source terms  $Q^*$  are used). This option is not advised for practical applications.
- $\chi = 0.5$  corresponds to the semi-explicit scheme, used in the WAM-Cycle 4 model [WAMDI, 1988] [Komen et al., 1994]. It enables to use fairly long time steps (about 20-30 min in an oceanic environment). This value was the only one considered in earlier versions of TOMAWAC. It is the default value of the keyword.
- $\chi = 1$  corresponds to the fully implicit scheme, as used for instance in a modified version of WAM [Hersbach and Janssen, 1999].

Emphasis should be laid on the fact that the source term integration step is « local », i.e. it is carried out independently for each point in the 2D spatial grid.

The numerical implementation of the scheme is briefly presented below.

We first define  $\Delta F = F^{n+1} - F^*$ , the change in the spectrum value. Then the source/sink terms are classified as linear ( $Q_l$ ) or non-linear terms ( $Q_{nl}$ ) in the wave spectrum  $F$ :

$$Q = Q_l + Q_{nl} \quad (6.11)$$

- As regards the source terms that are linear in  $F$ , note that:  $Q = \beta F$ , hence we get:

$$Q_l^{n+1} = \beta^{n+1} F^{n+1} = \beta^{n+1} F^* + \beta^{n+1} \Delta F \quad (6.12)$$

- As regards the source terms that are non-linear in  $F$ , a Taylor's expansion is done keeping only the first-order term:

$$Q_{nl}^{n+1} \approx Q_{nl}^* + \frac{\partial Q_{nl}^*}{\partial F} \Delta F \quad (6.13)$$

$\frac{\partial Q_{nl}^*}{\partial F}$  is a matrix of differential increments that is broken down into a diagonal component  $[A^*]$  and an extra-diagonal component  $[N^*]$ :

$$\frac{\partial Q_{nl}^*}{\partial F} = [M^*] = [A^*] + [N^*] \quad (6.14)$$

Substituting into the expression of  $Q_{nl}^{n+1}$ , this yields:

$$Q_{nl}^{n+1} \approx Q_{nl}^* + ([A^*] + [N^*])\Delta F \quad (6.15)$$

Adding the contributions from the linear and nonlinear terms, we obtain:

$$Q^* = \beta^* F^* + Q_{nl}^* \quad (6.16)$$

$$Q^{n+1} = Q_l^{n+1} + Q_{nl}^{n+1} = \beta^{n+1} F^* + \beta^{n+1} \Delta F + Q_{nl}^* + ([A^*] + [N^*])\Delta F \quad (6.17)$$

The variation of the variance density spectrum due to the source terms is written as:

$$\Delta F = F^{n+1} - F^* = \Delta t \left( (1 - \chi) Q^{n+1} + \chi Q^* \right) \quad (6.18)$$

i.e., after substitution of the source term expressions:

$$\Delta F = \Delta t \left\{ (1 - \chi) [\beta^* F^* + Q_{nl}^*] + \chi [\beta^{n+1} F^* + \beta^{n+1} \Delta F + Q_{nl}^* + ([A^*] + [N^*])\Delta F] \right\} \quad (6.19)$$

$$\Delta F [1 - \chi \Delta t (\beta^{n+1} + ([A^*] + [N^*]))] = \Delta t \left( (1 - \chi) \beta^* + \chi \beta^{n+1} \right) F^* + Q_{nl}^* \quad (6.20)$$

The matrix between brackets in the left-hand member of the latter equation cannot be easily inverted in the general case. The designers of the WAM model [WAMDI, 1988], however, demonstrated that the diagonal portion  $[A^*]$  usually prevails over the extra-diagonal portion  $[N^*]$ . Relying on comparative tests, they conclude that the extra-diagonal portion can be ignored in favour of the diagonal portion, even with time steps of 20 min or so. Due to that simplification, the inversion is much easier and we finally obtain:

$$\Delta F \approx \Delta t \frac{((1 - \chi) \beta^* + \chi \beta^{n+1}) F^* + Q_{nl}^*}{1 - \chi \Delta t (\beta^{n+1} + A^*)} \quad (6.21)$$

For the sake of convenience, that expression is rewritten as:

$$\Delta F = \frac{\Delta t Q_{TOT}}{1 - \chi \Delta t Q_{DER}} \quad (6.22)$$

where:  $Q_{TOT} = ((1 - \chi) \beta^* + \chi \beta^{n+1}) F^* + Q_{nl}^*$  denotes a total source term

and  $Q_{DER} = \beta^{n+1} + A^*$  denotes a source term derived with respect to F.

The contributions of the various source terms implemented in TOMAWAC and described in paragraph 4.2.3 are schematically illustrated in the Table 6.1.

The source term integration time step may be different from the propagation time step in TOMAWAC, but it should be a sub-multiple of it. Thus, several source term integration time sub-steps per propagation time step can be defined. That option is governed by the keyword *NUMBER OF ITERATIONS FOR THE SOURCE TERMS* in the steering file. The default value of that parameter is set to 1.



Source/sink terms	Linear or non-linear	Remarks	Type of contribution to $Q_{DER}$	Type of contribution to $Q_{TOT}$
Wind input	Linear or quasi-linear	$\beta$ depends on time	$\beta^{n+1}$	$\left((1-\chi)\beta^* + \chi\beta^{n+1}\right)F^*$
Whitecapping	Quasi-linear	Slightly non-linear	$\Lambda^*$	$\Lambda^*F^*$
Bottom friction	linear	$\beta$ does not depend on time	$\beta$	$\beta F^*$
Non-linear transfers between frequency quadruplets	non-lin.		$\Lambda^*$	$Q_{nl4}^*$
Bathymetric breaking	linear	$\beta$ does not depend on time $\beta^{n+1} = \beta^n = \beta$	$\beta$	$\beta F^*$
Non-linear transfers between triads	non-lin		$\Lambda^*$	$Q_{tr}^*$

Table 6.1: Contributions of the different source/sink terms implemented in TOMAWAC.

It was found experimentally that the depth-induced breaking source term, which is sometimes very strong, can still be overestimated if the time step that was selected for the source term integration is too long. In order to avoid that, TOMAWAC gives an opportunity to make a number of time sub-steps that are specific to that source term. These time sub-steps are in a geometric progression. In order to limit that number of time sub-step, TOMAWAC first clips the wave height by setting a maximum  $H_m/d$  ratio ( $d$  being the depth) to 1.

Subsequently, a Euler's explicit scheme is used at each time step:

$$\frac{F^{n+1} - F^*}{\Delta t_2} = Q^* \quad \text{i.e.} \quad \Delta F = \Delta t_2' Q^* \quad (6.23)$$

The  $H_m/d$  ratio can be modified through the keyword *MAXIMUM VALUE OF THE RATIO HMO ON D* (however, this is not advisable). The number of time sub-steps is specified through the keyword *NUMBER OF BREAKING TIME STEPS*. The geometric ratio is given by the keyword *COEFFICIENT OF THE TIME SUB-INCREMENTS FOR BREAKING*.

### 6.3.2. Monitoring the growth of the wave spectrum

In order to limit the possible risks of numerical instabilities related to the source term integration, TOMAWAC is provided with various options for limiting the growth of the directional spectrum per source term integration time step. The choice of option is done by the user in the steering file through the keyword *WAVE GROWTH LIMITER*, which can be set to 0, 1 (default value) or 2:

0 : no limiter is applied to the computed  $\Delta F$  from the various source/sink terms.

- 1 : the limiter is directly inspired by the criterion proposed by the WAM group [WAMDI, 1988]. The absolute variation of the variance density spectrum as it was computed by the scheme in paragraph 6.3.1. should remain lower than a fraction of an equilibrium spectrum  $\Delta F_{lim}$ :

$$\Delta F_{lim} = 6.4 \cdot 10^{-7} g^2 \frac{\Delta t}{1200} f^{-5} \quad (6.24)$$

This is presently the default value in TOMAWAC, as it was the only possibility in earlier versions of the code.

- 2 : the limiter is computed with an updated expression, proposed by Hersbach and Janssen [Hersbach and Janssen, 1999]:

$$\Delta F_{lim} = 3.0 \cdot 10^{-7} g \max(u^*, g \tilde{f}_{PM}/f) f^{-4} f_{NF} \Delta t \quad (6.25)$$

where  $u^*$  is the friction velocity at the water surface and  $\tilde{f}_{PM} = 5.6 \cdot 10^{-3}$  is the dimensionless Pierson–Moskowitz peak frequency.

This option should now be preferably used for practical applications.

## 6.4. Processing the boundaries – Boundary conditions

### 6.4.1. Spatial grid:

Two types of boundary conditions are considered in TOMAWAC for the finite element spatial grid:

- The former corresponds to a free boundary condition, i.e. that absorbs the whole wave energy. It may be a sea boundary, hence it is assumed that the waves propagate beyond the domain and nothing enters it. It may be a solid boundary, hence it is assumed that the coast absorbs completely the wave energy (no reflection).
- The latter corresponds to a prescribed value boundary condition. The whole wave spectrum is then prescribed at each point along that boundary and for each step. Energy enters into the computational domain.

### 6.4.2. Spectro-angular grid:

As regards the propagation directions, the grid generation is periodical over the range  $[0 ; 360^\circ]$ : hence there are no directional boundary conditions.

As regards the wave frequencies that are discretized, the minimum and maximum frequency markers are considered as “open boundary limits”, where the energy can be transferred to lower or higher frequencies, exiting the discretized frequency range.

## 7. Inputs-outputs

### 7.1. Preliminary remark

During a computation, the TOMAWAC software uses a number of files, some of which are optional, as inputs and outputs.

The input files are:

- The steering or CAS file (mandatory),
- The mesh or geometry file (mandatory),
- The boundary conditions or CONLIM file (mandatory),
- The seabed, bottom or bathymetry file (optional),
- The FORTRAN or PRINCI file (optional),
- The currents file (optional),
- The winds file (optional),
- The previous computation file (optional),
- The binary user file (optional),
- The formatted user file (optional).

The output files are:

- The 2D results or grid file (mandatory),
- The punctual results or spectra file (mandatory),
- The next computation file (optional),
- The listing printout (either on the display screen or in the file, see APPENDIX 1),
- The binary user file (optional),
- The formatted user file (optional).

### 7.2. The files

#### 7.2.1. The steering (or CAS) file

The steering file name is specified in the steering file through the keyword: *STEERING FILE*.

It is a text file created by means of a text editor. In a way, it serves as the computation control panel. It includes a set of keywords to which values are assigned. If a keyword does not appear in this file, then TOMAWAC will assign to it the default value as defined in the dictionary file (refer to the description in APPENDIX 3). If such a default value is not defined in the dictionary, then the computation will come to a halt and display an error message. For instance, the command *NUMBER OF DIRECTIONS* = 12 is for specifying that the direction spectrum of wave action or its moments will be discretised over 12 propagation directions.

TOMAWAC reads the steering file at the beginning of the computation.

Both dictionary file and steering file are read by the so-called DAMOCLES utility which is included in TOMAWAC. The syntactic rules of DAMOCLES should then be observed upon the creation of the steering file. These rules are described here below.

The write rules are as follows:

- The keywords can be of the Integer, Real, Logical or Character format type.
- The keyword sequence order in the steering file is of no importance.

- Each line has a maximum of 72 characters. However, as many linefeeds as one wants are allowed provided that the keyword name does not run from one line to the next.
- For the table-like keywords, the successive values are separated by a semi-colon. A number of values equal to the table dimension should not necessarily be given; in such a case, DAMOCLES returns the number of values being read. For example:  
*ABSCISSAE OF SPECTRUM PRINTOUT POINTS* = 1.2;3.4  
(that keyword is declared as a 99-valued table)
- The symbols ":" or "=" are indiscriminately used to separate a keyword from its value. They can be either preceded or followed with any number of blanks. The value itself may appear on the next line. For example:  
*NUMBER OF DIRECTIONS* = 12  
or  
*NUMBER OF DIRECTIONS*: 12  
or else  
*NUMBER OF DIRECTIONS* =  
12
- The characters occurring between a pair of "/" on one line are regarded as comments. Likewise, the characters occurring between a "/" and a the end of a line are regarded as comments. For example:  
*TYPE OF BOUNDARY DIRECTIONAL SPECTRUM* = 1 / Jonswap spectrum
- A whole line beginning with a "/" in the first column is regarded as a comment, even though another "/" occurs on the line. For example:  
/ The geometry file is ./maillage/geo
- Integer writing: Do not exceed the maximum size being allowed by the machine (in a machine with 32 bit architecture, the values range from -2 147 483 647 to + 2 147 483 648. Do not enter a blank between the sign (optional for the + sign) and the number. A dot at the end of the number is tolerated.
- Real writing: A dot or a comma is allowed as a decimal point, as well as the FORTRAN E and D formats (1.E-3 0.001 0,001 1.D-3 denote the same value).
- Logical value writing: The values 1, YES, OUI, .TRUE., TRUE, VRAI on the one hand, and 0, NO, NON, .FALSE., FALSE, FAUX on the other hand are allowed.
- Character string writing: Those strings including blanks or reserved symbols ("/", ":", "=", "&") should be put in single quotes (''). The value of a character keyword may include up to 144 characters. As in FORTRAN, the quotes occurring within a string should be doubled. A string may neither begin nor end with a blank. For example:  
*TITLE* = 'HOULE D'OUEST'

In addition to the keywords, a number of directives or metacommands that are interpreted during the sequential readout of the steering file may be used as well:

- The *&FIN* command indicates the end of file (even though the file is not completed). Thus, some keywords can be disabled simply by placing them behind that command for easily making it possible to enable them again subsequently.
- The *&ETA* command prints the list of keywords and the relevant values at the time when DAMOCLES meets that command. This display will occur at the beginning of listing printout.
- The *&LIS* command prints the list of keywords. This display will occur at the beginning of listing printout.

- The *&IND* command prints the detailed list of keywords. This display will occur at the beginning of listing printout.
- The *&STO* command causes the interruption of the program, the computation does not go on.

### 7.2.2. The geometry file

The geometry file name is specified in the steering file through the keyword: *GEOMETRY FILE*.

It is a SERAFIN-formatted binary file: it can be read by FUDAA PRE-PRO or RUBENS and it can be created by the STBTEL module from the file(s) as produced by the mesh generator. The SERAFIN format structure is described in APPENDIX 8.

This file includes the complete information about the horizontal mesh, i.e. the number of mesh points (variable NPOIN2), the number of elements (variable NELEM2), the X and Y vectors containing the co-ordinates of all the points and, lastly, the IKLE2 vector containing the connectivity table.

Furthermore, this file may also include bathymetry information in each point of the mesh, provided that the interpolation of the bathymetry was carried out during the execution of the STBTEL module or during the generation of the mesh.

TOMAWAC reproduces the information regarding the geometry at the beginning of the 2D results. Any computation results file can then be used as a geometry file when one wants to perform a further simulation on the same mesh.

### 7.2.3. The boundary conditions file.

The boundary conditions file name is specified in the steering file through the keyword: *BOUNDARY CONDITIONS FILE*.

It is a formatted file that can be created automatically by STBTEL and can be modified by means of a text editor. Each line in this file is assigned to one point of the boundary and listed in sequential order in terms of the boundary node numbers. The numbering of the boundary points first delineates the domain contour in the counterclockwise direction, then the islands in the clockwise direction.

This file is described in detail in 8.5.1.

### 7.2.4. The currents file

According to its type – binary or formatted- the currents file name is specified in the steering file through the keywords: *BINARY CURRENTS FILE* and *FORMATTED CURRENTS FILE*.

It is the file from which TOMAWAC reads the current field components. The current field may be either stationary or non-stationary. The current field will be non-stationary when the keyword *CONSIDERATION OF TIDE* is set to TRUE. When the current field is stationary, the keyword *CONSIDERATION OF A STATIONARY CURRENT* should be set to TRUE. By default, both keywords will be set to FALSE. When both are set to TRUE, the keywords will be inconsistent, and the program will halt.

Several commonly used formats can be read. This selection is made through the integer keyword *CURRENTS FILE FORMAT*. It can be set to a value from 1 to 4

- The format is 1: it is a finite-difference-typed format (as described in APPENDIX 8). The file is formatted and the file name should be assigned to the keyword: *FORMATTED CURRENTS FILE*
- The format is 2: it is a point pattern-type SINUSX format (as described in APPENDIX 8). This file is formatted and the file name should be assigned to the

keyword: *FORMATTED CURRENTS FILE*. This format cannot be used for reading a non-stationary current.

- The format is 3: it is a TELEMAC result file of the SERAFIN standard. It is a binary file and its name should be assigned to the keyword: *BINARY CURRENTS FILE*. If the current is assumed to be stationary, then the additional keyword *TIME INCREMENT NUMBER IN TELEMAC FILE* should be used in order to find the time step number related to the desired record. TELEMAC data other than the current components e.g. water levels, can also be read by means of this format (refer to 8.2.5).
- The format is 4: data written in a different format can be read provided that the user supplies the relevant subroutine in the relevant FORTRAN file (see 8.2.3 and 8.2.6).

#### 7.2.5. The tidal water level file

According to its type – binary or formatted- the tidal water level file name is specified in the steering file through the keywords: *BINARY TIDAL WATER LEVEL FILE* or *FORMATTED TIDAL WATER LEVEL FILE*.

This is the file from which TOMAWAC reads the tidal water level being referred to the *INITIAL STILL WATER LEVEL*. Several commonly used formats can be read. This selection is made by means of the integer keyword *TIDAL WATER LEVEL FILE FORMAT*. It can be set to a value from 1 to 3.

- The format is 1: it is a finite-difference-typed format (as described in APPENDIX 8). The file is formatted and the file name should be assigned to the keyword: *FORMATTED TIDAL WATER LEVEL FILE*.
- The format is 2: it is a TELEMAC result file of the SERAFIN standard. It is a binary file and its name should be assigned to the keyword: *BINARY TIDAL WATER LEVEL FILE*.
- The format is 3: data written in a different format can be read provided that the user supplies the relevant subroutine in the relevant FORTRAN file (see in 8.2.6).

#### 7.2.6. The winds file

According to its type – binary or formatted- the wind file name is specified in the steering file through the keywords: *BINARY WINDS FILE* or *FORMATTED WINDS FILE*.

This is the file from which TOMAWAC reads the information about the wind fields. As in the case of the current, several read formats are allowed. The integer keyword *WINDS FILE FORMAT* can be set to values from 1 to 4.

- The format is 1: it is a WAM-cycle 4 format type (as described in APPENDIX 8). The file is formatted and the file name should be assigned to the keyword: *FORMATTED WINDS FILE*
- The format is 2: it is a point pattern-type SINUSX format (as described in APPENDIX 8). The file is formatted and the file name should be assigned to the keyword: *FORMATTED WINDS FILE*.
- The format is 3: it is a TELEMAC result file of the SERAFIN standard. It is a binary file and its name should be assigned to the keyword: *BINARY WINDS FILE*. If the wind is assumed to be stationary, then the additional keyword *TIME STEP NUMBER IN TELEMAC FILE* should be used in order to find the time step number related to the desired record.
- The format is 4: data written in a different format can be read provided that the user supplies the relevant subroutine in the relevant FORTRAN file (see in 8.2.4).

### 7.2.7. The previous computation file

This previous computation file name is specified in the steering file through the character keyword: *PREVIOUS COMPUTATION FILE*.

If a *NEXT COMPUTATION* is done, TOMAWAC fetches this file in order to initialize the directional spectrum of wave action at every point. This file's format, which is specific to TOMAWAC, is described in APPENDIX 8. It is a binary file.

### 7.2.8. The global results file

The global results file name is specified in the steering file through the keyword: *GLOBAL RESULTS FILE*.

This file is created when a *GLOBAL OUTPUT AT THE END* is requested. It saves the wave action density directional spectrum at every point in the last time step. This file format is described in APPENDIX 8.

### 7.2.9. The 2D results file

The 2D results file name is specified in the steering file through the character keyword: *2D RESULTS FILE*.

This is the file into which TOMAWAC writes the results of the 2-dimensional variables during the computation. It is a binary file of the SERAFIN standard. The data contained in it are in the following order:

- 1- all the data about the mesh geometry;
- 2- the names of the variables being stored;
- 3- for each time step, the time and the values of the variables are given for each point of the 2D mesh.

Its content varies according to the values of the following keywords:

- *NUMBER OF FIRST ITERATION FOR GRAPHICS PRINTOUTS*: provided for determining from which time step will the data storage desirably begin, so that the file size will not be too large.
- *PERIOD FOR GRAPHICS PRINTOUTS*: sets the period, as a number of propagation time increments, of printouts so that the file size will not be too large.
- *VARIABLES FOR 2D GRAPHICS PRINTOUTS*: provided for specifying the list of variables to be stored into the 2D results file. Each variable is identified by 2, 3 or 4 letters. Table 7.1 lists the available variables. A more detailed description of the 2D variables is provided in APPENDIX 7.

M0	Total variance
HM0	Spectral significant wave height
DMOY	Mean wave direction
SPD	Mean directional spreading
ZF	Sea bottom level
WD	Water depth
UX	Current along X
UY	Current along Y
VX	Wind along X
VY	Wind along Y
FX	Driving force along X
FY	Driving force along Y

SXX	Radiation stress along xx
SYX	Radiation stress along yy
SXY	Radiation stress along xy
UWB	Bottom celerity
POW	Wave power (per meter along wave crest)
FMOY	Mean frequency FMOY
FM01	Mean frequency FM01
FM02	Mean frequency FM02
FPD	Discrete peak frequency
FPR5	Peak frequency by Read method of order 5
FPR8	Peak frequency by Read method of order 8
US	Surface friction velocity $u^*$
CD	Surface drag coefficient CD
Z0	Surface roughness length Z0
WS	Surface wave stress
TMOY	Mean period Tmoy
TM01	Mean period Tm01
TM02	Mean period Tm02
TPD	Discrete peak period
TPR5	Peak period by Read method of order 5
TPR8	Peak period by Read method of order 8
PRI	Private table
BETA	Breaking waves coefficient

Table 7.1: List of 2D results variables

For instance, if the significant wave heights, the water depths and the average wave propagation directions are desired,

*VARIABLES FOR 2D GRAPHICS PRINTOUTS* = HM0,WD,DMOY

must be entered in the steering file.

#### 7.2.10. The punctual or spectrum results file

This file's name is specified in the steering file through the character keyword: *PUNCTUAL RESULTS FILE*.

This is the file into which the directional spectra of wave action at some previously specified points are stored by TOMAWAC during the computation. These points are selected by means of the following keywords:

- *ABSCISSAE OF SPECTRUM PRINTOUT POINTS* and *ORDINATES OF SPECTRUM PRINTOUT POINTS*: they are chart keywords. The maximum number of points is 99, i.e. a maximum of 99 printout points. The spectrum will be recorded at the closest point to the specified position, no spatial interpolation is made.
- This file is a SERAFIN formatted file. It first includes all the data about the spectral mesh geometry, then the names-codes of displayed points. This name-code is of the type: *Fa\_PT2Db*, where *a* denotes the point's sequence order number within the list written in the steering file and *b* denotes the number of the closest 2D point to the specified position. Subsequently, for each graphic printout, it contains the time and the value of the directional spectrum of wave action for each pair (direction, frequency) in the spectral mesh.



The keywords *PERIOD FOR GRAPHICS PRINTOUTS* and *NUMBER OF FIRST ITERATION FOR GRAPHICS PRINTOUTS* are shared by the two results files; thus, the printouts are synchronous for either file.

#### 7.2.11. The printout listing

This file contains all the messages as generated by TOMAWAC during the computation. It is the main report of a TOMAWAC run. Its content depends on the value of the following keyword:

- *PERIOD FOR LISTING PRINTOUTS*: this sets the time between two time steps of message transmission. This value is given in terms of the number of iterations. For example, the following sequence:

*TIME INCREMENT = 30.*

*PERIOD                      FOR                      LISTING                      PRINTOUTS                      =                      2*

will result in a print in the output listing every 60 seconds of simulation.

The listing is either displayed on the monitor or saved in a file. The file name is defined by the user at the execution of the TOMAWAC simulation (refer to APPENDIX 1).

#### 7.2.12. The User FORTRAN file

This User FORTRAN file name is specified in the steering file through the character keyword: *FORTRAN FILE*.

The FORTRAN contains all the user-modified TOMAWAC subroutines as well as the specifically developed routines for that computation.

This file is compiled and linked during run time in order to generate the executable being used for the simulation.

#### 7.2.13. The auxiliary files

Other input/output files may be used by TOMAWAC.

- A binary data or results file: its name is specified through the character keyword *BINARY FILE 1*.
- A formatted data or results file: its name is specified through the character keyword *FORMATTED FILE 1*.

These files can be used either for supplying data to the program or for allowing data to be processed that are not available in the standard results files; obviously, the user must manage the read and write operations of these files within the FORTRAN program.

#### 7.2.14. The dictionary file

This dictionary file contains all the information about the keywords (French/English name, default values, type). This file can be viewed in a text editor by the user, but it must not be modified in any way.

#### 7.2.15. The libraries

At the beginning of a computation, the main user-written FORTRAN routine is compiled, then linked in order to generate the executable program that is subsequently run.

The following libraries are used during the link editing operation:

- TOMAWAC library: contains the specific subroutines of the TOMAWAC computation model.

- `telemac` library: contains the specific subroutines of the TELEMAC-2D computation model.
- `damocles` library: contains the subroutines handling the steering file reading.
- `BIEF` library: contains the computation modules related to the finite element-typed operations (operations on both matrixes and vectors). This library is shared by all the simulation models as developed by the LNHE within the TELEMAC structure (`BIEF` means "Bibliothèque d'Eléments Finis", i.e. Finite Element Library).

### 7.3. Binary files

Binary files are an efficient way to store data on disk. However, binary files written on different computers may differ. TOMAWAC recognizes three types of binary files, namely:

- the native binary of the computer,
- IBM binary (so that a file that has been generated on an IBM computer can be read), and
- IEEE binary, so that these files can be read on a workstation (provided that the suitable subroutines are set up when installing TOMAWAC on the computer).

The following keywords can be used:

- *GEOMETRY FILE BINARY*, for the geometry file,
- *2D RESULTS FILE BINARY* for the 2D results file.
- *PUNCTUAL RESULTS FILE BINARY* for the punctual results file.
- *GLOBAL RESULTS FILE BINARY*, for the global results file,
- *PREVIOUS COMPUTATION FILE BINARY*, for the previous computation file,
- *CURRENTS FILE BINARY*, for the currents and/or TELEMAC results file.
- *TIDAL WATER LEVEL FILE BINARY*, for the tidal water level file,
- *WINDS FILE BINARY*, for the winds file.
- *BINARY 1 FILE BINARY* for binary file.

In all the cases, the default value as specified in the dictionary file is 'STD' (default value of the machine being used). The other possible values are 'IBM' and 'I3E'.

### 7.4. Files standard

Almost all files that were in Serafin format in previous versions of TOMAWAC, have been given a key-word for the file format.

If the name of the file is: "GEOMETRY FILE" ("FICHIER DE GEOMETRIE"), the new keyword will be: "GEOMETRY FILE FORMAT" ("FORMAT DU FICHIER DE GEOMETRIE").

This format is given in 8 characters. Three choices are possible so far:

1. 'SERAFIN' (do not forget the space at the end): it is the default standard within the TELEMAC processing chain. The format is recognized by the FUDAA PRE-PRO graphics post-processor. The RUBENS graphics post-processor reads the SERAFIN format as well, but it won't be developed anymore and it is bound to disappear. The SERAFIN file format is described in detail in APPENDIX 8.
2. 'SERAFIND': Serafin format, but with double precision. Can be used for a more accurate "computation continued" or for more accurate validations. Neither FUDAA PRE-PRO nor Rubens can read this format.
3. 'MED ': this is an EDF-CEA format used in the Salomé platform, that enables to use the post-processors of this platform. It is based on hdf5. This new format is not activated if you use the

default subroutine med.f provided, which is mostly void. If you take instead the file med.edf and rename it med.f, med formats will be available, but two additional libraries are necessary to use this format and have to be specified in the systel.ini file. Full instructions will be given in further releases, this is so far for internal use at EDF.

A new file structure has been added to library BIEF for simplifying the opening/closing and reading/writing operations with these file formats, as well as for simplifying the coupling between programmes. The description of this file structure and of the operations on those files are given in APPENDIX 9.

As specified in section 7.2.7, a fourth binary format exists, which is specific to TOMAWAC and is used only for saving the results when they are used to initialize a next computation. This binary file format cannot be read by the RUBENS post-processor, or by FUDAA PRE-PRO graphics post-processor.

### 7.5. Bathymetry data

The bathymetry information can be supplied to TOMAWAC at two levels:

- Directly in the geometry/mesh file by a bathymetry value being assigned to each node in the mesh. In this case the bathymetry data have been processed previously, running the STBTTEL module or mesh generator. For example, STBTTEL reads the information from one or more bottom topography files (up to 5 files) and performs an interpolation at every point within the domain;
- In the form of an irregular pattern of spot heights without any necessary relation to the mesh nodes, during the TOMAWAC computation. The interpolation is then performed directly by TOMAWAC with the same algorithm as used by STBTTEL. The bathymetry file name is given by the character keyword *BOTTOM TOPOGRAPHY FILE*. Unlike STBTTEL, TOMAWAC only handles one bottom topography file. The file can be in SINUSX format or can consist of three columns X,Y,Z.

TOMAWAC also provides an opportunity to carry out a smoothing of the bathymetry in order to get a more consistent geometry. The smoothing algorithm can be iterated several times in order to achieve more or less extensive smoothing. The number of iterations is set using the keyword *BOTTOM SMOOTHINGS* and is carried out within the CORFON subroutine. This keyword's default value is 0. (also refer to the programming of the CORFON user subroutine in 8.6.1).

NOTE: the bathymetry data should preferably be supplied to TOMAWAC in the form of water depth and not of water height. If necessary, a conversion can be performed in the CORFON subroutine.

## 8. Controlling the simulation

### 8.1. General parameterisation

The general parameterisation of the computation is controlled using the steering file.

#### 8.1.1. Computation title

The computation case title is specified by the keyword *TITLE*

#### 8.1.2. Parallel computing

The release 6.0 of TOMAWAC includes the possibility to carry out parallel computing. The number of processors used in a TOMAWAC simulation is defined by the keyword *PARALLEL PROCESSORS*. For more detail see APPENDIX 10.

#### 8.1.3. Computation time

The time data are prescribed using the two keywords *TIME STEP* (real) and *NUMBER OF TIME INCREMENTS* (integer). The former sets the elapsed time, in seconds, between two consecutive computation instants (but not necessarily two outputs in the results file). The number of time steps is for setting the overall computation time (which is obviously equal to the time increment value multiplied by the number of time steps).

An additional keyword also refers to time. This is the *DATE OF COMPUTATION BEGINNING*, which is used to identify the time in relation to the date/times written in the *WINDS FILE* (refer to APPENDIX 8, WAM-typed format). The convention adopted for writing the *DATE OF COMPUTATION BEGINNING* is yymmddhhmm. For instance, 0311051110 corresponds to November 5th, 2003, at 11.10 AM.

Note that when a computation is resumed, the initial time of the new computation corresponds to the last time increment in the previous computation (i.e. the computation is not resumed at time zero).

#### 8.1.4. Spectral discretisation

The spectral discretisation is defined by the following 5 keywords:

- *NUMBER OF DIRECTIONS*,
- *NUMBER OF FREQUENCIES*,
- *MINIMUM FREQUENCY*,
- *FREQUENTIAL RATIO*,
- *SPECTRUM TAIL FACTOR*.

It should be reminded that the directions are evenly distributed from 0 to 360 degrees. Two conventions can be chosen by the user for expressing the wave propagation by means of the keyword *TRIGONOMETRICAL CONVENTION* (logical). The trigonometrical convention locates the wave propagation from the positive X axis and the direction of rotation is in a counterclockwise direction. The default convention is the nautical convention (*TRIGONOMETRICAL CONVENTION* = NO) that locates the propagation direction in relation to the true "North", i.e. the Y axis. The selected direction of rotation is a clockwise direction. The direction will then correspond to the "heading" in the sense of the navigational maps, i.e. the direction the waves are propagating towards.

The frequencies are distributed geometrically in accordance with the following relation:

$$f_k = f_0 r^{k-1} \quad (k = 1, NF)$$

where  $f_0$  is the *MINIMUM FREQUENCY*

$r$  is the *FREQUENTIAL RATIO*

$NF$  is the *NUMBER OF FREQUENCIES*

In order to take the contribution of high frequencies (higher than the maximum discretized frequency) into account in the computations, it is assumed that the decay of the spectrum follows a law that is of the type  $f^n$ . The keyword *SPECTRUM TAIL FACTOR* corresponds to the value of  $n$ .

### 8.1.5. Release

When generating the executable, the release number of libraries being used for editing the links is indirectly provided by the keyword *TOMAWAC RELEASE NUMBER*. By default, TOMAWAC release 6.0 utilises the 6.0 releases of the TELEMAC system libraries.

### 8.1.6. Environment

When a vector computer is used, the CPU vector length used in the forced vectorisation technique can be specified by means of the keyword *VECTOR LENGTH*. The default value is 1 and is appropriate for scalar machines such as the present workstations. If a value of 1 is used on a vector machine, then the advantage of the vectorisation loops (although they are few in TOMAWAC) is lost.

## 8.2. Computation options

### 8.2.1. Co-ordinate system

Cartesian co-ordinates (expressed in meters) are used by default. For domains of a large extent, working in spherical co-ordinates may become necessary. The value of the logical keyword *SPHERICAL COORDINATES* should then be set to "TRUE". The co-ordinates are then expressed in degrees.

### 8.2.2. Finite depth

In nearshore areas, wave conditions will be influenced by the water depth and therefore the bottom effect can no longer be ignored. This is the default case in TOMAWAC: the keyword *INFINITE DEPTH* is set to "FALSE". In situations where depths effects are to be explicitly ignored the keyword *INFINITE DEPTH* should be set to "TRUE".

### 8.2.3. Taking a stationary current into account

A stationary current can be taken into account in the TOMAWAC release 6.0. The relevant logical keyword is *CONSIDERATION OF A STATIONARY CURRENT*. The current affects mainly the convection step.

The current can be specified in various ways.

When the current is either constant over the domain or can be described analytically, the *ANACOS.f* subroutine can be included in the FORTRAN file and modified accordingly. In this subroutine the UC and VC are NPOINT2-sized (number of points in the horizontal mesh) vectors and correspond to the components along the X and Y axes of the current, respectively. This is how the current is specified when the keyword *FORMATTED CURRENTS FILE* or *BINARY CURRENTS*

*FILE* is not specified, whereas the keyword *CONSIDERATION OF A STATIONARY CURRENT* is "TRUE".

TOMAWAC can also take into account a current provided in a binary or formatted file. The keyword *BINARY CURRENTS FILE* or *FORMATTED CURRENTS FILE* should then be given a value (the name of the file). Three different formats are available to read this data. The value corresponds to the keyword *CURRENTS FILE FORMAT* (see 7.2.4). When the currents file is taken from TELEMAC-2D, then an additional keyword should be specified, namely the *TIME INCREMENT NUMBER IN TELEMAC FILE*. This locates the desired record.

If the predefined formats cannot be used, the COUUTI.f subroutine can be included in the FORTRAN and modified accordingly, specifying the format 4 for the INDIC FORTRAN variable in the CAS file. The current data are read from the file and are interpolated onto the nodes of the computation mesh.

#### 8.2.4. Taking a wind into account

Consideration of a wind is specified by the logical keyword *CONSIDERATION OF A WIND*. The wind may be either stationary or variable in time and is specified by means of the logical keyword *STATIONARY WIND*.

When the wind can be described analytically, the user subroutine ANAVEN.f can be used. The wind is fully specified when the keywords *FORMATTED WINDS FILE* and *BINARY WINDS FILE* do not have any value, whereas the keyword *CONSIDERATION OF A WIND* is "TRUE".

TOMAWAC can also take into account a wind given in a binary or formatted file. In this case a value (the name of the file) should be assigned to the keyword *FORMATTED WINDS FILE* or *BINARY WINDS FILE*. The available formats for reading out these data correspond to the keyword *WINDS FILE FORMAT* (see in section 7.2.6. and APPENDIX 8).

When these predefined formats cannot be used, the subroutine VENUTI.f can be included in the FORTRAN file and modified accordingly, specifying the format 4 for the INDIV FORTRAN variable. On completion of reading the winds file, the wind components are used as such if provided on the computational mesh, or interpolated over that mesh if provided on a different grid.

NOTE: an interpolation between two different meshes of equivalent sizes is usually computationally very expensive. Although possible, it is highly inadvisable, particularly as regards to the wind, since this is a time-varying data item. In such cases a pre-interpolation over the computation mesh, e.g using STBTTEL is recommended, followed by the reading of the wind data in format 3. Alternatively this pre-interpolation can be performed by means of the FASP subroutine from the BIEF library.

#### 8.2.5. Recovering a TELEMAC data item

Recovering a 2D result data item from a TELEMAC-2D hydrodynamic computation might be of interest, e.g. the value of wind-driven surge at every point. To avoid an increase in the number of files the *BINARY CURRENTS FILE* is used to specify this input file. The keyword *CURRENTS FILE FORMAT* should then be set to 3. This option is further specified using the logical keyword *RECOVERY OF TELEMAC DATA ITEM*. The data item is located within the file through the *TIME INCREMENT NUMBER IN TELEMAC FILE* and the *RANK OF THE TELEMAC DATA ITEM TO BE RECOVERED* that corresponds to desired variable's sequence number in the record. The needed data are read from the file and interpolated over the computation mesh.

NOTE: a TELEMAC data item and the components of a current can both be read simultaneously provided that they occur in the same file at the same record.

The recovered variable, which is interpolated over the mesh, can be utilised in the subroutine VARTEL.

### 8.2.6. Taking the tide into account

Tide-induced effects, i.e. unsteady/non-stationary water levels and currents can be taken into account. The relevant logic keyword is *CONSIDERATION OF TIDE*.

In order to take tide into account, a current and a tide water depth that is referenced in relation to the "INITIAL STILL WATER LEVEL" must be specified. These data can be initialized in various ways:

Should the tide be easy to describe analytically, the *ANAMAR.f* subroutine, can be included in the FORTRAN file and modified accordingly. In the subroutine the terms UC and VC, ZM and DZHDT are NPOIN2-sized (number of points in the horizontal mesh) vectors and correspond to the current components along the X and Y axes, the tidal water level in relation to the "INITIAL STILL WATER LEVEL" and the water depth variation in time, respectively. An analytical expression must be assigned to all of these vectors.

TOMAWAC can also take into account a current that is given in a binary or formatted file. A value (the name of the currents file) should be assigned to the keyword *BINARY CURRENTS FILE* or *FORMATTED CURRENTS FILE*. Two different formats are available for reading these data. This format is specified using the keyword *CURRENTS FILE FORMAT* (see 7.2.4). When these predefined formats cannot be used, the user subroutine *COUUTI.f* can be included in the FORTRAN file and modified accordingly. In such cases the *CURRENTS FILE FORMAT* (FORTRAN variable INDIC) must be set to 4 in the CAS file. Once the data of the currents file are read, the current components are interpolated over the computation mesh.

The tidal water level can be also provided in a binary or formatted file. A value (the name of the water level file) should be assigned to the keyword *BINARY TIDAL WATER LEVEL FILE* or *FORMATTED TIDAL WATER LEVEL FILE*. Two different predefined formats are available for reading this data. The format type is specified using the keyword *TIDAL WATER LEVEL FILE FORMAT* (refer to 7.2.5). If the user chooses the Serafin format (i.e. TELEMAC-2D format), then the *RANK OF THE WATER LEVEL DATA IN THE TELEMATC FILE* must also be specified. When the predefined formats cannot be used, the user subroutine *MARUTI.f* file can be included in the FORTRAN file and modified accordingly. In such cases the *TIDAL WATER LEVEL FILE FORMAT* (the INDIM FORTRAN variable) must be set to 4 in the CAS file.

Both currents and tidal water levels will be updated upon each *TIDE REFRESHING PERIOD*. This keyword corresponds to an integer multiple of the propagation *TIME STEP*, i.e. the currents and tidal levels cannot be specified at time steps less than the model *TIME STEPS*.

### 8.2.7. Convection step

For specific validation tests, for example, it may be interesting to drop the convection step and only consider the effect of the source terms. To do this requires assigning the "FALSE" value to the keyword *CONSIDERATION OF PROPAGATION*.

## 8.3. Parameterising the source term integration step

### 8.3.1. Introduction

When it is required to take into account the source/sink terms, the logic keyword *CONSIDERATION OF SOURCE TERMS* should be set to "TRUE".

It has been shown that the source term integration may require a shorter time step than the time step that is used for convection. The *TIME STEP* in the steering file corresponds to the convection time step. The source term integration step is controlled using the integer keyword *NUMBER OF ITERATIONS FOR THE SOURCE TERMS*. This keyword is set to the number of source terms

integration time steps that will be conducted after each convection step (default value = 1). The effective time-step used for source term integration is thus:

$(TIME\ STEP)/(NUMBER\ OF\ ITERATIONS\ FOR\ THE\ SOURCE\ TERMS)$ .

Depending on the source/sink terms, two different schemes are used for time integration:

- For the source/sink terms that are dominant in large and medium water depths (namely wind input, white-capping dissipation, nonlinear quadruplet interactions and bottom friction) a scheme with variable implicitation level is used (see section 8.3.2).
- For the source/sink terms that are dominant in shallow water depths (namely depth-induced breaking and, nonlinear triad interactions) an explicit scheme is used, possibly with sub-steps to cover one source term time-step (see section 8.3.3).

### 8.3.2. Source/sink terms in large and medium water depth

#### 8.3.2.1. Wind input

If the keyword *WIND GENERATION* is set to 0, no wind input will be taken into account. If, on the other hand, a strictly positive value (1, 2, ...) is chosen, the corresponding wind input formulation will be taken into account.

In TOMAWAC the Janssen's formulation (see section 4.2.3.2 for details) has been implemented and is activated using the value 1 for the *WIND GENERATION* keyword. Janssen's formulation requires several additional data, specified by the following keywords:

*AIR DENSITY,*  
*WATER DENSITY,*  
*WIND GENERATION COEFFICIENT,*  
*VON KARMAN CONSTANT,*  
*CHARNOCK CONSTANT,*  
*SHIFT GROWING CURVE DUE TO WIND,*  
*WIND DRAG COEFFICIENT,*  
*WIND MEASUREMENT LEVEL.*

As a general rule, the default values for these keywords shall not be modified.

#### 8.3.2.2. White capping dissipation

If the integer keyword *WHITE CAPPING DISSIPATION* is set to 0, this source term will be ignored. If a strictly positive value (1, 2, ...) is selected, the corresponding formulation will be taken into account.

The only formulation implemented is Komen's formulation (see section 4.2.3.3 for details) and corresponds to the value 1 of the *WHITE CAPPING DISSIPATION* keyword. This formulation requires two complementary data, specified by the following keywords:

*WHITE CAPPING DISSIPATION COEFFICIENT*  
*WHITE CAPPING WEIGHTING COEFFICIENT.*

As a general rule, the default values for these keywords shall not be modified.

#### 8.3.2.3. Bottom friction dissipation

If the integer keyword *BOTTOM FRICTION DISSIPATION* is set to 0, this source term will be ignored. If a strictly positive value (1, 2, ...) is chosen, the corresponding formulation will be taken into account. This source term is only taken account if the keyword *INFINITE DEPTH* is set to "FALSE".



The only formulation implemented is from Hasselmann (see section 4.2.3.4 for details) This formulation is specified by setting the *BOTTOM FRICTION DISSIPATION* keyword to 1. This formulation requires the specification of the keyword:

*BOTTOM FRICTION COEFFICIENT.*

As a general rule, the default value for this keyword shall not be modified.

#### 8.3.2.4. Non-linear transfers between quadruplets

If the integer keyword *NON-LINEAR TRANSFERS BETWEEN FREQUENCIES* is set to 0, this source term will not be taken into account. If a strictly positive value (1, 2, ...) is chosen, the corresponding formulation will be taken into account.

Only the formulation from Hasselmann (see in section 4.2.3.6) has been implemented and corresponds to the value 1 for the *NON-LINEAR TRANSFERS BETWEEN FREQUENCIES* keyword. This formulation does not require any additional data to be specified by the user.

### 8.3.3. Source/sink terms in shallow water depth

#### 8.3.3.1. Time integration scheme and time step

As mentioned above, the depth-induced breaking and nonlinear triad interaction terms are time-integrated with an explicit scheme.

As found practically, contributions from these source terms can be overestimated if the selected time step for source term integration is too long. In order to avoid this, TOMAWAC can perform a number of time sub-steps which are specific to these source terms through the keyword *NUMBER OF BREAKING TIME STEPS*.

These time sub-steps are arranged in a geometrical progression, i.e. they are defined in the following way:

$$\delta_{i+1} = q \delta_i$$

where the geometrical ratio  $q$  is specified through the keyword: *COEFFICIENT OF THE TIME SUB-INCREMENTS FOR BREAKING*

In order to limit this number of time-steps, TOMAWAC first clips the wave height by setting a maximum  $H_{m0}/D$  ratio ( $D$  is the water depth) to 1. This ratio can be modified by means of the keyword *MAXIMUM VALUE OF THE RATIO  $H_{m0}$  TO  $D$* . However, this is generally not advisable.

#### 8.3.3.2. Wave breaking dissipation

If the integer keyword *DEPTH-INDUCED BREAKING DISSIPATION* is taken as 0, this source term will be ignored. If a strictly positive value (1, 2, ...) is chosen, the corresponding formulation will be taken into account.

Four formulations have been implemented (see section 4.2.3.5 for details):

#### **1: Battjes and Janssen's model (1978)**

This formulation requires additional data to be provided, specified by the following keywords:

*DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT ALPHA*

*DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA1*

*DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA2*

*DEPTH-INDUCED BREAKING 1 (BJ) CHARACTERISTIC FREQUENCY*

*DEPTH-INDUCED BREAKING 1 (BJ) QB COMPUTATION METHOD***2: Thornton and Guza's model (1983)**

This formulation requires additional data to be provided, specified by the following keywords:

*DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT B*  
*DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT GAMMA*  
*DEPTH-INDUCED BREAKING 2 (TG) WEIGHTING FUNCTION*  
*DEPTH-INDUCED BREAKING 2 (TG) CHARACTERISTIC FREQUENCY*

**3: Roelvink's model (1993)**

This formulation requires additional data to be provided, specified by the following keywords:

*DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT ALPHA*  
*DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA*  
*DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA2*  
*DEPTH-INDUCED BREAKING 3 (RO) WAVE HEIGHT DISTRIBUTION*  
*DEPTH-INDUCED BREAKING 3 (RO) EXPONENT WEIGHTING FUNCTION*  
*DEPTH-INDUCED BREAKING 3 (RO) CHARACTERISTIC FREQUENCY*

**4: Izumiya and Horikawa's model (1984)**

This formulation requires additional data to be provided, specified by the following keywords:

*DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT BETA0*  
*DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT M2STAR*  
*DEPTH-INDUCED BREAKING 4 (IH) CHARACTERISTIC FREQUENCY*

***8.3.3.3. Triad interactions***

If the integer keyword *TRIAD INTERACTIONS* is set to 0, this source term will be ignored. If a strictly positive value (1, 2, ...) is specified, the corresponding formulation will be taken into account.

Two formulations (see section 4.2.3.7) have been implemented.

**1: LTA model**

This formulation requires additional associated data to be specified using the following keywords:

*TRIADS 1 (LTA) COEFFICIENT ALPHA*  
*TRIADS 1 (LTA) COEFFICIENT RFMLTA*

**2: SPB model**

This formulation requires additional associated data to be specified using the following keywords:

*TRIADS 2 (SPB) COEFFICIENT K*  
*TRIADS 2 (SPB) LOWER DIRECTIONAL BOUNDARY*  
*TRIADS 2 (SPB) UPPER DIRECTIONAL BOUNDARY*

ATTENTION: the SPB model is very time-consuming; compared to the LTA model formulation, it requires a computational time approximately 700 times higher.

***8.4. Prescribing the initial conditions***

Initial conditions can be prescribed using the integer keyword *TYPE OF INITIAL DIRECTIONAL SPECTRUM* Table 8.1 shows all the available options in TOMAWAC for computing the frequency

and directional distribution of wave action. It should be remembered that the variance density directional spectrum is computed as the product:

$$F(f, \theta) = E(f) \cdot D(\theta)$$

where  $E(f)$  here denotes the variance density spectrum and  $D(\theta)$  denotes the angular distribution function.

It is reminded that the parameterised JONSWAP spectrum is defined as:

$$E(f) = \alpha_{phil} H_{mo}^2 \frac{f_p^4}{f^5} \exp \left[ -\frac{5}{4} \left( \frac{f_p}{f} \right)^4 \right] \gamma^{\exp \left[ -\frac{(f-f_p)^2}{2\sigma^2 f_p^2} \right]}$$

where:  $\sigma = \sigma_a$  for  $f < f_p$  and  $\sigma = \sigma_b$  for  $f > f_p$

$$\alpha_{phil} = \frac{0.0624}{0.23 + 0.0336\gamma - \frac{0.185}{1.9 + \gamma}}$$

and that the TMA spectrum is a depth-corrected JONSWAP-type spectrum.

A parameterised spectrum with two directional peaks can also be generated. In such case, both main propagation directions ( $\theta_1$  and  $\theta_2$ ) as well as the weighting factor ( $\lambda$ ) between the two power peaks:

$$D(\theta) = \frac{\lambda}{\Delta_1} \tilde{D}(\theta - \theta_1) + \frac{1-\lambda}{\Delta_2} \tilde{D}(\theta - \theta_2)$$

must be specified.

$\Delta_1$  and  $\Delta_2$ , in the equation above, are automatically computed by TOMAWAC in order to normalize the angular distribution function.

Three angular distribution functions may be chosen using the keyword *INITIAL ANGULAR FUNCTION DISTRIBUTION*, which correspond to the following options:

- 1: model in  $\cos^{2s}(\theta - \theta_0)$ ;  $\theta \in [\theta_0 - \pi/2; \theta_0 + \pi/2]$
- 2: model in  $\exp(-0.5((\theta - \theta_0)/s)^2)$ ;  $\theta \in [\theta_0 - \pi/2; \theta_0 + \pi/2]$
- 3: model in  $\cos^{2s}((\theta - \theta_0)/2)$ ;  $\theta \in [\theta_0 - \pi; \theta_0 + \pi]$  [Mitsuyasu et al., 1975]

with  $\theta_0$  being the main sea-state propagation direction and  $s$  being the directional spread.

The forementioned constants can be specified using the following of keywords:

$H_{m0}$ : *INITIAL SIGNIFICANT WAVE HEIGHT,*

$f_p$ : *INITIAL PEAK FREQUENCY,*

$\gamma$ : *INITIAL PEAK FACTOR,*

$\sigma_a$ : *INITIAL VALUE OF SIGMA-A FOR SPECTRUM,*

$\sigma_b$ : *INITIAL VALUE OF SIGMA-B FOR SPECTRUM,*

$\alpha_{phil}$ : *INITIAL PHILLIPS CONSTANT,*

Fetch: *INITIAL MEAN FETCH VALUE,*

$f_{pmax}$ : *INITIAL MAXIMUM PEAK FREQUENCY,*

$\theta_1$ : *INITIAL MAIN DIRECTION 1,*

$s_1$ : *INITIAL DIRECTIONAL SPREAD 1,*

$\theta_2$ : *INITIAL MAIN DIRECTION 2,*

$s_2$ : *INITIAL DIRECTIONAL SPREAD 2,*

$\lambda$ : *INITIAL WEIGHTING FACTOR FOR ADF,*

The keyword *SPECTRUM ENERGY THRESHOLD* is used whatever option is chosen. It is only useful for comparisons with the WAM model.

Specific initial conditions can be prescribed directly for the directional spectrum of wave action using the `condiw.f` subroutine which can be called from the `speini.f` subroutine.

### 8.5. Prescribing the boundary conditions

The boundary conditions are prescribed over the relative spectrum of wave action, i.e. expressed in co-ordinate system that moves with the current.

Only two kinds of boundary conditions are available in TOMAWAC.

The first one corresponds to a free boundary i.e. a boundary that fully absorbs the wave energy. It may be a liquid boundary: it is then assumed that the waves propagate beyond the domain and nothing else enters it. It may be a solid boundary: it is then assumed that the shore fully absorbs the wave energy.

The second one corresponds to a boundary with a prescribed value. In this case the wave action spectrum is then strictly imposed at each point along that boundary. This boundary condition allows wave energy to enter the computational domain.

The boundary conditions are specified using the boundary conditions (CONLIM) file, the steering (CAS) file and the `LIMWAC.f`.

#### 8.5.1. The boundary conditions file

The boundary condition (CONLIM) file is normally supplied by STBTEL (or other TELEMAT mesh generators), but it can also be generated by means of a text editor. Each line in this file is assigned to one point of the boundary and listed in sequential order in terms of the boundary node numbers. The numbering of the boundary points first delineates the domain contour in a counterclockwise direction, then the islands in the clockwise direction. The total number of edge points is noted as `NPTFR`.

13 values are given for each point. Only data in columns 1, 12 and 13 are used by TOMAWAC:

- The 13th data column (integer variable `IPTR`) corresponds to the boundary point number ranked in terms of the boundary point numbering.
- The 12th data column (integer variable `IPOIN`) corresponds to the global number of the point in the 2D mesh.

Lastly, the 1st data column (integer variable `LIFBOR`) corresponds to the kind of boundary condition. Consistent with TELEMAT-2D, its value is 2 (Variable `KSORT`=2) in the case of a free boundary and 5 (Variable `KENT`=5) in the case of a boundary with a prescribed value.

Key-word value		Spectrum	Constants being used
0		Zero spectrum	none
1	Wind $\neq 0$	- Frequencies: Jonswap according to wind - Directions: unimodal about the wind ( $\theta_1 = \theta_w$ )	$f_{pmax}$ , $\gamma$ , $\sigma_a\sigma_b$ , Fetch, $s_1$
	Wind = 0	Zero spectrum	none
2	Wind $\neq 0$	- Frequencies: Jonswap according to wind - Directions: unimodal about the wind ( $\theta_1 = \theta_w$ )	$f_{pmax}$ , $\gamma$ , $\sigma_a\sigma_b$ , Fetch, $s_1$
	Wind = 0	- Frequencies: parameterised Jonswap ( $\alpha$ , $f_p$ ) - Directions: parameterised unimodal (same spectrum at every point)	$\alpha_{phil}$ , $f_p$ , $\gamma$ , $\sigma_a\sigma_b$ , $s_1$ , $\theta_1$
3	Wind $\neq 0$	- Frequencies: parameterised Jonswap ( $\alpha$ ) - Directions: unimodal about the wind ( $\theta_1 = \theta_w$ )	$\alpha_{phil}$ , $f_p$ , $\gamma$ , $\sigma_a\sigma_b$ , $s_1$
	Wind = 0	Zero spectrum	none
4	Wind $\neq 0$	- Frequencies: parameterised Jonswap ( $\alpha$ , $f_p$ )	$\alpha_{phil}$ , $f_p$ , $\gamma$ , $\sigma_a\sigma_b$ , $s_1$ , $\theta_1$ , $s_2$ , $\theta_2$ , $\lambda$
	Wind = 0	- Directions: parameterised angular distribution function. Same spectrum at every point	
5	Wind $\neq 0$	- Frequencies: parameterised Jonswap ( $H_{m0}$ ) - Directions: unimodal about the wind ( $\theta_1 = \theta_w$ )	$H_{m0}$ , $f_p$ , $\gamma$ , $\sigma_a\sigma_b$ , $s_1$
	Wind = 0	Zero spectrum	none
6	Wind $\neq 0$	- Frequencies: parameterised Jonswap ( $H_{m0}$ , $f_p$ )	$H_{m0}$ , $f_p$ , $\gamma$ , $\sigma_a\sigma_b$ , $s_1$ , $\theta_1$ , $s_2$ , $\theta_2$ , $\lambda$
	Wind = 0	- Directions: parameterised angular distribution function. Same spectrum at every point	
7	Wind $\neq 0$	- Frequencies: parameterised TMA ( $H_{m0}$ , $f_p$ )	$H_{m0}$ , $f_p$ , $\gamma$ , $\sigma_a\sigma_b$ , $s_1$ , $\theta_1$ , $s_2$ , $\theta_2$ , $\lambda$
	Wind = 0	- Directions: parameterised angular distribution function. Same spectrum at every point	

Table 8.1: Summary table of the spectrum types as proposed in TOMAWAC

### 8.5.2. Prescribing the boundary conditions in the CAS file

Boundary conditions prescribed using the CAS file will necessarily be homogeneous all along the domain entry boundaries (KENT=5).

The boundary conditions can be prescribed by means of the integer keyword *TYPE OF BOUNDARY DIRECTIONAL SPECTRUM*

Table 8.1 (see section 8.4) presents all the spectrum types available in TOMAWAC. The constants given in Table 8.1 can be prescribed using the following keywords:

$H_{m0}$ : *BOUNDARY SIGNIFICANT WAVE HEIGHT*,  
 $f_p$ : *BOUNDARY PEAK FREQUENCY*,  
 $\gamma$ : *BOUNDARY PEAK FACTOR*,  
 $\sigma_a$ : *BOUNDARY SPECTRUM VALUE OF SIGMA-A*,  
 $\sigma_b$ : *BOUNDARY SPECTRUM VALUE OF SIGMA-B*,  
 $\alpha_{phil}$ : *BOUNDARY PHILLIPS CONSTANT*,  
Fetch: *BOUNDARY MEAN FETCH VALUE*,  
 $f_{pmax}$ : *BOUNDARY MAXIMUM PEAK FREQUENCY*,  
 $\theta_1$ : *BOUNDARY MAIN DIRECTION 1*,  
 $s_1$ : *BOUNDARY DIRECTIONAL SPREAD 1*,  
 $\theta_2$ : *BOUNDARY MAIN DIRECTION 2*,  
 $s_2$ : *BOUNDARY DIRECTIONAL SPREAD 2*,  
 $\lambda$ : *BOUNDARY WEIGHTING FACTOR FOR ADF*,

Three angular distribution functions have been implemented and can be selected using of the keyword: *BOUNDARY ANGULAR DISTRIBUTION FUNCTION*, which corresponds to the following options:

- 1: model in  $\cos^{2s}(\theta - \theta_0)$  ;  $\theta \in [\theta_0 - \pi/2 ; \theta_0 + \pi/2]$
- 2: model in  $\exp(-0.5((\theta - \theta_0)/s)^2)$  ;  $\theta \in [\theta_0 - \pi/2 ; \theta_0 + \pi/2]$
- 3: model in  $\cos^{2s}((\theta - \theta_0)/2)$  ;  $\theta \in [\theta_0 - \pi ; \theta_0 + \pi]$  [Mitsuyasu et al., 1975]

Since the boundary spectrum computation procedures are similar to those for the initial spectrum, refer to section 8.4 for further details.

### 8.5.3. The LIMWAC user subroutine

It should be reminded that the spectrum is discretized over both frequencies and directions and that it is a relative spectrum, i.e. expressed in a coordinate system that moves with the current.

The subroutine LIMWAC, in its original version, allows to impose the spectrum components at each point of a boundary with a prescribed value. The spectrum components are calculated from the parameters specified in the CAS file (see section 7.2.1). This subroutine, however, can easily be modified to specify e.g. non-homogeneous (in space) boundary conditions. When such specific boundary conditions are required, these will ideally be incorporated in the user part provided in the code of the LIMWAC procedure. The keyword *BOUNDARY SPECTRUM MODIFIED BY USER* must also be set to YES.

## 8.6. Some useful subroutines

### 8.6.1. Modification of bottom topography: CORFON subroutine

The seabed levels can be modified in two different ways, as already stated in section 7.5.

The seabed levels can be modified at the beginning of the computation using the CORFON subroutine, which is called once at the beginning of the computation. This subroutine allows the value of the ZF variable to be modified at each mesh point. For this purpose, a number of variables such as, for instance, the point coordinates, the element area values, the connectivity table, etc., are provided.

By default, the CORFON subroutine performs the same number of bottom smoothing iterations as LISFON, i.e. the same value as specified by the integer keyword *BOTTOM SMOOTHINGS*.

Note that the CORFON subroutine is not called in case the computation is initialized with the result of a former TOMAWAC run ("hot start").

This subroutine is part of the TELEMAC-2D library and is listed in APPENDIX 2.

### 8.6.2. Modifying the co-ordinates: CORRXY subroutine

TOMAWAC allows the mesh point co-ordinates to be modified at the beginning of the computation, so that an up-scaling (switching from a small scale model to a full-size model), a rotation or a translation can be performed.

Such changes are made using the CORRXY subroutine from the BIEF library, which is called in at the beginning of the computation. This subroutine is void by default and provides, in the form of a comment, an example of programming relevant to a change of scale and origin. It is part of the TELEMAC-2D library and is listed in APPENDIX 2.

### 8.6.3. Operations on vectors: OV subroutine

The BIEF library has a range of very useful subroutines including, in particular, subroutines for operations on vectors. A number of relations have been programmed so that loops can be replaced by a mere procedure call.

The syntax is as follows:

```
CALL OV(OP, X, Y, Z, C, NPOIN)
```

Where OP is a string of exactly 8 digits that is indicative of the operation about to be performed on the X, Y, Z vectors and the constant C. The result is the vector X.

Example:

```
CALL OV('X=X+Y ', X, Y, Z, C, NPOIN)
```

Y is added to X, the result will be stored in X.

A full list of available operations is given in the documentation of BIEF, which is part of the TELEMAC system.

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## APPENDIX 1: Launching a TOMAWAC computation at a workstation

A computation can be launched through the TOMAWAC control at a workstation.

That control activates the execution of an Unix script that is shared by all the computation modules in the TELEMAT processing chain.

That control's syntax is as follows:

`TOMAWAC [-s] [-D] [-b| -n| -d heure] [cas]`

- s: if the program is launched in an interactive mode the check listing is stored on the disk (by default, the check listing is only displayed on the screen).
  - D: compilation and execution mode under debugger.
  - b: batch launching (immediate start)
  - n: night batch launching (start at 8.00 p.m.)
  - d: delayed batch start (start at the specified time)
- cas: steering file name.

When the steering file name is not specified, the procedure uses the name 'cas'. By default, the procedure performs the computation in an interactive mode.

Examples:

- TOMAWAC: immediately launches a computation in a interactive mode by reading the steering file cas. The listings are displayed on the screen.
- TOMAWAC -b test2: start computation immediately in batch mode using the test2 steering file.
- TOMAWAC -d 22:00 modtot launches a computation in a batch mode at 10.00 p.m. on the very night by reading the steering file modtot.
- telemac2d -n: start computation at 20:00 the same evening in batch mode using the cas steering file.

The main operations performed by that script are as follows:

- Creation of a temporary directory,
- Duplication of the dictionary and the steering file in that directory,
- Execution of the DAMOCLES software in order to determine the work files names,
- Creation of the computation launching script,
- Allocation of the files,
- Compilation of the FORTRAN file and link edit,
- Computation launching,
- Retrieval of the results files and deletion of the temporary directory.

The procedure operation differs slightly according to the selected options.

A detailed description of this procedure may be obtained by using the command `TOMAWAC -H`.

## **APPENDIX 2: List of useful subroutines**

The following subroutines can be modified by the user:

- `ANACOS.f` : Specification of an analytical stationary current.
- `ANAMAR.f` : Specification of an analytical tide (current and water level).
- `ANAVEN.f` : Specification of an analytical wind.
- `CORFON.f` : Modification of bottom topography.
- `CORRXY.f` : Modification of coordinates.
- `COUUTI.f` : Currents file reading from a user-defined format.
- `LIMWAC.f` : Specification of the boundary conditions.
- `MARUTI.f` : Tide level file reading from a user-defined format.
- `VARTEL.f` : Processing of a TELEMAC data.
- `VENUTI.f` : Winds file reading from a user-defined format.

When these subroutines are used, they should be integrated into the user's FORTRAN file, then modified.

## APPENDIX 3: Alphabetical list of keywords

### 2D RESULTS FILE

Type:	Character
Dimension:	1
Default value:	'resu2d'
FORTRAN variable:	WAC_FILES(WACRES)%NAME
French translation:	FICHER DES RESULTATS 2D

Name of the file to which the results of the two-dimensional computation will be written.

Associated keywords: 2D RESULTS FILE BINARY  
 VARIABLES FOR 2D GRAPHIC PRINTOUTS  
 PERIOD FOR GRAPHIC PRINTOUTS  
 NUMBER OF FIRST ITERATION FOR GRAPHIC PRINTOUTS

### 2D RESULTS FILE BINARY

Type:	Character
Dimension:	1
Default value:	'STD'
FORTRAN variable:	BINRES
French translation:	BINAIRE DU FICHER DES RESULTATS 2D

Type of the binary used for writing the 2D results file. That type depends on the machine in which the file was generated. The possible values are as follows:

- IBM; for a file created in an IBM machine;
- I3E; for a file created in a HP machine;
- STD; normal READ and WRITE instructions are then generated.

Associated keywords: 2D RESULTS FILE

### ABSCISSAE OF SPECTRUM PRINTOUT POINTS

Type:	Real
Dimension:	Variable
Default value:	0.;0.;0.;0.;0.;0.;0.;0.;0.
FORTRAN variable:	XLEO
French translation:	ABSCISSES DES POINTS DE SORTIE DU SPECTRE

Array providing the abscissa of the SERAFIN spectrum printout points with a maximum dimension of 10.

The chosen spectrum points are the closest 2D points to the specified co-ordinates.

Associated keywords: ORDINATES OF SPECTRUM PRINTOUT POINTS  
 PUNCTUAL RESULTS FILE

## AIR DENSITY

Type: Real  
 Dimension: 1  
 Default value: 1.225  
 FORTRAN variable: ROAIR  
 French translation: DENSITE DE LAIR

The ratio ROAIR/ROEAU is used in the wind generation

Associated keywords: WIND GENERATION  
 WATER DENSITY

## BINARY CURRENTS FILE

Type: Character  
 Dimension: 1  
 Default value: ''  
 FORTRAN variable: WAC\_FILES(WACCOB)%NAME  
 French translation: FICHIER DES COURANTS BINAIRE

Name of the current data file (if binary).

Associated keywords: CONSIDERATION OF A STATIONARY CURRENT  
 CONSIDERATION OF TIDE  
 FORMATTED CURRENTS FILE  
 CURRENTS FILE FORMAT

## BINARY DATA FILE 1 FORMAT

Type: Character  
 Dimension: 1  
 Default value: 'SERAFIN'  
 FORTRAN variable: 'WAC\_FILES(WACBI1)%FMT'  
 French translation: FORMAT DU FICHIER DE DONNEES BINAIRE 1

Possible values are:

- SERAFIN: classical single precision format in Telemac;
- SERAFIND: classical double precision format in Telemac;
- MED : MED format based on HDF5

## BINARY FILE 1

Type: Character  
 Dimension: 1

Default value:            ‘ ‘  
 FORTRAN variable:        WAC\_FILES(WACBI1)%NAME  
 French translation:       FICHER BINAIRE 1

Binary-coded data file made available to the user.

Associated keywords:    CONSIDERATION OF A STATIONARY CURRENT  
                                  CONSIDERATION OF TIDE  
                                  FORMATTED CURRENTS FILE  
                                  CURRENTS FILE FORMAT

#### BINARY FILE 1 BINARY

Type:                        Character  
 Dimension:                1  
 Default value:            ‘STD’  
 FORTRAN variable:        BINBI1  
 French translation:       BINAIRE DU FICHER BINAIRE 1

Type of the binary used for writing the binary file1. This type depends on the machine in which the file was generated. The possible values are the same as for the geometry file.

Associated keywords:    BINARY FILE 1

#### BINARY TIDAL WATER LEVEL FILE

Type:                        Character  
 Dimension:                1  
 Default value:            ‘ ‘  
 FORTRAN variable:        WAC\_FILES(WACMAB)%NAME  
 French translation:       FICHER DU NIVEAU DE LA MAREE BINAIRE

Name of the water level data file (if binary).

Associated keywords:    CONSIDERATION OF TIDE  
                                  FORMATTED TIDAL WATER LEVEL FILE  
                                  TIDAL WATER LEVEL FILE FORMAT  
                                  TIDE REFRESHING PERIOD  
                                  TIDAL WATER LEVEL FILE BINARY

#### BINARY WINDS FILE

Type:                        Character  
 Dimension:                1  
 Default value:            ‘ ‘  
 FORTRAN variable:        WAC\_FILES(WACVEB)%NAME

French translation: FICHER DES VENTS BINAIRE

Name of wind data file (if binary).

Associated keywords: CONSIDERATION OF WIND  
FORMATTED WINDS FILE  
WINDS FILE FORMAT

#### BOTTOM FRICTION COEFFICIENT

Type: Real  
Dimension: 1  
Default value: 0.038  
FORTRAN variable: CFROT1  
French translation: COEFFICIENT DE FROTTEMENT SUR LE FOND

Bottom friction coefficient.

Associated keywords: INFINITE DEPTH  
BOTTOM FRICTION-INDUCED DISSIPATION

#### BOTTOM FRICTION DISSIPATION

Type: INTEGER  
Dimension: 1  
Default value: 0  
FORTRAN variable: SFROT  
French translation: DISSIPATION PAR FROTTEMENT SUR LE FOND

Selection of the modelling type of the bottom friction source term. If its value is 0, the bottom friction dissipation is ignored; if its value is 1, it is integrated in accordance with a formula that is similar to that of WAM cycle 4.

Associated keywords: INFINITE DEPTH  
BOTTOM FRICTION COEFFICIENT

#### BOTTOM SMOOTHINGS

Type: INTEGER  
Dimension: 1  
Default value: 0  
FORTRAN variable: LISFON  
French translation: LISSAGES DU FOND

Number of smoothings made on bottom features. Each smoothing, being made by means of a mass matrix, is conservative. To be used when the bathymetric data yield too irregular data after interpolation. Also refer to the CORFON subroutine.

## BOTTOM TOPOGRAPHY FILE

Type: Character  
 Dimension: 1  
 Default value: ''  
 FORTRAN variable: WAC\_FILES(WACFON)%NAME  
 French translation: FICHER DES FONDS

Name of any file containing the bathymetric data associated to the SINUSX-formatted grid. If this keyword is used, these bathymetric data shall be used for the computation.

## BOUNDARY ANGULAR DISTRIBUTION FUNCTION

Type: INTEGER  
 Dimension: 1  
 Default value: 1  
 FORTRAN variable: FRABL  
 French translation: FONCTION DE REPARTITION ANGULAIRE AUX LIMITES

This is one of the constants used for computing the boundary directional spectrum. The following angular distribution functions are allowed:

- 1:  $\cos^2 s(T-T_0)$  ; T in range  $[T_0-\pi/2; T_0+\pi/2]$
- 2:  $\exp(-0.5((T-T_0)/s)^2)$  ; T in range  $[T_0-\pi/2; T_0+\pi/2]$
- 3:  $\cos^2 s((T-T_0)/2)$  (Mitsuyasu type)

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

## BOUNDARY CONDITIONS FILE

Type: Character  
 Dimension: 1  
 Default value: dynam  
 FORTRAN variable: WAC\_FILES(WACCLI)%NAME  
 French translation: FICHER DES CONDITIONS AUX LIMITES

Name of the file containing the boundary conditions types.

## BOUNDARY DIRECTIONAL SPREAD 1

Type: Real  
 Dimension: 1  
 Default value: 2.  
 FORTRAN variable: SPRE1L  
 French translation: ETALEMENT DIRECTIONNEL 1 AUX LIMITES



This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

#### BOUNDARY DIRECTIONAL SPREAD 2

Type: Real  
 Dimension: 1  
 Default value: 2.  
 FORTRAN variable: SPRE2L  
 French translation: ETALEMENT DIRECTIONNEL 2 AUX LIMITES

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

#### BOUNDARY MAIN DIRECTION 1

Type: Real  
 Dimension: 1  
 Default value: 0.  
 FORTRAN variable: TETA1L  
 French translation: DIRECTION PRINCIPALE 1 AUX LIMITES

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

#### BOUNDARY MAIN DIRECTION 2

Type: Real  
 Dimension: 1  
 Default value: 0.  
 FORTRAN variable: TETA2L  
 French translation: DIRECTION PRINCIPALE 2 AUX LIMITES

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

#### BOUNDARY MAXIMUM PEAK FREQUENCY

Type: Real  
 Dimension: 1

Default value: 0.2  
FORTRAN variable: FPMAXL  
French translation: FREQUENCE DE PIC MAXIMALE AUX LIMITES

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

#### BOUNDARY MEAN FETCH VALUE

Type: Real  
Dimension: 1  
Default value: 30000.  
FORTRAN variable: FETCHL  
French translation: VALEUR MOYENNE DU FETCH AUX LIMITES

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

#### BOUNDARY PEAK FACTOR

Type: Real  
Dimension: 1  
Default value: 3.3  
FORTRAN variable: GAMMAL  
French translation: FACTEUR DE PIC AUX LIMITES

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

#### BOUNDARY PEAK FREQUENCY

Type: Real  
Dimension: 1  
Default value: 0.067  
FORTRAN variable: FPICL  
French translation: FREQUENCE DE PIC AUX LIMITES

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

**BOUNDARY PHILLIPS CONSTANT**

Type:	Real
Dimension:	1
Default value:	0.018
FORTTRAN variable:	APHILL
French translation:	CONSTANTE DE PHILLIPS AUX LIMITES

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

**BOUNDARY SIGNIFICANT WAVE HEIGHT**

Type:	Real
Dimension:	1
Default value:	1.
FORTTRAN variable:	HM0L
French translation:	HAUTEUR SIGNIFICATIVE AUX LIMITES

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

**BOUNDARY SPECTRUM VALUE OF SIGMA-A**

Type:	Real
Dimension:	1
Default value:	0.07
FORTTRAN variable:	SIGMAL
French translation:	VALEUR AUX LIMITES DE SIGMA-A POUR SPECTRE

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

**BOUNDARY SPECTRUM VALUE OF SIGMA-B**

Type:	Real
Dimension:	1
Default value:	0.09
FORTTRAN variable:	SIGMBL
French translation:	VALEUR AUX LIMITES DE SIGMA-B POUR SPECTRE

This is one of the constants used for computing the boundary directional spectrum as a function of the wind

field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

#### BOUNDARY WEIGHTING FACTOR FOR ADF

Type: Real  
Dimension: 1  
Default value: 1.  
FORTRAN variable: XLAMD  
French translation: FACTEUR DE PONDERATION POUR FRA AUX LIMITES

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

#### CHARNOCK CONSTANT

Type: Real  
Dimension: 1  
Default value: 0.01  
FORTRAN variable: ALPHA  
French translation: CONSTANCE DE CHARNOK

Constant used in the wind source term.

Associated keywords: WIND GENERATION

#### COEFFICIENT OF THE TIME SUB-INCREMENTS FOR BREAKING

Type: Real  
Dimension: 1  
Default value: 1.45  
FORTRAN variable: XDTBRK  
French translation: COEFFICIENT POUR LES SOUS-PAS DE TEMPS POUR LE DEFERLEMENT

Geometrical ratio of the time sub-increments for the depth-induced breaking

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
NUMBER OF BREAKING TIME STEPS

#### CONSIDERATION OF A STATIONARY CURRENT

Type: LOGICAL  
Dimension: 1  
Default value: .FALSE.

FORTTRAN variable: COUSTA

French translation: PRISE EN COMPTE D'UN COURANT STATIONNAIRE

It indicates whether a stationary current is taken into account, either in a file or in condw.f.

Associated keywords: CURRENTS FILE FORMAT

#### CONSIDERATION OF A WIND

Type: LOGICAL

Dimension: 1

Default value: FALSE.

FORTTRAN variable: VENT

French translation: PRISE EN COMPTE DU VENT

It indicates whether a wind is taken into account, either in a file or in anaven.f.

Associated keywords: WINDS FILE FORMAT

#### CONSIDERATION OF PROPAGATION

Type: LOGICAL

Dimension: 1

Default value: .TRUE.

FORTTRAN variable: PROP

French translation: PRISE EN COMPTE DE LA PROPAGATION

It indicates whether propagation is taken into account.

#### CONSIDERATION OF SOURCE TERMS

Type: LOGICAL

Dimension: 1

Default value: .FALSE.

FORTTRAN variable: TSOU

French translation: PRISE EN COMPTE DES TERMES SOURCES

It indicates whether the source terms are taken into account or not.

Associated keywords: WIND GENERATION

BOTTOM FRICTION DISSIPATION

WHITE CAPPING DISSIPATION

DEPTH-INDUCED BREAKING DISSIPATION

NON-LINEAR TRANSFERTS BETWEEN FREQUENCIES

TRIAD INTERACTION

#### CONSIDERATION OF TIDE

Type: LOGICAL

Dimension: 1  
 Default value: .FALSE.  
 FORTRAN variable: MAREE  
 French translation: PRISE EN COMPTE DE LA MAREE

Indicates whether a current is taken into account, either in a file or in maruti.f.

Associated keywords: FORMATTED TIDAL WATER LEVEL FILE  
 BINARY TIDAL WATER LEVEL FILE  
 TIDAL WATER LEVEL FILE FORMAT  
 TIDE REFRESHING PERIOD  
 TIDAL WATER LEVEL FILE BINARY

#### CURRENTS FILE BINARY

Type: Character  
 Dimension: 1  
 Default value: 'STD'  
 FORTRAN variable: BINCOU  
 French translation: BINAIRE DU FICHIER DES COURANTS

Type of the binary used for writing the currents file. This type depends on the machine in which the file was generated. The possible values are as follows:

- IBM; for a file created in an IBM machine;
- I3E; for a file created in a HP machine;
- STD; normal READ and WRITE instructions are then generated.

Associated keywords: BINARY CURRENTS FILE  
 FORMATTED CURRENTS FILE  
 CURRENTS FILE FORMAT

#### CURRENTS FILE FORMAT

Type: INTEGER  
 Dimension: 1  
 Default value: 1  
 FORTRAN variable: INDIC  
 French translation: FORMAT DU FICHIER DES COURANTS

Selection of the type of currents file format:

- 1 finite differences, WAM cycle 4 format type
- 2 X Y UX UY, SINUSX format type
- 3 SERAFIN, TELEMAC type
- 4 user format (the couuti.f procedure should then be modified)

Associated keywords: CURRENTS BINARY FILE

## CURRENTS FORMATTED FILE

## CURRENTS FILE BINARY

## DATE OF COMPUTATION BEGINNING

Type:	Real
Dimension:	1
Default value:	0
FORTTRAN variable:	DDC
French translation:	DATE DE DEBUT DU CALCUL

This gives the start date of the computation. The format is yymmddhhmm, for example 9310241524 means the 24 October 93 at 15h24. This date gives a reference for the reading of the wind file.

Associated keywords:	BINARY WIND FILE
	FORMATTED WIND FILE
	WIND FILE BINARY
	WIND FILE FORMAT

## DEFAULT EXECUTABLE

Type:	Character
Dimension:	1
Default value:	TOMAWAC towa_VVV PPP TOMAWACMMMVVV.exe
FORTTRAN variable:	EXEDEF
French translation:	EXECUTABLE PAR DEFAULT

Default executable file name for TOMAWAC

## DEFAULT PARALLEL EXECUTABLE

Type:	Character
Dimension:	1
Default value:	TOMAWAC towa_VVV PPP TOMAWACMMMVVV_MP.exe
FORTTRAN variable:	EXEDEF PARA
French translation:	EXECUTABLE PARALLELE PAR DEFAULT

Default parallel executable file name for TOMAWAC

## DEPTH-INDUCED BREAKING 1 (BJ) CHARACTERISTIC FREQUENCY

Type:	INTEGER
Dimension:	1
Default value:	2
FORTTRAN variable:	IFRBJ

French translation: DEFERLEMENT 1 (BJ) CHOIX FREQUENCE CARACTERISTIQUE

Selection of the characteristic frequency of the wave spectrum:

- 1: Frequency Fmoy
- 2: Frequency F01 (defined by the 0th and 1<sup>st</sup> moments of the spectrum)
- 3: Frequency F02 (defined by the 0th and 2<sup>nd</sup> moments of the spectrum)
- 4: Frequency Fpic (sampling frequency corresponding to the max)
- 5: Frequency Fread order 5 (peak frequency, 5th order Read method)
- 6: Frequency Fread order 8 (peak frequency, 8th order Read method)

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
DEPTH-INDUCED BREAKING 1 (BJ) QB COMPUTATION METHOD  
DEPTH-INDUCED BREAKING 1 (BJ) HM COMPUTATION METHOD  
DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT ALPHA  
DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA1  
DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA2

#### DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT ALPHA

Type: Real  
Dimension: 1  
Default value: 1.  
FORTRAN variable: ALFABJ  
French translation: DEFERLEMENT 1 (BJ) CONSTANCE ALPHA

ALPHA constant for the Battjes and Janssen model.

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
NUMBER OF BREAKING TIME STEPS  
DEFERLEMENT 1 (BJ) MODE DE CALCUL DE QB  
DEFERLEMENT 1 (BJ) MODE DE CALCUL DE HM  
DEFERLEMENT 1 (BJ) CHOIX FREQUENCE CARACTERISTIQUE  
DEFERLEMENT 1 (BJ) CONSTANCE GAMMA1  
DEFERLEMENT 1 (BJ) CONSTANCE GAMMA2

#### DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA1

Type: Real  
Dimension: 1  
Default value: 0.88  
FORTRAN variable: GAMBJ1  
French translation: DEFERLEMENT 1 (BJ) CONSTANCE GAMMA1

GAMMA1 constant of the Battjes and Janssen model.

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION



## NUMBER OF BREAKING TIME STEPS

DEFERLEMENT 1 (BJ) MODE DE CALCUL DE QB

DEFERLEMENT 1 (BJ) MODE DE CALCUL DE HM

DEFERLEMENT 1 (BJ) CHOIX FREQUENCE CARACTERISTIQUE

DEFERLEMENT 1 (BJ) CONSTANTE ALPHA

DEFERLEMENT 1 (BJ) CONSTANTE GAMMA2

## DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA2

Type: Real

Dimension: 1

Default value: 0.8

FORTRAN variable: GAMBJ2

French translation: DEFERLEMENT 1 (BJ) CONSTANTE GAMMA2

GAMMA1 constant of the Battjes and Janssen model.

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION

NUMBER OF BREAKING TIME STEPS

DEFERLEMENT 1 (BJ) MODE DE CALCUL DE QB

DEFERLEMENT 1 (BJ) MODE DE CALCUL DE HM

DEFERLEMENT 1 (BJ) CHOIX FREQUENCE CARACTERISTIQUE

DEFERLEMENT 1 (BJ) CONSTANTE ALPHA

DEFERLEMENT 1 (BJ) CONSTANTE GAMMA1

## DEPTH-INDUCED BREAKING 1 (BJ) HM COMPUTATION METHOD

Type: INTEGER

Dimension: 1

Default value: 1

FORTRAN variable: IHMBJ

French translation: DEFERLEMENT 1 (BJ) MODE DE CALCUL DE HM

Selection of the depth-induced breaking criterium giving the breaking wave height:

1:  $H_m \text{ GAMMA} \cdot D$  ;2:  $H_m$  given the Miche criterium.

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION

DEPTH-INDUCED BREAKING 1 (BJ) CHARACTERISTIC

FREQUENCY

DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA1

DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA2

## DEPTH-INDUCED BREAKING 1 (BJ) QB COMPUTATION METHOD

Type: INTEGER  
Dimension: 1  
Default value: 2  
FORTRAN variable: IQBBJ  
French translation: DEFERLEMENT 1 (BJ) MODE DE CALCUL DE QB

Selection of the method for the resolution of the implicit equation for QB.

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
DEPTH-INDUCED BREAKING 1 (BJ) HM COMPUTATION METHOD  
DEPTH-INDUCED BREAKING 1 (BJ) CHARACTERISTIC  
FREQUENCY  
DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT ALPHA  
DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA1  
DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA2

#### DEPTH-INDUCED BREAKING 2 (TG) CHARACTERISTIC FREQUENCY

Type: INTEGER  
Dimension: 1  
Default value: 5  
FORTRAN variable: IFRTG  
French translation: DEFERLEMENT 2 (TG) CHOIX FREQUENCE CARACTERISTIQUE

Selection of the characteristic frequency of the wave spectrum

- 1: Frequency Fmoy
- 2: Frequency F01 (defined by the 0th and 1<sup>st</sup> moments of the spectrum)
- 3: Frequency F02 (defined by the 0th and 2<sup>nd</sup> moments of the spectrum)
- 4: Frequency Fpic (sampling frequency corresponding to the max)
- 5: Frequency Fread order 5 (peak frequency, 5th order Read method)
- 6: Frequency Fread order 8 (peak frequency, 8th order Read method)

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
DEPTH-INDUCED BREAKING 2 (TG) WEIGHTING FUNCTION  
DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT B  
DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT GAMMA

#### DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT B

Type: Real  
Dimension: 1  
Default value: 1.0  
FORTRAN variable: BORETG  
French translation: DEFERLEMENT 2 (TG) CONSTANCE B

Coefficient B of the Thornton and Guza model.

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
NUMBER OF BREAKING TIME STEPS  
DEPTH-INDUCED BREAKING 2 (TG) WEIGHTING FUNCTION  
DEPTH-INDUCED BREAKING 2 (TG) CHARACTERISTIC  
FREQUENCY  
DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT GAMMA

DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT GAMMA

Type: Real  
Dimension: 1  
Default value: 0.42  
FORTRAN variable: GAMATG  
French translation: DEFERLEMENT 2 (TG) CONSTANCE GAMMA

Coefficient GAMMA of the Thornton and Guza model.

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
NUMBER OF BREAKING TIME STEPS  
DEPTH-INDUCED BREAKING 2 (TG) WEIGHTING FUNCTION  
DEPTH-INDUCED BREAKING 2 (TG) CHARACTERISTIC  
FREQUENCY  
DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT B

DEPTH-INDUCED BREAKING 2 (TG) WEIGHTING FUNCTION

Type: INTEGER  
Dimension: 1  
Default value: 2  
FORTRAN variable: IWHTG  
French translation: DEFERLEMENT 2 (TG) FONCTION DE PONDERATION

Selection of the expression for the weighting function based on a probability distribution of the wave heights.

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
DEPTH-INDUCED BREAKING 2 (TG) CHARACTERISTIC  
FREQUENCY  
DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT B  
DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT GAMMA

DEPTH-INDUCED BREAKING 3 (RO) CHARACTERISTIC FREQUENCY

Type: INTEGER

Dimension: 1  
 Default value: 5  
 FORTRAN variable: IFRRO  
 French translation: DEFERLEMENT 3 (RO) CHOIX FREQUENCE CARACTERISTIQUE

Selection of the characteristic frequency of the wave spectrum

- 1: Frequency Fmoy
- 2: Frequency F01 (defined by the 0th and 1<sup>st</sup> moments of the spectrum)
- 3: Frequency F02 (defined by the 0th and 2<sup>nd</sup> moments of the spectrum)
- 4: Frequency Fpic (sampling frequency corresponding to the max)
- 5: Frequency Fread order 5 (peak frequency, 5th order Read method)
- 6: Frequency Fread order 8 (peak frequency, 8th order Read method)

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
 DEPTH-INDUCED BREAKING 3 (RO) WAVE HEIGHT DISTRIBUTION  
 DEPTH-INDUCED BREAKING 3 (RO) EXPONENT WEIGHTING  
 FUNCTION  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT ALPHA  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA2

DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT ALPHA

Type: Real  
 Dimension: 1  
 Default value: 1.  
 FORTRAN variable: ALFARO  
 French translation: DEFERLEMENT 3 (RO) CONSTANCE ALPHA

Coefficient ALPHA of the Roelvink model (1993).

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
 NUMBER OF BREAKING TIME STEPS  
 DEPTH-INDUCED BREAKING 3 (RO) WAVE HEIGHT DISTRIBUTION  
 DEPTH-INDUCED BREAKING 3 (RO) EXPONENT WEIGHTING  
 FUNCTION  
 DEPTH-INDUCED BREAKING 3 (RO) CHARACTERISTIC  
 FREQUENCY  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA2

DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA

Type: Real

Dimension: 1  
 Default value: 0.54  
 FORTRAN variable: GAMARO  
 French translation: DEFERLEMENT 3 (RO) CONSTATE GAMMA

Coefficient GAMMA of the Roelvink model (1993).

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
 NUMBER OF BREAKING TIME STEPS  
 DEPTH-INDUCED BREAKING 3 (RO) WAVE HEIGHT DISTRIBUTION  
 DEPTH-INDUCED BREAKING 3 (RO) EXPONENT WEIGHTING  
 FUNCTION  
 DEPTH-INDUCED BREAKING 3 (RO) CHARACTERISTIC  
 FREQUENCY  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT ALPHA  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA2

#### DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA2

Type: Real  
 Dimension: 1  
 Default value: 0.65  
 FORTRAN variable: GAM2RO  
 French translation: DEFERLEMENT 3 (RO) CONSTATE GAMMA2

Coefficient GAMMA2 of the Roelvink model (1993).

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
 NUMBER OF BREAKING TIME STEPS  
 DEPTH-INDUCED BREAKING 3 (RO) WAVE HEIGHT DISTRIBUTION  
 DEPTH-INDUCED BREAKING 3 (RO) EXPONENT WEIGHTING  
 FUNCTION  
 DEPTH-INDUCED BREAKING 3 (RO) CHARACTERISTIC  
 FREQUENCY  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT ALPHA  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA

#### DEPTH-INDUCED BREAKING 3 (RO) EXPONENT WEIGHTING FUNCTION

Type: INTEGER  
 Dimension: 1  
 Default value: 10  
 FORTRAN variable: IEXPRO  
 French translation: DEFERLEMENT 3 (RO) EXPOSANT FONCTION DE PONDERATION

$n$  exponent of the weighting function used in the Roelvink breaking model.

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
 DEPTH-INDUCED BREAKING 3 (RO) WAVE HEIGHT DISTRIBUTION  
 DEPTH-INDUCED BREAKING 3 (RO) CHARACTERISTIC  
 FREQUENCY  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT ALPHA  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA2

#### DEPTH-INDUCED BREAKING 3 (RO) WAVE HEIGHT DISTRIBUTION

Type: INTEGER  
 Dimension: 1  
 Default value: 1  
 FORTRAN variable: IDISRO  
 French translation: DEFERLEMENT 3 (RO) DISTRIBUTION DES HAUTEURS DE HOULE

Selection of the wave height distribution for the Roelvink breaking model:

- 1...Weibull,
- 2...Rayleigh.

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
 DEPTH-INDUCED BREAKING 3 (RO) EXPONENT WEIGHTING  
 FUNCTION  
 DEPTH-INDUCED BREAKING 3 (RO) CHARACTERISTIC  
 FREQUENCY  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT ALPHA  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA  
 DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA2

#### DEPTH-INDUCED BREAKING 4 (IH) CHARACTERISTIC FREQUENCY

Type: INTEGER  
 Dimension: 1  
 Default value: 5  
 FORTRAN variable: IFRIH  
 French translation: DEFERLEMENT 4 (IH) CHOIX FREQUENCE CARACTERISTIQUE

Selection of the characteristic frequency of the wave spectrum

- 1: Frequency  $F_{moy}$
- 2: Frequency  $F_{01}$  (defined by the 0th and 1<sup>st</sup> moments of the spectrum)
- 3: Frequency  $F_{02}$  (defined by the 0th and 2<sup>nd</sup> moments of the spectrum)
- 4: Frequency  $F_{pic}$  (sampling frequency corresponding to the max)

5: Frequency Fread order 5 (peak frequency, 5th order Read method)

6: Frequency Fread order 8 (peak frequency, 8th order Read method)

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT BETA0  
DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT M2STAR

#### DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT BETA0

Type: Real  
Dimension: 1  
Default value: 1.8  
FORTRAN variable: BETAIH  
French translation: DEFERLEMENT 4 (IH) CONSTANCE BETA0

Coefficient BETA0 of the Izumiya and Horikawa model (1984).

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
NUMBER OF BREAKING TIME STEPS  
DEPTH-INDUCED BREAKING 4 (IH) CHARACTERISTIC FREQUENCY  
DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT M2STAR

#### DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT M2STAR

Type: Real  
Dimension: 1  
Default value: 0.009  
FORTRAN variable: EM2SIH  
French translation: DEFERLEMENT 4 (IH) CONSTANCE M2STAR

Coefficient M2STAR of the Izumiya and Horikawa model (1984).

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
NUMBER OF BREAKING TIME STEPS  
DEPTH-INDUCED BREAKING 4 (IH) CHARACTERISTIC FREQUENCY  
DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT BETA0

#### DEPTH-INDUCED BREAKING DISSIPATION

Type: INTEGER  
Dimension: 1  
Default value: 0  
FORTRAN variable: SBREK  
French translation: DISSIPATION PAR DEFERLEMENT

Selection of the modelling type of the bathymetric-induced breaking dissipation source term:

- 0: Breaking is ignored.
- 1: Battjes and Janssen model (1978).
- 2: Thornton and Guza model (1983)
- 3: Roelvink model (1993)(
- 4: Izumiya and Horikawa model (1984).

Associated keywords:

NUMBER OF BREAKING TIME STEPS

DEPTH-INDUCED BREAKING 1 (BJ) QB COMPUTATION METHOD

DEPTH-INDUCED BREAKING 1 (BJ) HM COMPUTATION METHOD

DEPTH-INDUCED BREAKING 1 (BJ) CHARACTERISTIC FREQUENCY

DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT ALPHA

DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA1

DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA2

DEPTH-INDUCED BREAKING 2 (TG) WEIGHTING FUNCTION

DEPTH-INDUCED BREAKING 2 (TG) CHARACTERISTIC FREQUENCY

DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT B

DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT GAMMA

DEPTH-INDUCED BREAKING 3 (RO) WAVE HEIGHT DISTRIBUTION

DEPTH-INDUCED BREAKING 3 (RO) EXPONENT WEIGHTING FUNCTION

DEPTH-INDUCED BREAKING 3 (RO) CHARACTERISTIC FREQUENCY

DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT ALPHA

DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA

DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA2

DEPTH-INDUCED BREAKING 4 (IH) CHARACTERISTIC FREQUENCY

DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT BETA0

DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT M2STAR

#### DESCRIPTION OF LIBRARIES

Type: Character

Dimension: 5

Default value: 'TOMAWAC|toma\_VVV|PPP|TOMAWACMMMVVV.LLL';  
'bief|bief\_VVV|PPP|biefMMMVVV.LLL';  
'damocles|damo\_VVV|PPP|damoMMMVVV.LLL';  
'paravoid|paravoid\_VVV|PPP|paravoidMMMVVV.LLL';  
'special|special\_VVV|PPP|specialMMMVVV.LLL'



FORTRAN variable: LINKLIBS  
 French translation: DESCRIPTION DES LIBRAIRIES

TOMAWAC LIBRARIES description

#### DICTIONARY

Type: Character  
 Dimension: 1  
 Default value: 'TOMAWACv6p0.dico'  
 FORTRAN variable:  
 French translation: DICTIONNAIRE

Key word dictionary.

#### FORMATTED CURRENTS FILE

Type: Character  
 Dimension: 1  
 Default value: ''  
 FORTRAN variable: WAC\_FILES(WACCOF)%NAME  
 French translation: FICHIER DES COURANTS FORMATE

Name of the current data file (if formatted).

Associated keywords: CONSIDERATION OF A STATIONARY CURRENT  
 CONSIDERATION OF TIDE  
 BINARY CURRENTS FILE  
 CURRENTS FILE FORMAT

#### FORMATTED FILE 1

Type: Character  
 Dimension: 1  
 Default value: ''  
 FORTRAN variable: WAC\_FILES(WACFO1)%NAME  
 French translation: FICHIER FORMATE 1

Formatted data file made available to the user.

#### FORMATTED TIDAL WATER LEVEL FILE

Type: Character  
 Dimension: 1  
 Default value: ''  
 FORTRAN variable: WAC\_FILES(WACMAF)%NAME

French translation: FICHIER DU NIVEAU DE LA MAREE FORMATE

Name of the current data file (if formatted).

Associated keywords: CONSIDERATION OF TIDE  
BINARY TIDAL WATER LEVEL FILE  
TIDAL WATER LEVEL FILE FORMAT  
TIDE REFRESHING PERIOD  
TIDAL WATER LEVEL FILE BINARY

#### FORMATTED WINDS FILE

Type: Character  
Dimension: 1  
Default value: ''  
FORTRAN variable: WAC\_FILES(WACVEF)%NAME  
French translation: FICHIER DES VENTS FORMATE

Name of wind data file (if formatted).

Associated keywords: CONSIDERATION OF WIND  
BINARY WINDS FILE  
WINDS FILE FORMAT

#### FORTRAN FILE

Type: Character  
Dimension: 1  
Default value: 'DEFAUT1'  
FORTRAN variable: NOMFOR  
French translation: FICHIER FORTRAN

Name of FORTRAN file to be submitted.

#### FREQUENTIAL RATIO

Type: Real  
Dimension: 1  
Default value: 1.1  
FORTRAN variable: RAISF  
French translation: RAISON FREQUENTIELLE

It defines the ratio between 2 successive discretised frequencies

Associated keywords: MINIMAL FREQUENCY  
NUMBER OF FREQUENCIES  
SPECTRUM TAIL FACTOR

## GEOMETRY FILE

Type: Character  
 Dimension: 1  
 Default value: geo  
 FORTRAN variable: WAC\_FILES(WACGEO)%NAME  
 French translation: FICHIER DE GEOMETRIE

Name of the file containing the grid of the computation to be made.

Associated keywords: GEOMETRY FILE BINARY

## GEOMETRY FILE BINARY

Type: Character  
 Dimension: 1  
 Default value: 'STD'  
 FORTRAN variable: BINGEO  
 French translation: BINAIRE DU FICHIER DE GEOMETRIE

Type of the binary used for writing the geometry file. This type depends on the machine in which the file was generated. The possible values are as follows:

- IBM; for a file created in an IBM machine;
- I3E; for a file created in a HP machine;
- STD; normal READ and WRITE instructions are then generated.

Associated keywords: GEOMETRY FILE

## GEOMETRY FILE FORMAT

Type: Character  
 Dimension: 1  
 Default value: 'SERAFIN'  
 FORTRAN variable: WAC\_FILES(WACGEO)%FMT  
 French translation: FORMAT DU FICHIER DE GEOMETRIE

Geometry file format. Possible values are:

- SERAFIN: classical single precision format in Telemac;
- SERAFIND: classical double precision format in Telemac;
- MED : MED format based on HDF5'

## GLOBAL OUTPUT AT THE END

Type: LOGICAL  
 Dimension: 1  
 Default value: .FALSE.

FORTRAN variable:        GLOB  
 French translation:       SORTIE GLOBALE A LA FIN

It indicates whether a global output is made at the end of this computation (for a next computation).

Associated keywords:       GLOBAL RESULTS FILE

#### GLOBAL RESULT FILE

Type:                      Character  
 Dimension:                1  
 Default value:            ' '  
 FORTRAN variable:        WAC\_FILES(WACRBI)%NAME  
 French translation:       FICHER DES RESULTATS GLOBAUX

Name of the file in which the table F (density spectrum) is written at the end of the computation to be used in a subsequent computation

Associated keywords:       BINARY OF THE GLOBAL RESULT FILE

#### GLOBAL RESULT FILE BINARY

Type:                      Character  
 Dimension:                1  
 Default value:            'STD'  
 FORTRAN variable:        BINRBI  
 French translation:       BINAIRE DU FICHER DES RESULTATS GLOBAUX

Type of the binary used for writing the global result file. This type depends on the machine in which the file was generated. The possible values are as follows:

- IBM; for a file created in an IBM machine;
- I3E; for a file created in a HP machine;
- STD; normal READ and WRITE instructions are then generated.

Associated keywords:       GLOBAL RESULT FILE

#### IMPLICITATION COEFFICIENT FOR SOURCE TERMS

Type:                      Real  
 Dimension:                1  
 Default value:            0.5'  
 FORTRAN variable:        CIMPLI  
 French translation:       COEFFICIENT IMPLICITATION POUR TERMES SOURCES

Implication coefficient for the source terms integration, included between 0 et 1.

CIMPLI=0.: explicit

CIMPLI=0.5: semi-implicit

CIMPLI=1.: implicit

Associated keywords: CONSIDERATION OF SOURCE TERMS

#### INFINITE DEPTH

Type: LOGICAL  
 Dimension: 1  
 Default value: .FALSE.  
 FORTRAN variable: PROINF  
 French translation: PROFONDEUR INFINIE

Indicates whether an infinite depth is assumed. If so, bottom friction is inhibited.

Associated keywords: GLOBAL RESULT FILE

#### INITIAL ANGULAR DISTRIBUTION FUNCTION

Type: SPECTRE DIRECTIONNEL INITIAL  
 Dimension: 1  
 Default value: 1  
 FORTRAN variable: FRABI  
 French translation: FONCTION DE REPARTITION ANGULAIRE INITIALE

This is one of the constants used for computing the boundary directional spectrum. The following angular distribution functions are allowed:

- 1:  $\cos^2 s(T-T_0)$  ; T in range  $[T_0-\pi/2; T_0+\pi/2]$
- 2:  $\exp(-0.5((T-T_0)/s)^2)$  ; T in range  $[T_0-\pi/2; T_0+\pi/2]$
- 3:  $\cos^2 s((T-T_0)/2)$  (Mitsuyasu type)

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

#### INITIAL DIRECTIONAL SPREAD 1

Type: Real  
 Dimension: 1  
 Default value: 2.  
 FORTRAN variable: SPRED1  
 French translation: ETALEMENT DIRECTIONNEL 1 INITIAL

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

#### INITIAL DIRECTIONAL SPREAD 2

Type: Real  
 Dimension: 1

Default value: 2.  
 FORTRAN variable: SPRED2  
 French translation: ETALEMENT DIRECTIONNEL 2 INITIAL

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

#### INITIAL MAIN DIRECTION 1

Type: Real  
 Dimension: 1  
 Default value: 0.  
 FORTRAN variable: TETA1  
 French translation: DIRECTION PRINCIPALE 1 INITIALE

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

#### INITIAL MAIN DIRECTION 2

Type: Real  
 Dimension: 1  
 Default value: 0.  
 FORTRAN variable: TETA2  
 French translation: DIRECTION PRINCIPALE 2 INITIALE

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

#### INITIAL MAXIMUM PEAK FREQUENCY

Type: Real  
 Dimension: 1  
 Default value: 0.2  
 FORTRAN variable: FREMAX  
 French translation: FREQUENCE DE PIC MAXIMALE INITIALE

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

#### INITIAL MEAN FETCH VALUE

Type: Real  
Dimension: 1  
Default value: 30000.  
FORTRAN variable: FETCH  
French translation: VALEUR MOYENNE DU FETCH INITIAL

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

#### INITIAL PEAK FACTOR

Type: Real  
Dimension: 1  
Default value: 3.3  
FORTRAN variable: GAMMA  
French translation: FACTEUR DE PIC INITIAL

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

#### INITIAL PEAK FREQUENCY

Type: Real  
Dimension: 1  
Default value: 0.067  
FORTRAN variable: FPIC  
French translation: FREQUENCE DE PIC INITIALE

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

#### INITIAL PHILLIPS CONSTANT

Type: Real  
Dimension: 1  
Default value: 0.018  
FORTRAN variable: ALPHIL  
French translation: CONSTANCE DE PHILLIPS INITIALE

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

## INITIAL SIGNIFICANT WAVE HEIGHT

Type: Real  
Dimension: 1  
Default value: 1.  
FORTRAN variable: HM0  
French translation: HAUTEUR SIGNIFICATIVE INITIALE

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

## INITIAL STILL WATER LEVEL

Type: Real  
Dimension: 1  
Default value: 0.  
FORTRAN variable: ZREPOS  
French translation: COTE INITIALE DU PLAN DEAU AU REPOS

Parameter used in the computation of the initial water DEPTH: DEPTH=ZREPOS-ZF.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

## INITIAL VALUE OF SIGMA-A FOR SPECTRUM

Type: Real  
Dimension: 1  
Default value: 0.07  
FORTRAN variable: SIGMAA  
French translation: VALEUR INITIALE DE SIGMA-A POUR SPECTRE

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

## INITIAL VALUE OF SIGMA-B FOR SPECTRUM

Type: Real  
Dimension: 1  
Default value: 0.09  
FORTRAN variable: SIGMAB  
French translation: VALEUR INITIALE DE SIGMA-B POUR SPECTRE

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.



Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

#### INITIAL WEIGHTING FACTOR FOR ADF

Type: Real  
 Dimension: 1  
 Default value: 1.  
 FORTRAN variable: XLAMDA  
 French translation: FACTEUR DE PONDERATION POUR FRA INITIALE

This is one of the constants used for computing the boundary directional spectrum as a function of the wind field.

Associated keywords: TYPE OF INITIAL DIRECTIONAL SPECTRUM

#### LIMIT SPECTRUM MODIFIED BY USER

Type: LOGICAL  
 Dimension: 1  
 Default value: .FALSE.  
 FORTRAN variable: SPEULI  
 French translation: SPECTRE AUX LIMITES MODIFIE PAR LUTILISATEUR

It indicates whether the user wants to modify the boundary spectrum. It should then retrieve the limwac.f subroutine.

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

#### LIST OF FILES

Type: Character  
 Dimension: 20  
 Default value: DEFAULT1 ='STEERING FILE';  
 'DICTIONARY';  
 'FORTRAN FILE';  
 'GEOMETRY FILE';  
 'BOUNDARY CONDITIONS FILE';  
 'BOTTOM TOPOGRAPHY FILE';  
 '2D RESULTS FILE';  
 'PUNCTUAL RESULTS FILE';  
 'PREVIOUS COMPUTATION FILE';  
 'GLOBAL RESULT FILE';  
 'BINARY CURRENTS FILE';  
 'FORMATTED CURRENTS FILE';

'BINARY FILE 1';  
 'FORMATTED FILE 1';  
 'BINARY WINDS FILE';  
 'FORMATTED WINDS FILE';  
 'VALIDATION FILE';  
 'BINARY TIDAL WATER LEVEL FILE';  
 'FORMATTED TIDAL WATER LEVEL FILE'

FORTTRAN variable:

French translation: LISTE DES FICHIERS

Names of the files used by the software

Associated keywords: TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

#### MAXIMUM VALUE OF THE RATIO HM0 ON D

Type: Real

Dimension: 1

Default value: 1.

FORTTRAN variable: COEFHS

French translation: VALEUR MAXIMALE DU RAPPORT HM0 SUR D

At the beginning of the integration of the source terms, the wave height is limited in order to satisfy the specified criterion.

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION

#### MINIMAL FREQUENCY

Type: Real

Dimension: 1

Default value: 1

FORTTRAN variable: F1

French translation: FREQUENCE MINIMALE

It defines the minimal frequency in Hz. The discretised frequencies are computed from the FREQUENTIAL RATIO  $r$  and the NUMBER OF FREQUENCIES  $NF$  by the relation

$$f = f_0 * r^{(k-1)} \quad k=1, NF.$$

Associated keywords: FREQUENTIAL RATIO  
 NUMBER OF FREQUENCIES  
 SPECTRUM TAIL FACTOR

#### MINIMUM WATER DEPTH

Type: Real

Dimension: 1  
Default value: 0.1  
FORTRAN variable: PROMIN  
French translation: PROFONDEUR DEAU MINIMALE

It defines the minimum water depth below which bottom elevations are regarded as dry.

Associated keywords: FREQUENTIAL RATIO  
NUMBER OF FREQUENCIES  
SPECTRUM TAIL FACTOR

#### NEXT COMPUTATION

Type: LOGICAL  
Dimension: 1  
Default value: .FALSE.  
FORTRAN variable: SUIT  
French translation: SUITE DE CALCUL

It indicates whether a subsequent computation is to be done.

Associated keywords: PREVIOUS RESULTS FILE

#### NON-LINEAR TRANSFERTS BETWEEN FREQUENCIES

Type: INTEGER  
Dimension: 1  
Default value: 0  
FORTRAN variable: STRIF  
French translation: TRANSFERTS NON LINEAIRES INTER-FREQUENCES

Selection of the modelling type of the non-linear transfer (quadruplets) source term. If its value is 0, the non-linear transfers are ignored; if its value is 1, they are integrated in accordance with the formula of WAM cycle 4.

#### NUMBER OF BREAKING TIME STEPS

Type: INTEGER  
Dimension: 1  
Default value: 1  
FORTRAN variable: NDTBRK  
French translation: NOMBRE DE SOUS-PAS DE TEMPS POUR LE DEFERLEMENT

Number of time steps for the breaking source term. These time steps are in a geometric progression

Associated keywords: DEPTH-INDUCED BREAKING DISSIPATION  
COEFFICIENT FOR THE BREAKING TIME STEPS

## NUMBER OF DIRECTIONS

Type:	INTEGER
Dimension:	1
Default value:	12
FORTRAN variable:	NPLAN
French translation:	NOMBRE DE DIRECTIONS

It defines the number of wave propagation directions. The propagation directions are evenly distributed from 0 to 360 degrees.

## NUMBER OF FIRST ITERATION FOR GRAPHICS PRINTOUTS

Type:	INTEGER
Dimension:	1
Default value:	0
FORTRAN variable:	GRADEB
French translation:	NUMERO DE LA PREMIERE ITERATION POUR LES SORTIES GRAPHIQUES

It determines the number of iterations over the mean angular frequency from which the results are written into the 2D RESULTS FILE and the PUNCTUAL RESULTS FILE.

Associated keywords:	PERIOD FOR GRAPHIC PRINTOUTS
	VARIABLES FOR 2D GRAPHIC PRINTOUTS
	ABSCISSAE OF SPECTRUM PRINTOUT POINTS
	ORDINATES OF SPECTRUM PRINTOUT POINTS
	2D RESULTS FILE
	PUNCTUAL RESULTS FILE

## NUMBER OF FREQUENCIES

Type:	INTEGER
Dimension:	1
Default value:	15
FORTRAN variable:	NF
French translation:	NOMBRE DE FREQUENCES

It defines the number of wave propagation frequencies. The propagation frequencies are geometrically distributed as a function of the MINIMAL FREQUENCY OF THE COMPUTATION and the FREQUENTIAL RATIO

Associated keywords:	FREQUENTIAL RATIO
	SPECTRUM TAIL FACTOR

## NUMBER OF ITERATIONS FOR THE SOURCE TERMS

Type:	INTEGER
Dimension:	1
Default value:	1
FORTTRAN variable:	NSITS
French translation:	NOMBRE DE SOUS-ITERATIONS POUR LES TERMES SOURCES

Number of sub-iterations for the computation of the source terms. The time step considered in the integration of the source terms is the ratio between the TIME STEP and the NUMBER OF SUB-ITERATIONS.

Associated keywords: TIME STEP

## NUMBER OF PRIVATE ARRAYS

Type:	INTEGER
Dimension:	1
Default value:	0
FORTTRAN variable:	NPRIV
French translation:	NOMBRE DE TABLEAUX PRIVES

Number of private arrays used by the user

## NUMBER OF TIME STEP

Type:	INTEGER
Dimension:	1
Default value:	1
FORTTRAN variable:	NIT
French translation:	NOMBRE DE PAS DE TEMPS

It defines the number of time step.

Associated keywords: TIME STEP

## ORDINATES OF SPECTRUM PRINTOUT POINTS

Type:	Real
Dimension:	Variable
Default value:	0.;0.;0.;0.;0.;0.;0.;0.;0.;0.
FORTTRAN variable:	YLEO
French translation:	ORDONNEES DES POINTS DE SORTIE DU SPECTRE

Array providing the ordinates of the SERAFIN spectrum printout points with a maximum dimension of 10.

The spectrum printout points are the closest 2D points to the specified co-ordinates

Associated keywords: ABSCISSAE OF SPECTRUM PRINTOUT POINTS

## PUNCTUAL RESULT FILE

## ORIGIN COORDINATES

Type: Integer  
 Dimension: 2  
 Default value: 0.;0  
 FORTRAN variable: I\_ORIG,J\_ORIG  
 French translation: COORDONNEES DE L'ORIGINE

Value in metres, used to avoid large real numbers, added in SERAFIN format, but so far no other treatment

## PARALLEL PROCESSORS

Type: Integer  
 Dimension: 1  
 Default value: 0  
 FORTRAN variable: NCSIZE  
 French translation: PROCESSEURS PARALLELES

Number of processors for parallel processing

0: 1 machine, compiling without parallel library

1: 1 machine, compiling with a parallel library

2: 2 processors or machines in parallel

etc....'

## PERIOD FOR GRAPHIC PRINTOUTS

Type: INTEGER  
 Dimension: 1  
 Default value: 1  
 FORTRAN variable: GRAPRD  
 French translation: PERIODE POUR LES SORTIES GRAPHIQUES

It determines the printing period of graphical output.

Associated keywords: VARIABLES FOR 2D GRAPHIC PRINTOUTS  
 ABSCISSAE OF SPECTRUM PRINTOUT POINTS  
 ORDINATES OF SPECTRUM PRINTOUT POINTS  
 2D RESULTS FILE  
 PUNCTUAL RESULTS FILE  
 NUMBER OF FIRST ITERATION FOR GRAPHIC PRINTOUTS

## PERIOD FOR LISTING PRINTOUTS

Type: INTEGER  
Dimension: 1  
Default value: 1  
FORTRAN variable: LISPRD  
French translation: PERIODE POUR LES SORTIES LISTING

It determines the printing period of output to the list file.

Associated keywords: VARIABLES FOR 2D GRAPHIC PRINTOUTS  
ABSCISSAE OF SPECTRUM PRINTOUT POINTS  
ORDINATES OF SPECTRUM PRINTOUT POINTS  
2D RESULTS FILE  
PUNCTUAL RESULTS FILE  
NUMBER OF FIRST ITERATION FOR GRAPHIC PRINTOUTS

#### PREVIOUS COMPUTATION FILE

Type: Character  
Dimension: 1  
Default value: ''  
FORTRAN variable: WAC\_FILES(WACPRE)%NAME  
French translation: FICHIER DU CALCUL PRECEDENT

Name of the file containing the global results of a previous computation carried out with the same mesh.

This file gives the initial conditions for a next computation.

Associated keywords: BINARY OF THE PREVIOUS COMPUTATION FILE

#### PREVIOUS COMPUTATION FILE BINARY

Type: Character  
Dimension: 1  
Default value: 'STD'  
FORTRAN variable: BINPRE  
French translation: BINAIRE DU FICHIER DU CALCUL PRECEDENT

Type of the binary used for reading the previous computation file. This type depends on the machine in which the file was generated. The possible values are as follows:

- IBM; for a file created in an IBM machine;
- I3E; for a file created in a HP machine;
- STD; normal READ and WRITE instructions are then generated.

Associated keywords: PREVIOUS COMPUTATION FILE

#### PREVIOUS COMPUTATION FILE FORMAT

Type: Character  
 Dimension: 1  
 Default value: 'SERAFIN'  
 FORTRAN variable: WAC\_FILES(WACPRE)%FMT  
 French translation: FORMAT DU FICHIER DU CALCUL PRECEDENT

Previous computation results file format. Possible values are:

- SERAFIN: classical single precision format in Telemac;
- SERAFIND: classical double precision format in Telemac;
- MED : MED format based on HDF5'

#### PUNCTUAL RESULTS FILE

Type: Character  
 Dimension: 1  
 Default value: 'spect'  
 FORTRAN variable: WAC\_FILES(WACLEO)%NAME  
 French translation: FICHIER DES RESULTATS PONCTUELS

Name of the file to which the spectra will be written.

Associated keywords: PUNCTUAL RESULTS FILE BINARY  
 ABSCISSAE OF SPECTRUM PRINTOUT POINTS  
 ORDINATES OF SPECTRUM PRINTOUT POINTS  
 PERIOD FOR GRAPHIC PRINTOUTS  
 NUMBER OF FIRST ITERATION FOR GRAPHIC PRINTOUTS

#### PUNCTUAL RESULTS FILE BINARY

Type: Character  
 Dimension: 1  
 Default value: 'STD'  
 FORTRAN variable: BINLEO  
 French translation: BINAIRE DU FICHIER DES RESULTATS PONCTUELS

Type of the binary used for writing the spectral results file. This type depends on the machine in which the file was generated. The possible values are as follows:

- IBM; for a file created in an IBM machine;
- I3E; for a file created in a HP machine;
- STD; normal READ and WRITE instructions are then generated.

Associated keywords: PUNCTUAL RESULTS FILE

#### RANK OF THE TELEMAT DATA ITEM TO BE RECOVERED



Type: INTEGER  
 Dimension: 1  
 Default value: 0  
 FORTRAN variable: IDTEL  
 French translation: RANG DE LA DONNEE TELEMAT A RECUPERER

It indicates the rank of the TELEMAT data to be recovered in the currents file.

Associated keywords: TIME INCREMENT NUMBER IN TELEMAT FILE  
 RECOVERY OF TELEMAT DATA ITEM

#### RANK OF THE WATER LEVEL DATA IN THE TELEMAT FILE

Type: INTEGER  
 Dimension: 1  
 Default value: 4  
 FORTRAN variable: IDHMA  
 French translation: RANG DU NIVEAU DE LA MAREE DANS LE FICHIER TELEMAT

The rank of the water level data in the TELEMAT file

Associated keywords: CONSIDERATION OF TIDE  
 BINARY TIDAL WATER LEVEL FILE  
 FORMATTED TIDAL WATER LEVEL FILE  
 TIDAL WATER LEVEL FILE BINARY  
 TIDE REFRESHING PERIOD

#### RECOVERY OF TELEMAT DATA ITEM

Type: LOGICAL  
 Dimension: 1  
 Default value: .FALSE.  
 FORTRAN variable: DONTEL  
 French translation: RECUPERATION DE DONNEE TELEMAT

It indicates whether TELEMAT data are recovered in lecdon.f. If so, a proper-formatted CURRENTS FILE should be used and the rank of the respective variable should be entered into the TELEMAT file.

Associated keywords: BINARY CURRENTS FILE  
 FORMATTED CURRENTS FILE  
 CURRENTS FILE FORMAT  
 RANK OF THE TELEMAT DATA ITEM TO BE RECOVERED  
 TIME INCREMENT NUMBER IN TELEMAT FILE

#### REFERENCE FILE FORMAT

Type: Character

Dimension: 1  
 Default value: 'SERAFIN'  
 FORTRAN variable: WAC\_FILES(WACREF)%FMT  
 French translation: FORMAT DU FICHIER DE REFERENCE

Possible values are:

- SERAFIN: classical single precision format in Telemac;
- SERAFIND: classical double precision format in Telemac;
- MED : MED format based on HDF5'

#### RELEASE

Type: Character  
 Dimension: 1  
 Default value: V6P0  
 FORTRAN variable: VERS  
 French translation: NUMERO DE VERSION

Release number

#### RESULTS FILE FORMAT

Type: Character  
 Dimension: 1  
 Default value: 'SERAFIN'  
 FORTRAN variable: WAC\_FILES(WACRES)%FMT  
 French translation: FORMAT DU FICHIER DE RESULTATS

Results file format. Possible values are:

- SERAFIN: classical single precision format in Telemac;
- SERAFIND: classical double precision format in Telemac;
- MED : MED format based on HDF5'

#### SHIFT GROWING CURVE DUE TO WIND

Type: Real  
 Dimension: 1  
 Default value: 0.011  
 FORTRAN variable: DECAL  
 French translation: DECALAGE COURBE DE CROISSANCE DUE AU VENT

Constant used in the wind source term.

Associated keywords: WIND GENERATION

#### SPECTRUM FILE FORMAT

Type:	Character
Dimension:	1
Default value:	'SERAFIN'
FORTTRAN variable:	WAC_FILES(WACLEO)%FMT
French translation:	FORMAT DU FICHIER DE SPECTRE

Possible values are:

- SERAFIN: classical single precision format in Telemac;
- SERAFIND: classical double precision format in Telemac;
- MED : MED format based on HDF5'

#### SPECTRUM ENERGY THRESHOLD

Type:	Real
Dimension:	1
Default value:	1.D-30
FORTTRAN variable:	E2FMIN
French translation:	SEUIL DENERGIE CONSIDERE POUR LE SPECTRE

For initial conditions, the energy, for all frequency-direction components, lower to this threshold are set to 0.

Useful for comparisons with WAM cycle 4.

Associated keywords: WIND GENERATION

#### SPECTRUM TAIL FACTOR

Type:	Real
Dimension:	1
Default value:	5.
FORTTRAN variable:	TAILF
French translation:	FACTEUR DE QUEUE DU SPECTRE

Used to consider the contribution of the non discretised high frequencies in the computations.

Associated keywords: NUMBER OF FREQUENCIES  
FREQUENTIAL RATIO

#### SPHERICAL COORDINATES

Type:	LOGICAL
Dimension:	1
Default value:	.FALSE.
FORTTRAN variable:	SPHE
French translation:	COORDONNEES SPHERIQUES

It indicates whether the coordinates are spherical (unit= degree) or Cartesian (unit metre).

ATTENTION, in Cartesian co-ordinates, the co-ordinates are expressed in metres whereas they are

expressed in degrees in spherical co-ordinates

#### STANDARD CONFIGURATION PARAMETER

Type: Real  
 Dimension: 1  
 Default value: 0.25  
 FORTRAN variable: XLAMD  
 French translation: PARAMETRE DE LA CONFIGURATION STANDARD

Parameter defining the standard configuration for the quadruplet interactions in the DIA method.

Associated keywords: NON-LINEAR TRANSFERTS

#### STATIONNARY WIND

Type: Logical  
 Dimension: 1  
 Default value: TRUE  
 FORTRAN variable: VENSTA  
 French translation: VENT STATIONNAIRE

It indicates whether the wind evolves temporally and requires to be updated

Associated keywords: CONSIDERATION OF A WIND

#### STEERING FILE

Type: Character  
 Dimension: 1  
 Default value: 'cas'  
 FORTRAN variable: WACCAS  
 French translation: FICHIER DES PARAMETRES

Name of the file containing the parameters of the computation to be made.

#### TIDAL WATER LEVEL FILE BINARY

Type: Character  
 Dimension: 1  
 Default value: 'STD'  
 FORTRAN variable: BINMAR  
 French translation: BINAIRE DU FICHIER DU NIVEAU DE LA MAREE

Type of the binary used for writing the currents file. This type depends on the machine in which the file was generated. The possible values are as follows:

- IBM; for a file created in an IBM machine;

- I3E; for a file created in a HP machine;
- STD; normal READ and WRITE instructions are then generated.

Associated keywords:

- CONSIDERATION OF TIDE
- BINARY TIDAL WATER LEVEL FILE
- FORMATTED TIDAL WATER LEVEL FILE
- TIDAL WATER LEVEL FILE FORMAT
- TIDE REFRESHING PERIOD

#### TIDAL WATER LEVEL FILE FORMAT

Type: INTEGER  
 Dimension: 1  
 Default value: 1  
 FORTRAN variable: INDIM  
 French translation: FORMAT DU FICHIER DU NIVEAU DE LA MAREE

Selection of the type of currents file format:

- 1 finite differences, WAM cycle 4 format type
- 2 X Y UX UY, SINUSX format type
- 3 SERAFIN, TELEMAC type
- 4 user format (the maruti.f procedure should then be modified)

Associated keywords:

- CONSIDERATION OF TIDE
- BINARY TIDAL WATER LEVEL FILE
- FORMATTED TIDAL WATER LEVEL FILE
- TIDAL WATER LEVEL FILE BINARY
- TIDE REFRESHING PERIOD

#### TIDE REFRESHING PERIOD

Type: INTEGER  
 Dimension: 1  
 Default value: 1  
 FORTRAN variable: LAM  
 French translation: PERIODE D'ACTUALISATION DE LA MAREE

It determines the period in number of iterations to update the tidal currents and the water depth.

Associated keywords:

- CONSIDERATION OF TIDE
- BINARY TIDAL WATER LEVEL FILE
- FORMATTED TIDAL WATER LEVEL FILE
- TIDAL WATER LEVEL FILE BINARY
- FORMAT DU FICHIER DU NIVEAU DE LA MAREE

#### TIME INCREMENT NUMBER IN TELEMATC FILE

Type: INTEGER  
 Dimension: 1  
 Default value: 1  
 FORTRAN variable: NPTT  
 French translation: NUMERO DU PAS DE TEMPS DU FICHER TELEMATC

It indicates the number of the time step in the TELEMATC results (currents) file corresponding to the desired time for data recovery.

Associated keywords: RANK OF THE TELEMATC DATA ITEM TO BE RECOVERED  
 RECOVERY OF TELEMATC DATA ITEM

#### TIME STEP

Type: Real  
 Dimension: 1  
 Default value: 1.  
 FORTRAN variable: DT  
 French translation: PAS DE TEMPS

It defines the time step in seconds.

Associated keywords: NUMBER OF TIME STEPS

#### TITLE

Type: Character  
 Dimension: 1  
 Default value: 'SET A TITLE !!!'  
 FORTRAN variable: TITCAS  
 French translation: TITRE

Title of the case being studied.

#### TRIAD INTERACTIONS

Type: INTEGER  
 Dimension: 1  
 Default value: 0  
 FORTRAN variable: STRIA  
 French translation: TRANSFERTS ENTRE TRIPLETS DE FREQUENCES

Selection of the triad interaction model:

- 0: no triad interactions
- 1: LTA model (Eldeberky, 1996)

## 2: SPB model (Becq, 1998)

Associated keywords: TRIADS 1 (LTA) COEFFICIENT ALPHA  
 TRIADS 1 (LTA) COEFFICIENT RFMLTA  
 TRIADS 2 (SPB) COEFFICIENT K  
 TRIADS 2 (SPB) LOWER DIRECTIONAL BOUND  
 TRIADS 2 (SPB) UPPER DIRECTIONAL BOUND

## TRIADS 1 (LTA) COEFFICIENT ALPHA

Type: Real  
 Dimension: 1  
 Default value: 0.5  
 FORTRAN variable: ALFLTA  
 French translation: TRIADS 1 (LTA) CONSTANCE ALPHA

Coefficient alpha of the LTA model proposed by Eldeberky (1996). If alpha=0, no energy transfers will occur. The energy transfers increases with alpha.

Associated keywords: TRIAD INTERACTIONS  
 TRIADS 1 (LTA) COEFFICIENT RFMLTA

## TRIADS 1 (LTA) COEFFICIENT RFMLTA

Type: Real  
 Dimension: 1  
 Default value: 2.5  
 FORTRAN variable: RFMLTA  
 French translation: TRIADS 1 (LTA) CONSTANCE RFMLTA

This determines the upper frequency on which the energy transfers may occur. The maximal frequency is calculated as the product of the constant RFMLTA and the peak frequency of the spectrum.

Associated keywords: TRIAD INTERACTIONS  
 TRIADS 1 (LTA) COEFFICIENT ALPHA

## TRIADS 2 (SPB) COEFFICIENT K

Type: Real  
 Dimension: 1  
 Default value: 0.34  
 FORTRAN variable: KSPB  
 French translation: TRIADS 2 (SPB) CONSTANCE K

Coefficient K of the SPB model

Associated keywords: TRIAD INTERACTIONS

## TRIADS 2 (SPB) LOWER DIRECTIONAL BOUNDARY

## TRIADS 2 (SPB) UPPER DIRECTIONAL BOUNDARY

### TRIADS 2 (SPB) LOWER DIRECTIONAL BOUNDARY

Type: Real  
 Dimension: 1  
 Default value: 0.  
 FORTRAN variable: BDISPB  
 French translation: TRIADS 2 (SPB) BORNE DIRECTIONNELLE INFERIEURE

Lower directional boundary of the SPB model

Associated keywords: TRIAD INTERACTIONS  
 TRIADS 2 (SPB) COEFFICIENT K  
 TRIADS 2 (SPB) UPPER DIRECTIONAL BOUNDARY  
 NOM = 'TRIADS 2 (SPB) BORNE DIRECTIONNELLE INFERIEURE'

### TRIADS 2 (SPB) UPPER DIRECTIONAL BOUNDARY

Type: Real  
 Dimension: 1  
 Default value: 360.  
 FORTRAN variable: DBSSPB  
 French translation: TRIADS 2 (SPB) BORNE DIRECTIONNELLE SUPERIEURE

Upper directional boundary of the SPB model

Associated keywords: TRIAD INTERACTIONS  
 TRIADS 2 (SPB) COEFFICIENT K  
 TRIADS 2 (SPB) LOWER DIRECTIONAL BOUNDARY

### TRIGONOMETRICAL CONVENTION

Type: LOGICAL  
 Dimension: 1  
 Default value: .FALSE.  
 FORTRAN variable: TRIGO  
 French translation: CONVENTION TRIGONOMETRIQUE

True if the wave directions are measured counterclockwise from the positive x-axis, false if they are measured clockwise from geographic North

### TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

Type: INTEGER



Dimension: 1  
 Default value: 0  
 FORTRAN variable: LIMSPE  
 French translation: TYPE DE SPECTRE DIRECTIONNEL AUX LIMITES

If this keyword is set to 0, a zero valued spectrum is specified at the inlet boundaries of the domain. If it ranges from 1 to 7, a JONSWAP (or TMA) -typed spectrum is specified at these points as a function of the initial wind field and/or of the values of the following keywords

Associated keywords: BOUNDARY SIGNIFICANT HEIGHT  
 BOUNDARY PEAK FREQUENCY  
 BOUNDARY PEAK FACTOR  
 BOUNDARY VALUE OF SIGMA-A FOR SPECTRUM  
 BOUNDARY VALUE OF SIGMA-B FOR SPECTRUM  
 BOUNDARY PHILLIPS CONSTANT  
 BOUNDARY MEAN FETCH VALUE  
 BOUNDARY MAXIMUM PEAK FREQUENCY  
 BOUNDARY MAIN DIRECTION 1  
 BOUNDARY DIRECTIONAL SPREAD 1  
 BOUNDARY MAIN DIRECTION 2  
 BOUNDARY DIRECTIONAL SPREAD 2  
 BOUNDARY WEIGHTING FACTOR FOR ADF

#### TYPE OF INITIAL DIRECTIONAL SPECTRUM

Type: INTEGER  
 Dimension: 1  
 Default value: 0  
 FORTRAN variable: INISPE  
 French translation: TYPE DE SPECTRE DIRECTIONNEL INITIAL

If this keyword is set to 0, a zero valued spectrum is specified at the inlet boundaries of the domain. If it ranges from 1 to 7, a JONSWAP (or TMA)-typed spectrum is specified at these very points as a function of the initial wind field and/or of the values of the following keywords

Associated keywords: INITIAL SIGNIFICANT WAVE HEIGHT  
 INITIAL PEAK FREQUENCY  
 INITIAL PEAK FACTOR  
 INITIAL VALUE OF SIGMA-A FOR SPECTRUM  
 INITIAL VALUE OF SIGMA-B FOR SPECTRUM  
 INITIAL PHILLIPS CONSTANT  
 INITIAL MEAN FETCH VALUE  
 INITIAL MAXIMUM PEAK FREQUENCY

INITIAL MAIN DIRECTION 1  
 INITIAL DIRECTIONAL SPREAD 1  
 INITIAL MAIN DIRECTION 2  
 INITIAL DIRECTIONAL SPREAD 2  
 INITIAL WEIGHTING FACTOR FOR ADF

#### VALIDATION

Type: LOGICAL  
 Dimension: 1  
 Default value: .FALSE.  
 FORTRAN variable: VALID  
 French translation: VALIDATION

True if the computation is a validation, in which case a validation file is expected.

Associated keywords: VALIDATION FILE

#### VALIDATION FILE

Type: Character  
 Dimension: 1  
 Default value: ''  
 FORTRAN variable: WAC\_FILES(WACREF)%NAME  
 French translation: FICHER DE REFERENCE

Name of validation data file

Associated keywords: VALIDATION

#### VARIABLES FOR 2D GRAPHIC PRINTOUTS

Type: Character  
 Dimension: 1  
 Default value: HM0,DMOY  
 FORTRAN variable: SORT2D  
 French translation: VARIABLES POUR LES SORTIES GRAPHIQUES 2D

Codes of the variables the user wants to write into the 2D RESULTS FILE. The available variables are as follows:

M0: Total variance  
 HM0: Spectral significant wave height  
 DMOY: Mean wave direction  
 SPD: Mean directional spreading  
 ZF: Sea bottom level

WD: Water depth  
 UX: Current along X  
 UY: Current along Y  
 VX: Wind along X  
 VY: Wind along Y  
 FX: Driving force along X  
 FY: Driving force along Y  
 SXX: Radiation stress along xx  
 SYY: Radiation stress along yy  
 SXY: Radiation stress along xy  
 UWB: Bottom celerity  
 POW: Wave power (per meter along wave crest)  
 FMOY: Mean frequency FMOY  
 FM01: Mean frequency FM01  
 FM02: Mean frequency FM02  
 FPD: Discrete peak frequency  
 FPR5: Peak frequency by Read method of order 5  
 FPR8: Peak frequency by Read method of order 8  
 US: Surface friction velocity  $u^*$   
 CD: Surface drag coefficient CD  
 Z0: Surface roughness length Z0  
 WS: Surface wave stress  
 TMOY: Mean period Tmoy  
 TM01: Mean period Tm01  
 TM02: Mean period Tm02  
 TPD: Discrete peak period  
 TPR5: Peak period by Read method of order 5  
 TPR8: Peak period by Read method of order 8  
 PRI: Private table  
 BETA: Breaking waves coefficient

Associated keywords:     2D RESULTS FILE  
                                      NUMBER OF FIRST ITERATION FOR GRAPHIC PRINTOUTS  
                                      PERIOD FOR GRAPHIC PRINTOUTS

#### VECTOR LENGTH

Type:	INTEGER
Dimension:	1
Default value:	1

FORTTRAN variable: LVMAC

French translation: LONGUEUR DU VECTEUR

It indicates the vector length of the vector machine being used.

#### VON KARMAN CONSTANT

Type: Real

Dimension: 1

Default value: 0.41

FORTTRAN variable: XKAPPA

French translation: CONSTANCE DE VON KARMAN

Constant used in the wind source term.

Associated keywords: WIND GENERATION

#### WATER DENSITY

Type: Real

Dimension: 1

Default value: 1000.

FORTTRAN variable: ROEAU

French translation: DENSITE DE LEAU

The ratio ROAIR/ROEAU is used in the wind generation source term.

Associated keywords: WIND GENERATION

AIR DENSITY

#### WAVE GROWTH LIMITER

Type: INTEGER

Dimension: 1

Default value: 1

FORTTRAN variable: LIMIT

French translation: LIMITEUR DE CROISSANCE

Choice of the wave growth limiter.

If LIMIT=0, no wave growth limiter.

If LIMIT=1, WAM 4 original limiter.

If LIMIT=2, Hersbach et Janssen (1999) limiter.

Associated keywords: CONSIDERATION OF SOURCE TERMS

#### WHITE CAPPING DISSIPATION

Type: INTEGER

Dimension: 1

Default value: 0  
 FORTRAN variable: SMOUT  
 French translation: DISSIPATION PAR MOUTONNEMENT

Selection of the modelling type of the white capping source term. If its value is 0, the white capping dissipation is ignored; if its value is 1, it is integrated in accordance with a formula that is similar to that of WAM cycle 4.

Associated keywords: WHITE CAPPING DISSIPATION COEFFICIENT  
 WHITE CAPPING WEIGHTING COEFFICIENT

#### WHITE CAPPING DISSIPATION COEFFICIENT

Type: Real  
 Dimension: 1  
 Default value: 4.5  
 FORTRAN variable: CMOUT1  
 French translation: COEFFICIENT DE DISSIPATION PAR MOUTONNEMENT

White capping dissipation coefficient.

Associated keywords: WHITE CAPPING DISSIPATION  
 WHITE CAPPING WEIGHTING COEFFICIENT

#### WHITE CAPPING WEIGHTING COEFFICIENT

Type: Real  
 Dimension: 1  
 Default value: 0.5  
 FORTRAN variable: CMOUT2  
 French translation: COEFFICIENT DE PONDERATION POUR LE MOUTONNEMENT

White capping weighting coefficient.

Associated keywords: WHITE CAPPING DISSIPATION  
 WHITE CAPPING DISSIPATION COEFFICIENT

#### WIND DRAG COEFFICIENT

Type: Real  
 Dimension: 1  
 Default value: 1.2875E-3  
 FORTRAN variable: CDRAG  
 French translation: COEFFICIENT DE TRAINEE DE VENT

Constant used in the wind source term.

Associated keywords: WIND GENERATION

## WIND GENERATION

Type:	INTEGER
Dimension:	1
Default value:	0
FORTRAN variable:	SVENT
French translation:	APPORTS DUS AU VENT

Selection of the type of modelling of the wind generation source term. If its value is 0, the wind generation is ignored; if its value is 1, it is integrated in accordance with the WAM cycle 4 formula.

Associated keywords:	CONSIDERATION OF A WIND
	WINDS FILE FORMAT
	AIR DENSITY
	WATER DENSITY
	WIND GENERATION COEFFICIENT
	VON KARMAN CONSTANT
	CHARNOCK CONSTANT
	SHIFT GROWING CURVE DUE TO WIND
	WIND MEASUREMENTS LEVEL
	WIND DRAG COEFFICIENT

## WIND GENERATION COEFFICIENT

Type	Real
Dimension:	1
Default value:	1.2
FORTRAN variable:	BETAM
French translation:	COEFFICIENT DE GENERATION PAR LE VENT

Constant used in the wind source term.

Associated keywords:	WIND GENERATION
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## WIND MEASUREMENTS LEVEL

Type:	Real
Dimension:	1
Default value:	10.
FORTRAN variable:	ZVENT
French translation:	COTE DE MESURE DES VENTS

Constant used in the wind source term.

Associated keywords:	WIND GENERATION
----------------------	-----------------

## WIND VELOCITY ALONG X

Type: Real  
 Dimension: 1  
 Default value: 0.  
 FORTRAN variable: VX\_CTE  
 French translation: VITESSE DU VENT SUIVANT X

Wind velocity along X axis, constant and homogeneous (m/s)

Associated keywords: CONSIDERATION OF A WIND

#### WIND VELOCITY ALONG Y

Type: Real  
 Dimension: 1  
 Default value: 0.  
 FORTRAN variable: VY\_CTE  
 French translation: VITESSE DU VENT SUIVANT Y

Wind velocity along Y axis, constant and homogeneous (m/s)

Associated keywords: CONSIDERATION OF A WIND

#### WINDS FILE BINARY

Type: Character  
 Dimension: 1  
 Default value: 'STD'  
 FORTRAN variable: BINVEN  
 French translation: BINAIRE DU FICHIER DES VENTS

Type of the binary used for writing the winds file. This type depends on the machine in which the file was generated. The possible values are the same as for the geometry file.

WARNING! This file is a binary file so the keyword WINDS FILE FORMAT must be set higher than 2.

Associated keywords: BINARY WINDS FILE  
 WINDS FILE FORMAT

#### WINDS FILE FORMAT

Type: INTEGER  
 Dimension: 1  
 Default value: 1  
 FORTRAN variable: INDIV  
 French translation: FORMAT DU FICHIER DES VENTS

Selection of winds file format Type:

1 finite differences, WAM cycle 4 format type

<b>EDF R&amp;D</b>	TOMAWAC software for sea state modelling on unstructured grids over oceans and coastal seas. Release 6.0	Page 120/150
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2 X Y UX UY, SINUSX format type

3 SERAFIN, TELEMAT type

4 user format (the venuti.f procedure should then be modified)

Associated keywords: WINDS FILE BINARY



## APPENDIX 4: List of keywords classified by subject

### INPUT-OUTPUT FILES

RANK OF THE WATER LEVEL DATA IN THE TELEMATC FILE

#### BINARY SPECIFICATION

BINARY FILE 1 BINARY

GEOMETRY FILE BINARY

CURRENTS FILE BINARY

2D RESULTS FILE BINARY

GLOBAL RESULT FILE BINARY

PUNCTUAL RESULTS FILE BINARY

WINDS FILE BINARY

PREVIOUS COMPUTATION FILE BINARY

TIDAL WATER LEVEL FILE BINARY

#### FILE NAMES

BINARY FILE 1

GEOMETRY FILE

VALIDATION FILE

BOUNDARY CONDITIONS FILE

BINARY CURRENTS FILE

FORMATTED CURRENTS FILE

BOTTOM TOPOGRAPHY FILE

STEERING FILE

2D RESULTS FILE

GLOBAL RESULT FILE

PUNCTUAL RESULTS FILE

BINARY WINDS FILE

FORMATTED WINDS FILE

PREVIOUS COMPUTATION FILE

BINARY TIDAL WATER LEVEL FILE

FORMATTED TIDAL WATER LEVEL FILE

FORMATTED FILE 1

FORTTRAN FILE

### FORMATS

BINARY DATA FILE 1 FORMAT

CURRENTS FILE FORMAT

GEOMETRY FILE FORMAT

PREVIOUS COMPUTATION FILE FORMAT

REFERENCE FILE FORMAT

RESULTS FILE FORMAT

SPECTRUM FILE FORMAT

WINDS FILE FORMAT

TIDAL WATER LEVEL FILE FORMAT

### TELEMATC

TIME INCREMENT NUMBER IN TELEMATC FILE

RANK OF THE TELEMAC DATA ITEM TO BE RECOVERED

## INPUT-OUTPUT, GRAPHICS AND LISTING

### SPECTRA

ABSCISSAE OF SPECTRUM PRINTOUT POINTS

ORDINATES OF SPECTRUM PRINTOUT POINTS

### GENERAL

PERIOD FOR GRAPHIC PRINTOUTS

PERIOD FOR LISTING PRINTOUTS

NUMBER OF FIRST ITERATION FOR GRAPHICS PRINTOUTS

### GRID

VARIABLES FOR 2D GRAPHIC PRINTOUTS

## SOURCE TERMS

### WIND GENERATION

WIND GENERATION

WIND GENERATION COEFFICIENT

WIND DRAG COEFFICIENT

WIND GENERATION COEFFICIENT

CHARNOCK CONSTANT

VON KARMAN CONSTANT

WIND MEASUREMENTS LEVEL

SHIFT GROWING CURVE DUE TO WIND

STATIONARY WIND

WIND VELOCITY ALONG X

WIND VELOCITY ALONG Y

AIR DENSITY

WATER DENSITY

### WHITE-CAPPING

WHITE CAPPING DISSIPATION COEFFICIENT

WHITE CAPPING WEIGHTING COEFFICIENT

WHITE CAPPING DISSIPATION

### SEABED FRICTION

BOTTOM FRICTION COEFFICIENT

BOTTOM FRICTION DISSIPATION

### DEPTH LIMITED WAVE BREAKING

COEFFICIENT OF THE TIME SUB-INCREMENTS FOR BREAKING

DEPTH-INDUCED BREAKING 1 (BJ) CHARACTERISTIC FREQUENCY

DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT ALPHA

DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA1

DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA2

DEPTH-INDUCED BREAKING 1 (BJ) HM COMPUTATION METHOD

DEPTH-INDUCED BREAKING 1 (BJ) QB COMPUTATION METHOD

DEPTH-INDUCED BREAKING 2 (TG) CHARACTERISTIC FREQUENCY

DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT B

DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT GAMMA  
DEPTH-INDUCED BREAKING 2 (TG) WEIGHTING FUNCTION  
DEPTH-INDUCED BREAKING 3 (RO) CHARACTERISTIC FREQUENCY  
DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT ALPHA  
DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA  
DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA2  
DEPTH-INDUCED BREAKING 3 (RO) WAVE HEIGHT DISTRIBUTION  
DEPTH-INDUCED BREAKING 3 (RO) EXPONENT WEIGHTING FUNCTION  
DEPTH-INDUCED BREAKING 4 (IH) CHARACTERISTIC FREQUENCY  
DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT BETA0  
DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT M2STAR  
DEPTH-INDUCED BREAKING DISSIPATION  
NUMBER OF BREAKING TIME STEPS  
MAXIMUM VALUE OF THE RATIO HM0 ON D

#### NON-LINEAR TRANSFER

STANDARD CONFIGURATION PARAMETER  
NON-LINEAR TRANSFERTS BETWEEN FREQUENCIES

#### GENERAL

CONSIDERATION OF SOURCE TERMS  
IMPLICITATION COEFFICIENT FOR SOURCE TERMS

#### TRIAD INTERACTIONS

TRIAD INTERACTIONS  
TRIADS 1 (LTA) COEFFICIENT ALPHA  
TRIADS 1 (LTA) COEFFICIENT RFMLTA  
TRIADS 2 (SPB) LOWER DIRECTIONAL BOUNDARY  
TRIADS 2 (SPB) UPPER DIRECTIONAL BOUNDARY  
TRIADS 2 (SPB) COEFFICIENT K

#### COMPUTATION OPTIONS

TRIGONOMETRICAL CONVENTION

#### TIDE

CONSIDERATION OF TIDE

#### CURRENTS

CONSIDERATION OF A STATIONARY CURRENT  
TIDE REFRESHING PERIOD

#### SPHERICAL COORDINATES

SPHERICAL COORDINATES

#### SMOOTHING

BOTTOM SMOOTHINGS

#### PROPAGATION

CONSIDERATION OF PROPAGATION

#### WIND

CONSIDERATION OF A WIND

#### DEPTH

INFINITE DEPTH  
MINIMUM WATER DEPTH

**TELEMAC**

RECOVERY OF TELEMAC DATA ITEM

**CALCULATION CONTINUATION**

GLOBAL OUTPUT AT THE END

NEXT COMPUTATION

**VALIDATION**

VALIDATION

**BOUNDARY CONDITIONS**

BOUNDARY PHILLIPS CONSTANT

BOUNDARY MAIN DIRECTION 1

BOUNDARY MAIN DIRECTION 2

BOUNDARY DIRECTIONAL SPREAD 1

BOUNDARY DIRECTIONAL SPREAD 2

BOUNDARY PEAK FACTOR

BOUNDARY WEIGHTING FACTOR FOR ADF

BOUNDARY PEAK FREQUENCY

BOUNDARY MAXIMUM PEAK FREQUENCY

BOUNDARY SIGNIFICANT WAVE HEIGHT

TYPE OF BOUNDARY DIRECTIONAL SPECTRUM

BOUNDARY SPECTRUM VALUE OF SIGMA-A

BOUNDARY SPECTRUM VALUE OF SIGMA-B

BOUNDARY MEAN FETCH VALUE

BOUNDARY ANGULAR DISTRIBUTION FUNCTION

**INITIALISATION OF SPECTRA**

LIMIT SPECTRUM MODIFIED BY USER

SPECTRUM ENERGY THRESHOLD

INITIAL PHILLIPS CONSTANT

INITIAL MAIN DIRECTION 1

INITIAL MAIN DIRECTION 2

INITIAL DIRECTIONAL SPREAD 1

INITIAL DIRECTIONAL SPREAD 2

INITIAL PEAK FACTOR

INITIAL WEIGHTING FACTOR FOR ADF

INITIAL ANGULAR DISTRIBUTION FUNCTION

INITIAL PEAK FREQUENCY

INITIAL MAXIMUM PEAK FREQUENCY

INITIAL SIGNIFICANT WAVE HEIGHT

TYPE OF INITIAL DIRECTIONAL SPECTRUM

INITIAL VALUE OF SIGMA-A FOR SPECTRUM

INITIAL VALUE OF SIGMA-B FOR SPECTRUM

INITIAL MEAN FETCH VALUE

**GENERAL****DURATION OF CALCULATION**

DATE OF COMPUTATION BEGINNING

NUMBER OF TIME STEP

NUMBER OF ITERATIONS FOR THE SOURCE TERMS  
TIME STEP

## DISCRETISATION OF SPECTRA

SPECTRUM TAIL FACTOR  
MINIMAL FREQUENCY  
NUMBER OF DIRECTIONS  
NUMBER OF FREQUENCIES  
FREQUENTIAL RATIO

## OTHERS

NUMBER OF PRIVATE ARRAYS  
INITIAL STILL WATER LEVEL  
DESCRIPTION OF LIBRARIES  
DICTIONARY  
DEFAULT EXECUTABLE  
DEFAULT PARALLEL EXECUTABLE  
PARALLEL PROCESSORS  
LIST OF FILES  
VECTOR LENGTH

## VERSION

RELEASE

## TITLE

TITLE

## APPENDIX 5: French/English keyword dictionary

ABSCISSES DES POINTS DE SORTIE DU SPECTRE	ABSCISSAE OF SPECTRUM PRINTOUT POINTS
APPORTS DUS AU VENT	WIND GENERATION
BINAIRE DU FICHIER BINAIRE 1	BINARY FILE 1 BINARY
BINAIRE DU FICHIER DE GEOMETRIE	GEOMETRY FILE BINARY
BINAIRE DU FICHIER DES COURANTS	CURRENTS FILE BINARY
BINAIRE DU FICHIER DES RESULTATS 2D	2D RESULTS FILE BINARY
BINAIRE DU FICHIER DES RESULTATS GLOBAUX	GLOBAL RESULT FILE BINARY
BINAIRE DU FICHIER DES RESULTATS PONCTUELS	PUNCTUAL RESULTS FILE BINARY
BINAIRE DU FICHIER DES VENTS	WINDS FILE BINARY
BINAIRE DU FICHIER DU CALCUL PRECEDENT	PREVIOUS COMPUTATION FILE BINARY
BINAIRE DU FICHIER DU NIVEAU DE LA MAREE	TIDAL WATER LEVEL FILE BINARY
COEFFICIENT DE DISSIPATION PAR MOUTONNEMENT	WHITE CAPPING DISSIPATION COEFFICIENT
COEFFICIENT DE FROTTEMENT SUR LE FOND	BOTTOM FRICTION COEFFICIENT
COEFFICIENT DE GENERATION PAR LE VENT	WIND GENERATION COEFFICIENT
COEFFICIENT DE PONDERATION POUR LE MOUTONNEMENT	WHITE CAPPING WEIGHTING COEFFICIENT
COEFFICIENT DE TRAINEE DE VENT	WIND DRAG COEFFICIENT
COEFFICIENT IMPLICITATION POUR TERMES SOURCES	IMPLICITATION COEFFICIENT FOR SOURCE TERMS
COEFFICIENT POUR LES SOUS-PAS DE TEMPS POUR LE DEFERLEMENT	COEFFICIENT OF THE TIME SUB-INCREMENTS FOR BREAKING
CONSTANTE DE CHARNOCK	CHARNOCK CONSTANT
CONSTANTE DE PHILLIPS AUX LIMITES	BOUNDARY PHILLIPS CONSTANT
CONSTANTE DE PHILLIPS INITIALE	INITIAL PHILLIPS CONSTANT
CONSTANTE DE VON KARMAN	VON KARMAN CONSTANT
CONVENTION TRIGONOMETRIQUE	TRIGONOMETRICAL CONVENTION
COORDONNEES SPHERIQUES	SPHERICAL COORDINATES
COTE DE MESURE DES VENTS	WIND MEASUREMENTS LEVEL
COTE INITIALE DU PLAN DEAU AU REPOS	INITIAL STILL WATER LEVEL
DATE DE DEBUT DU CALCUL	DATE OF COMPUTATION BEGINNING
DECALAGE COURBE DE CROISSANCE DUE AU VENT	SHIFT GROWING CURVE DUE TO WIND
DEFERLEMENT 1 (BJ) CHOIX FREQUENCE CARACTERISTIQUE	DEPTH-INDUCED BREAKING 1 (BJ) CHARACTERISTIC FREQUENCY
DEFERLEMENT 1 (BJ) MODE DE CALCUL DE HM	DEPTH-INDUCED BREAKING 1 (BJ) HM COMPUTATION METHOD
DEFERLEMENT 1 (BJ) MODE DE CALCUL DE QB	DEPTH-INDUCED BREAKING 1 (BJ) QB COMPUTATION METHOD
DEFERLEMENT 1 (BJ) CONSTANTE ALPHA	DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT ALPHA
DEFERLEMENT 1 (BJ) CONSTANTE GAMMA1	DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA1
DEFERLEMENT 1 (BJ) CONSTANTE GAMMA2	DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA2
DEFERLEMENT 2 (TG) CHOIX FREQUENCE CARACTERISTIQUE	DEPTH-INDUCED BREAKING 2 (TG) CHARACTERISTIC FREQUENCY
DEFERLEMENT 2 (TG) FONCTION DE PONDERATION	DEPTH-INDUCED BREAKING 2 (TG) WEIGHTING FUNCTION
DEFERLEMENT 2 (TG) CONSTANTE B	DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT B

DEFERLEMENT 2 (TG) CONSTANCE GAMMA	DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT GAMMA
DEFERLEMENT 3 (RO) CHOIX FREQUENCE CARACTERISTIQUE	DEPTH-INDUCED BREAKING 3 (RO) CHARACTERISTIC FREQUENCY
DEFERLEMENT 3 (RO) DISTRIBUTION DES HAUTEURS DE HOULE	DEPTH-INDUCED BREAKING 3 (RO) WAVE HEIGHT DISTRIBUTION
DEFERLEMENT 3 (RO) EXPOSANT FONCTION DE PONDERATION	DEPTH-INDUCED BREAKING 3 (RO) EXPONENT WEIGHTING FUNCTION
DEFERLEMENT 3 (RO) CONSTANCE ALPHA	DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT ALPHA
DEFERLEMENT 3 (RO) CONSTANCE GAMMA	DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA
DEFERLEMENT 3 (RO) CONSTANCE GAMMA2	DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA2
DEFERLEMENT 4 (IH) CHOIX FREQUENCE CARACTERISTIQUE	DEPTH-INDUCED BREAKING 4 (IH) CHARACTERISTIC FREQUENCY
DEFERLEMENT 4 (IH) CONSTANCE BETA0	DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT BETA0
DEFERLEMENT 4 (IH) CONSTANCE M2STAR	DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT M2STAR
DESCRIPTION DES LIBRAIRIES	DESCRIPTION OF LIBRARIES
DICTIONNAIRE	DICTIONARY
DIRECTION PRINCIPALE 1 AUX LIMITES	BOUNDARY MAIN DIRECTION 1
DIRECTION PRINCIPALE 1 INITIALE	INITIAL MAIN DIRECTION 1
DIRECTION PRINCIPALE 2 AUX LIMITES	BOUNDARY MAIN DIRECTION 2
DIRECTION PRINCIPALE 2 INITIALE	INITIAL MAIN DIRECTION 2
DISSIPATION PAR DEFERLEMENT	DEPTH-INDUCED BREAKING DISSIPATION
DISSIPATION PAR FROTTEMENT SUR LE FOND	BOTTOM FRICTION DISSIPATION
DISSIPATION PAR MOUTONNEMENT	WHITE CAPPING DISSIPATION
ETALEMENT DIRECTIONNEL 1 AUX LIMITES	BOUNDARY DIRECTIONAL SPREAD 1
ETALEMENT DIRECTIONNEL 1 INITIAL	INITIAL DIRECTIONAL SPREAD 1
ETALEMENT DIRECTIONNEL 2 AUX LIMITES	BOUNDARY DIRECTIONAL SPREAD 2
ETALEMENT DIRECTIONNEL 2 INITIAL	INITIAL DIRECTIONAL SPREAD 2
EXECUTABLE PAR DEFAUT	DEFAULT EXECUTABLE
EXECUTABLE PARALLELE PAR DEFAUT	DEFAULT PARALLEL EXECUTABLE
FACTEUR DE PIC AUX LIMITES	BOUNDARY PEAK FACTOR
FACTEUR DE PIC INITIAL	INITIAL PEAK FACTOR
FACTEUR DE PONDERATION POUR FRA AUX LIMITES	BOUNDARY WEIGHTING FACTOR FOR ADF
FACTEUR DE PONDERATION POUR FRA INITIALE	INITIAL WEIGHTING FACTOR FOR ADF
FACTEUR DE QUEUE DU SPECTRE	SPECTRUM TAIL FACTOR
FICHIER BINAIRE 1	BINARY FILE 1
FICHIER DE GEOMETRIE	GEOMETRY FILE
FICHIER DE REFERENCE	VALIDATION FILE
FICHIER DES CONDITIONS AUX LIMITES	BOUNDARY CONDITIONS FILE
FICHIER DES COURANTS BINAIRE	BINARY CURRENTS FILE
FICHIER DES COURANTS FORMATE	FORMATTED CURRENTS FILE
FICHIER DES FONDS	BOTTOM TOPOGRAPHY FILE
FICHIER DES PARAMETRES	STEERING FILE
FICHIER DES RESULTATS 2D	2D RESULTS FILE
FICHIER DES RESULTATS GLOBAUX	GLOBAL RESULT FILE
FICHIER DES RESULTATS PONCTUELS	PUNCTUAL RESULTS FILE
FICHIER DES VENTS BINAIRE	BINARY WINDS FILE
FICHIER DES VENTS FORMATE	FORMATTED WINDS FILE
FICHIER DU CALCUL PRECEDENT	PREVIOUS COMPUTATION FILE

FICHER DU NIVEAU DE LA MAREE BINAIRE	BINARY TIDAL WATER LEVEL FILE
FICHER DU NIVEAU DE LA MAREE FORMATE	FORMATTED TIDAL WATER LEVEL FILE
FICHER FORMATE 1	FORMATTED FILE 1
FICHER FORTRAN	FORTRAN FILE
FONCTION DE REPARTITION ANGULAIRE AUX LIMITES	BOUNDARY ANGULAR DISTRIBUTION FUNCTION
FONCTION DE REPARTITION ANGULAIRE INITIALE	INITIAL ANGULAR DISTRIBUTION FUNCTION
FORMAT DU FICHER DE GEOMETRIE	GEOMETRY FILE FORMAT
FORMAT DU FICHER DE DONNEES BINAIRE 1	BINARY DATA FILE 1 FORMAT
FORMAT DU FICHER DE REFERENCE	REFERENCE FILE FORMAT
FORMAT DU FICHER DE RESULTATS	RESULTS FILE FORMAT
FORMAT DU FICHER DE SPECTRE	SPECTRUM FILE FORMAT
FORMAT DU FICHER DES COURANTS	CURRENTS FILE FORMAT
FORMAT DU FICHER DES VENTS	WINDS FILE FORMAT
FORMAT DU FICHER DU CALCUL PRECEDENT	PREVIOUS COMPUTATION FILE FORMAT
FORMAT DU FICHER DU NIVEAU DE LA MAREE	TIDAL WATER LEVEL FILE FORMAT
FREQUENCE DE PIC AUX LIMITES	BOUNDARY PEAK FREQUENCY
FREQUENCE DE PIC INITIALE	INITIAL PEAK FREQUENCY
FREQUENCE DE PIC MAXIMALE AUX LIMITES	BOUNDARY MAXIMUM PEAK FREQUENCY
FREQUENCE DE PIC MAXIMALE INITIALE	INITIAL MAXIMUM PEAK FREQUENCY
FREQUENCE MINIMALE	MINIMAL FREQUENCY
HAUTEUR SIGNIFICATIVE AUX LIMITES	BOUNDARY SIGNIFICANT WAVE HEIGHT
HAUTEUR SIGNIFICATIVE INITIALE	INITIAL SIGNIFICANT WAVE HEIGHT
LIMITEUR DE CROISSANCE	WAVE GROWTH LIMITER
LISSAGES DU FOND	BOTTOM SMOOTHINGS
LISTE DES FICHERS	LIST OF FILES
LONGUEUR DU VECTEUR	VECTOR LENGTH
DENSITE DE LAIR	AIR DENSITY
DENSITE DE LEAU	WATER DENSITY
NOMBRE DE DIRECTIONS	NUMBER OF DIRECTIONS
NOMBRE DE FREQUENCES	NUMBER OF FREQUENCIES
NOMBRE DE PAS DE TEMPS	NUMBER OF TIME STEP
NOMBRE DE SOUS-ITERATIONS POUR LES TERMES SOURCES	NUMBER OF ITERATIONS FOR THE SOURCE TERMS
NOMBRE DE SOUS-PAS DE TEMPS POUR LE DEFERLEMENT	NUMBER OF BREAKING TIME STEPS
NOMBRE DE TABLEAUX PRIVES	NUMBER OF PRIVATE ARRAYS
NUMERO DE LA PREMIERE ITERATION POUR LES SORTIES GRAPHIQUES	NUMBER OF FIRST ITERATION FOR GRAPHICS PRINTOUTS
NUMERO DE VERSION	RELEASE
NUMERO DU PAS DE TEMPS DU FICHER TELEMAT	TIME INCREMENT NUMBER IN TELEMAT FILE
ORDONNEES DES POINTS DE SORTIE DU SPECTRE	ORDINATES OF SPECTRUM PRINTOUT POINTS
PARAMETRE DE LA CONFIGURATION STANDARD	STANDARD CONFIGURATION PARAMETER
PAS DE TEMPS	TIME STEP
PERIODE D'ACTUALISATION DE LA MAREE	TIDE REFRESHING PERIOD
PERIODE POUR LES SORTIES GRAPHIQUES	PERIOD FOR GRAPHIC PRINTOUTS
PERIODE POUR LES SORTIES LISTING	PERIOD FOR LISTING PRINTOUTS
PRISE EN COMPTE DE LA MAREE	CONSIDERATION OF TIDE
PRISE EN COMPTE DE LA PROPAGATION	CONSIDERATION OF PROPAGATION
PRISE EN COMPTE DES TERMES SOURCES	CONSIDERATION OF SOURCE TERMS



PRISE EN COMPTE DU VENT	CONSIDERATION OF A WIND
PRISE EN COMPTE DUN COURANT STATIONNAIRE	CONSIDERATION OF A STATIONARY CURRENT
PROCESSEURS PARALLELES	PARALLEL PROCESSORS
PROFONDEUR DEAU MINIMALE	MINIMUM WATER DEPTH
PROFONDEUR INFINIE	INFINITE DEPTH
RAISON FREQUENTIELLE	FREQUENTIAL RATIO
RANG DE LA DONNEE TELEMATAC A RECUPERER	RANK OF THE TELEMATAC DATA ITEM TO BE RECOVERED
RANG DU NIVEAU DE LA MAREE DANS LE FICHIER TELEMATAC	RANK OF THE WATER LEVEL DATA IN THE TELEMATAC FILE
RECUPERATION DE DONNEE TELEMATAC	RECOVERY OF TELEMATAC DATA ITEM
SEUIL DENERGIE CONSIDERE POUR LE SPECTRE	SPECTRUM ENERGY THRESHOLD
SORTIE GLOBALE A LA FIN	GLOBAL OUTPUT AT THE END
SPECTRE AUX LIMITES MODIFIE PAR LUTILISATEUR	LIMIT SPECTRUM MODIFIED BY USER
SUITE DE CALCUL	NEXT COMPUTATION
TITRE	TITLE
TRANSFERTS ENTRE TRIPLETS DE FREQUENCES	TRIAD INTERACTIONS
TRANSFERTS NON LINEAIRES INTER-FREQUENCES	NON-LINEAR TRANSFERTS BETWEEN FREQUENCIES
TRIADS 1 (LTA) CONSTANTE ALPHA	TRIADS 1 (LTA) COEFFICIENT ALPHA
TRIADS 1 (LTA) CONSTANTE RFMLTA	TRIADS 1 (LTA) COEFFICIENT RFMLTA
TRIADS 2 (SPB) BORNE DIRECTIONNELLE INFERIEURE	TRIADS 2 (SPB) LOWER DIRECTIONAL BOUNDARY
TRIADS 2 (SPB) BORNE DIRECTIONNELLE SUPERIEURE	TRIADS 2 (SPB) UPPER DIRECTIONAL BOUNDARY
TRIADS 2 (SPB) CONSTANTE K	TRIADS 2 (SPB) COEFFICIENT K
TYPE DE SPECTRE DIRECTIONNEL AUX LIMITES	TYPE OF BOUNDARY DIRECTIONAL SPECTRUM
TYPE DE SPECTRE DIRECTIONNEL INITIAL	TYPE OF INITIAL DIRECTIONAL SPECTRUM
VALEUR AUX LIMITES DE SIGMA-A POUR SPECTRE	BOUNDARY SPECTRUM VALUE OF SIGMA-A
VALEUR AUX LIMITES DE SIGMA-B POUR SPECTRE	BOUNDARY SPECTRUM VALUE OF SIGMA-B
VALEUR INITIALE DE SIGMA-A POUR SPECTRE	INITIAL VALUE OF SIGMA-A FOR SPECTRUM
VALEUR INITIALE DE SIGMA-B POUR SPECTRE	INITIAL VALUE OF SIGMA-B FOR SPECTRUM
VALEUR MAXIMALE DU RAPPORT HM0 SUR D	MAXIMUM VALUE OF THE RATIO HM0 ON D
VALEUR MOYENNE DU FETCH AUX LIMITES	BOUNDARY MEAN FETCH VALUE
VALEUR MOYENNE DU FETCH INITIAL	INITIAL MEAN FETCH VALUE
VALIDATION	VALIDATION
VARIABLES POUR LES SORTIES GRAPHIQUES 2D	VARIABLES FOR 2D GRAPHIC PRINTOUTS
VENT STATIONNAIRE	STATIONARY WIND
VITESSE DU VENT SUIVANT X	WIND VELOCITY ALONG X
VITESSE DU VENT SUIVANT Y	WIND VELOCITY ALONG Y

## APPENDIX 6: English/French keyword dictionary

2D RESULTS FILE	FICHER DES RESULTATS 2D
2D RESULTS FILE BINARY	BINAIRE DU FICHER DES RESULTATS 2D
ABSCISSAE OF SPECTRUM PRINTOUT POINTS	ABSCISSES DES POINTS DE SORTIE DU SPECTRE
AIR DENSITY	DENSITE DE LAIR
BINARY CURRENTS FILE	FICHER DES COURANTS BINAIRE
BINARY DATA FILE 1 FORMAT	FORMAT DU FICHER DE DONNEES BINAIRE 1
BINARY FILE 1	FICHER BINAIRE 1
BINARY FILE 1 BINARY	BINAIRE DU FICHER BINAIRE 1
BINARY TIDAL WATER LEVEL FILE	FICHER DU NIVEAU DE LA MAREE BINAIRE
BINARY WINDS FILE	FICHER DES VENTS BINAIRE
BOTTOM FRICTION COEFFICIENT	COEFFICIENT DE FROTTEMENT SUR LE FOND
BOTTOM FRICTION DISSIPATION	DISSIPATION PAR FROTTEMENT SUR LE FOND
BOTTOM SMOOTHINGS	LISSAGES DU FOND
BOTTOM TOPOGRAPHY FILE	FICHER DES FONDS
BOUNDARY ANGULAR DISTRIBUTION FUNCTION	FONCTION DE REPARTITION ANGULAIRE AUX LIMITES
BOUNDARY CONDITIONS FILE	FICHER DES CONDITIONS AUX LIMITES
BOUNDARY DIRECTIONAL SPREAD 1	ETALEMENT DIRECTIONNEL 1 AUX LIMITES
BOUNDARY DIRECTIONAL SPREAD 2	ETALEMENT DIRECTIONNEL 2 AUX LIMITES
BOUNDARY MAIN DIRECTION 1	DIRECTION PRINCIPALE 1 AUX LIMITES
BOUNDARY MAIN DIRECTION 2	DIRECTION PRINCIPALE 2 AUX LIMITES
BOUNDARY MAXIMUM PEAK FREQUENCY	FREQUENCE DE PIC MAXIMALE AUX LIMITES
BOUNDARY MEAN FETCH VALUE	VALEUR MOYENNE DU FETCH AUX LIMITES
BOUNDARY PEAK FACTOR	FACTEUR DE PIC AUX LIMITES
BOUNDARY PEAK FREQUENCY	FREQUENCE DE PIC AUX LIMITES
BOUNDARY PHILLIPS CONSTANT	CONSTANTE DE PHILLIPS AUX LIMITES
BOUNDARY SIGNIFICANT WAVE HEIGHT	HAUTEUR SIGNIFICATIVE AUX LIMITES
BOUNDARY SPECTRUM VALUE OF SIGMA-A	VALEUR AUX LIMITES DE SIGMA-A POUR SPECTRE
BOUNDARY SPECTRUM VALUE OF SIGMA-B	VALEUR AUX LIMITES DE SIGMA-B POUR SPECTRE
BOUNDARY WEIGHTING FACTOR FOR ADF	FACTEUR DE PONDERATION POUR FRA AUX LIMITES
CHARNOCK CONSTANT	CONSTANTE DE CHARNOCK
COEFFICIENT OF THE TIME SUB-INCREMENTS FOR BREAKING	COEFFICIENT POUR LES SOUS-PAS DE TEMPS POUR LE DEFERLEMENT
CONSIDERATION OF A STATIONARY CURRENT	PRISE EN COMPTE DUN COURANT STATIONNAIRE
CONSIDERATION OF A WIND	PRISE EN COMPTE DU VENT
CONSIDERATION OF PROPAGATION	PRISE EN COMPTE DE LA PROPAGATION
CONSIDERATION OF SOURCE TERMS	PRISE EN COMPTE DES TERMES SOURCES
CONSIDERATION OF TIDE	PRISE EN COMPTE DE LA MAREE
CURRENTS FILE BINARY	BINAIRE DU FICHER DES COURANTS
CURRENTS FILE FORMAT	FORMAT DU FICHER DES COURANTS
DATE OF COMPUTATION BEGINNING	DATE DE DEBUT DU CALCUL
DEFAULT EXECUTABLE	EXECUTABLE PAR DEFAULT
DEFAULT PARALLEL EXECUTABLE	EXECUTABLE PARALLELE PAR DEFAULT
DEPTH-INDUCED BREAKING 1 (BJ) CHARACTERISTIC FREQUENCY	DEFERLEMENT 1 (BJ) CHOIX FREQUENCE CARACTERISTIQUE
DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT ALPHA	DEFERLEMENT 1 (BJ) CONSTANTE ALPHA

DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA1	DEFERLEMENT 1 (BJ) CONSTANTE GAMMA1
DEPTH-INDUCED BREAKING 1 (BJ) COEFFICIENT GAMMA2	DEFERLEMENT 1 (BJ) CONSTANTE GAMMA2
DEPTH-INDUCED BREAKING 1 (BJ) HM COMPUTATION METHOD	DEFERLEMENT 1 (BJ) MODE DE CALCUL DE HM
DEPTH-INDUCED BREAKING 1 (BJ) QB COMPUTATION METHOD	DEFERLEMENT 1 (BJ) MODE DE CALCUL DE QB
DEPTH-INDUCED BREAKING 2 (TG) CHARACTERISTIC FREQUENCY	DEFERLEMENT 2 (TG) CHOIX FREQUENCE CARACTERISTIQUE
DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT B	DEFERLEMENT 2 (TG) CONSTANTE B
DEPTH-INDUCED BREAKING 2 (TG) COEFFICIENT GAMMA	DEFERLEMENT 2 (TG) CONSTANTE GAMMA
DEPTH-INDUCED BREAKING 2 (TG) WEIGHTING FUNCTION	DEFERLEMENT 2 (TG) FONCTION DE PONDERATION
DEPTH-INDUCED BREAKING 3 (RO) CHARACTERISTIC FREQUENCY	DEFERLEMENT 3 (RO) CHOIX FREQUENCE CARACTERISTIQUE
DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT ALPHA	DEFERLEMENT 3 (RO) CONSTANTE ALPHA
DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA	DEFERLEMENT 3 (RO) CONSTANTE GAMMA
DEPTH-INDUCED BREAKING 3 (RO) COEFFICIENT GAMMA2	DEFERLEMENT 3 (RO) CONSTANTE GAMMA2
DEPTH-INDUCED BREAKING 3 (RO) EXPONENT WEIGHTING FUNCTION	DEFERLEMENT 3 (RO) EXPOSANT FONCTION DE PONDERATION
DEPTH-INDUCED BREAKING 3 (RO) WAVE HEIGHT DISTRIBUTION	DEFERLEMENT 3 (RO) DISTRIBUTION DES HAUTEURS DE HOULE
DEPTH-INDUCED BREAKING 4 (IH) CHARACTERISTIC FREQUENCY	DEFERLEMENT 4 (IH) CHOIX FREQUENCE CARACTERISTIQUE
DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT BETA0	DEFERLEMENT 4 (IH) CONSTANTE BETA0
DEPTH-INDUCED BREAKING 4 (IH) COEFFICIENT M2STAR	DEFERLEMENT 4 (IH) CONSTANTE M2STAR
DEPTH-INDUCED BREAKING DISSIPATION	DISSIPATION PAR DEFERLEMENT
DESCRIPTION OF LIBRARIES	DESCRIPTION DES LIBRAIRIES
DICTIONARY	DICTIONNAIRE
FORMATTED CURRENTS FILE	FICHIER DES COURANTS FORMATE
FORMATTED FILE 1	FICHIER FORMATE 1
FORMATTED TIDAL WATER LEVEL FILE	FICHIER DU NIVEAU DE LA MAREE FORMATE
FORMATTED WINDS FILE	FICHIER DES VENTS FORMATE
FORTRAN FILE	FICHIER FORTRAN
FREQUENTIAL RATIO	RAISON FREQUENTIELLE
GEOMETRY FILE	FICHIER DE GEOMETRIE
GEOMETRY FILE BINARY	BINAIRE DU FICHIER DE GEOMETRIE
GEOMETRY FILE FORMAT	FORMAT DU FICHIER DE GEOMETRIE
GLOBAL OUTPUT AT THE END	SORTIE GLOBALE A LA FIN
GLOBAL RESULT FILE	FICHIER DES RESULTATS GLOBAUX
GLOBAL RESULT FILE BINARY	BINAIRE DU FICHIER DES RESULTATS GLOBAUX
IMPLICITATION COEFFICIENT FOR SOURCE TERMS	COEFFICIENT IMPLICITATION POUR TERMES SOURCES
INFINITE DEPTH	PROFONDEUR INFINIE
INITIAL ANGULAR DISTRIBUTION FUNCTION	FONCTION DE REPARTITION ANGULAIRE INITIALE
INITIAL DIRECTIONAL SPREAD 1	ETALEMENT DIRECTIONNEL 1 INITIAL
INITIAL DIRECTIONAL SPREAD 2	ETALEMENT DIRECTIONNEL 2 INITIAL
INITIAL MAIN DIRECTION 1	DIRECTION PRINCIPALE 1 INITIALE
INITIAL MAIN DIRECTION 2	DIRECTION PRINCIPALE 2 INITIALE
INITIAL MAXIMUM PEAK FREQUENCY	FREQUENCE DE PIC MAXIMALE INITIALE

INITIAL MEAN FETCH VALUE	VALEUR MOYENNE DU FETCH INITIAL
INITIAL PEAK FACTOR	FACTEUR DE PIC INITIAL
INITIAL PEAK FREQUENCY	FREQUENCE DE PIC INITIALE
INITIAL PHILLIPS CONSTANT	CONSTANTE DE PHILLIPS INITIALE
INITIAL SIGNIFICANT WAVE HEIGHT	HAUTEUR SIGNIFICATIVE INITIALE
INITIAL STILL WATER LEVEL	COTE INITIALE DU PLAN DEAU AU REPOS
INITIAL VALUE OF SIGMA-A FOR SPECTRUM	VALEUR INITIALE DE SIGMA-A POUR SPECTRE
INITIAL VALUE OF SIGMA-B FOR SPECTRUM	VALEUR INITIALE DE SIGMA-B POUR SPECTRE
INITIAL WEIGHTING FACTOR FOR ADF	FACTEUR DE PONDERATION POUR FRA INITIALE
LIMIT SPECTRUM MODIFIED BY USER	SPECTRE AUX LIMITES MODIFIE PAR LUTILISATEUR
LIST OF FILES	LISTE DES FICHIERS
MAXIMUM VALUE OF THE RATIO HM0 ON D	VALEUR MAXIMALE DU RAPPORT HM0 SUR D
MINIMAL FREQUENCY	FREQUENCE MINIMALE
MINIMUM WATER DEPTH	PROFONDEUR DEAU MINIMALE
NEXT COMPUTATION	SUITE DE CALCUL
NON-LINEAR TRANSFERTS BETWEEN FREQUENCIES	TRANSFERTS NON LINEAIRES INTER- FREQUENCES
NUMBER OF BREAKING TIME STEPS	NOMBRE DE SOUS-PAS DE TEMPS POUR LE DEFERLEMENT
NUMBER OF DIRECTIONS	NOMBRE DE DIRECTIONS
NUMBER OF FIRST ITERATION FOR GRAPHICS PRINTOUTS	NUMERO DE LA PREMIERE ITERATION POUR LES SORTIES GRAPHIQUES
NUMBER OF FREQUENCIES	NOMBRE DE FREQUENCES
NUMBER OF ITERATIONS FOR THE SOURCE TERMS	NOMBRE DE SOUS-ITERATIONS POUR LES TERMES SOURCES
NUMBER OF PRIVATE ARRAYS	NOMBRE DE TABLEAUX PRIVES
NUMBER OF TIME STEP	NOMBRE DE PAS DE TEMPS
ORDINATES OF SPECTRUM PRINTOUT POINTS	ORDONNEES DES POINTS DE SORTIE DU SPECTRE
PARALLEL PROCESSORS	PROCESSEURS PARALLELES
PERIOD FOR GRAPHIC PRINTOUTS	PERIODE POUR LES SORTIES GRAPHIQUES
PERIOD FOR LISTING PRINTOUTS	PERIODE POUR LES SORTIES LISTING
PREVIOUS COMPUTATION FILE	FICHIER DU CALCUL PRECEDENT
PREVIOUS COMPUTATION FILE BINARY	BINAIRE DU FICHIER DU CALCUL PRECEDENT
PUNCTUAL RESULTS FILE	FICHIER DES RESULTATS PONCTUELS
PUNCTUAL RESULTS FILE BINARY	BINAIRE DU FICHIER DES RESULTATS PONCTUELS
RANK OF THE TELEMAT DATA ITEM TO BE RECOVERED	RANG DE LA DONNEE TELEMAT A RECUPERER
RANK OF THE WATER LEVEL DATA IN THE TELEMAT FILE	RANG DU NIVEAU DE LA MAREE DANS LE FICHIER TELEMAT
RECOVERY OF TELEMAT DATA ITEM	RECUPERATION DE DONNEE TELEMAT
REFERENCE FILE FORMAT	FORMAT DU FICHIER DE REFERENCE
RELEASE	NUMERO DE VERSION
SHIFT GROWING CURVE DUE TO WIND	DECALAGE COURBE DE CROISSANCE DUE AU VENT
SPECTRUM FILE FORMAT	FORMAT DU FICHIER DE SPECTRE
SPECTRUM ENERGY THRESHOLD	SEUIL DENERGIE CONSIDERE POUR LE SPECTRE
SPECTRUM TAIL FACTOR	FACTEUR DE QUEUE DU SPECTRE
SPHERICAL COORDINATES	COORDONNEES SPHERIQUES
STANDARD CONFIGURATION PARAMETER	PARAMETRE DE LA CONFIGURATION STANDARD
STATIONARY WIND	VENT STATIONNAIRE
STEERING FILE	FICHIER DES PARAMETRES
TIDAL WATER LEVEL FILE BINARY	BINAIRE DU FICHIER DU NIVEAU DE LA MAREE

<i>TIDAL WATER LEVEL FILE FORMAT</i>	<i>FORMAT DU FICHIER DU NIVEAU DE LA MAREE</i>
<i>TIDE REFRESHING PERIOD</i>	<i>PERIODE D'ACTUALISATION DE LA MAREE</i>
<i>TIME INCREMENT NUMBER IN TELEMAC FILE</i>	<i>NUMERO DU PAS DE TEMPS DU FICHIER TELEMAC</i>
<i>TIME STEP</i>	<i>PAS DE TEMPS</i>
<i>TITLE</i>	<i>TITRE</i>
<i>TRIAD INTERACTIONS</i>	<i>TRANSFERTS ENTRE TRIPLETS DE FREQUENCES</i>
<i>TRIADS 1 (LTA) COEFFICIENT ALPHA</i>	<i>TRIADS 1 (LTA) CONSTANTE ALPHA</i>
<i>TRIADS 1 (LTA) COEFFICIENT RFMLTA</i>	<i>TRIADS 1 (LTA) CONSTANTE RFMLTA</i>
<i>TRIADS 2 (SPB) COEFFICIENT K</i>	<i>TRIADS 2 (SPB) CONSTANTE K</i>
<i>TRIADS 2 (SPB) LOWER DIRECTIONAL BOUNDARY</i>	<i>TRIADS 2 (SPB) BORNE DIRECTIONNELLE INFERIEURE</i>
<i>TRIADS 2 (SPB) UPPER DIRECTIONAL BOUNDARY</i>	<i>TRIADS 2 (SPB) BORNE DIRECTIONNELLE SUPERIEURE</i>
<i>TRIGONOMETRICAL CONVENTION</i>	<i>CONVENTION TRIGONOMETRIQUE</i>
<i>TYPE OF BOUNDARY DIRECTIONAL SPECTRUM</i>	<i>TYPE DE SPECTRE DIRECTIONNEL AUX LIMITES</i>
<i>TYPE OF INITIAL DIRECTIONAL SPECTRUM</i>	<i>TYPE DE SPECTRE DIRECTIONNEL INITIAL</i>
<i>VALIDATION</i>	<i>VALIDATION</i>
<i>VALIDATION FILE</i>	<i>FICHIER DE REFERENCE</i>
<i>VARIABLES FOR 2D GRAPHIC PRINTOUTS</i>	<i>VARIABLES POUR LES SORTIES GRAPHIQUES 2D</i>
<i>VECTOR LENGTH</i>	<i>LONGUEUR DU VECTEUR</i>
<i>VON KARMAN CONSTANT</i>	<i>CONSTANTE DE VON KARMAN</i>
<i>WATER DENSITY</i>	<i>DENSITE DE LEAU</i>
<i>WAVE GROWTH LIMITER</i>	<i>LIMITEUR DE CROISSANCE</i>
<i>WHITE CAPPING DISSIPATION</i>	<i>DISSIPATION PAR MOUTONNEMENT</i>
<i>WHITE CAPPING DISSIPATION COEFFICIENT</i>	<i>COEFFICIENT DE DISSIPATION PAR MOUTONNEMENT</i>
<i>WHITE CAPPING WEIGHTING COEFFICIENT</i>	<i>COEFFICIENT DE PONDERATION POUR LE MOUTONNEMENT</i>
<i>WIND DRAG COEFFICIENT</i>	<i>COEFFICIENT DE TRAINEE DE VENT</i>
<i>WIND GENERATION</i>	<i>APPORTS DUS AU VENT</i>
<i>WIND GENERATION COEFFICIENT</i>	<i>COEFFICIENT DE GENERATION PAR LE VENT</i>
<i>WIND MEASUREMENTS LEVEL</i>	<i>COTE DE MESURE DES VENTS</i>
<i>WIND VELOCITY ALONG X</i>	<i>VITESSE DU VENT SUIVANT X</i>
<i>WIND VELOCITY ALONG Y</i>	<i>VITESSE DU VENT SUIVANT Y</i>
<i>WINDS FILE BINARY</i>	<i>BINAIRE DU FICHIER DES VENTS</i>
<i>WINDS FILE FORMAT</i>	<i>FORMAT DU FICHIER DES VENTS</i>

## APPENDIX 7: Output variables of TOMAWAC V6P0

N°	Symbol	Description of the variable	Unit	Output name
1	<b>M0</b>	Variance of the sea state $m_0$ (moment of order 0 of the wave spectrum). $m_0 = \int_0^\infty \int_0^{2\pi} F(f, \theta) df d\theta = \int_0^\infty S(f) df$	$m^2$	VARIANCE M0
2	<b>HM0</b>	Spectral significant wave height $H_{m0}$ $H_{m0} = 4\sqrt{m_0}$	m	WAVE HEIGHT HM0
3	<b>DMOY</b>	Mean wave direction $\theta_m$ with respect to the North or to the X axis depending on the adopted choice. $\theta_m = \text{Arc tan}\left(\frac{b}{a}\right) * (180/\pi)$ $a = \frac{\int_0^\infty \int_0^{2\pi} \cos(\theta) F(f, \theta) df d\theta}{m_0} \quad b = \frac{\int_0^\infty \int_0^{2\pi} \sin(\theta) F(f, \theta) df d\theta}{m_0}$	deg.	MEAN DIRECTION
4	<b>SPD</b>	Mean angular spreading $\sigma$ of the directional wave spectrum. $\sigma = \sqrt{2\left(1 - \sqrt{a^2 + b^2}\right)} * (180/\pi)$	deg.	WAVE SPREAD
5	<b>ZF</b>	Sea bottom elevation.	m	BOTTOM
6	<b>WD</b>	Water depth.	m	WATER DEPTH
7	<b>UX</b>	Component along X axis of the marine flow velocity vector (input data)	m/s	VELOCITY U
8	<b>UY</b>	Component along Y axis of the marine flow velocity vector (input data)	m/s	VELOCITY V
9	<b>VX</b>	Component along X axis of the wind velocity vector (input data)	m/s	WIND ALONG X
10	<b>VY</b>	Component along Y axis of the wind velocity vector (input data)	m/s	WIND ALONG Y
11	<b>FX</b>	Component along X axis of the radiation force due to waves.	$m/s^2$	FORCE FX
12	<b>FY</b>	Component along Y axis of the radiation force due to waves.	$m/s^2$	FORCE FY
13	<b>SXX</b>	Component Sxx of the radiation stress tensor.	$m^3/s^2$	STRESS SXX
14	<b>SXY</b>	Component Sxy of the radiation stress tensor.	$m^3/s^2$	STRESS SXY
15	<b>SYX</b>	Component Sxy of the radiation stress tensor.	$m^3/s^2$	STRESS SYX
16	<b>UWB</b>	Mean orbital wave velocity at the bottom.	m/s	BOTTOM VELOCITY
17	<b>PRI</b>	« Private » variable as chosen by the user.	(user)	PRIVATE 1

N°	Symbol	Description of the variable	Unit	Output name
18	<b>FMOY</b>	Mean wave frequency, computed from the moments of order -1 and 0 of the wave spectrum. $f_{\text{moy}} = f_{-10} = \left( \frac{m_{-1}}{m_0} \right)^{-1} = \left( \frac{\int_0^\infty \frac{S(f)}{f} df}{\int_0^\infty S(f) df} \right)^{-1}$	Hz	MEAN FREQ FMOY
19	<b>FM01</b>	Mean wave frequency, computed from the moments of order 0 and 1 of the wave spectrum. $f_{01} = \frac{m_1}{m_0} = \frac{\int_0^\infty f.S(f) df}{\int_0^\infty S(f) df}$	Hz	MEAN FREQ FM01
20	<b>FM02</b>	Mean wave frequency, computed from the moments of order 0 and 2 of the wave spectrum. $f_{02} = \sqrt{\frac{m_2}{m_0}} = \sqrt{\frac{\int_0^\infty f^2.S(f) df}{\int_0^\infty S(f) df}}$	Hz	MEAN FREQ FM02
21	<b>FPD</b>	Discrete peak frequency (among the frequencies used to discretise the spectrum).	Hz	PEAK FREQ FPD
22	<b>FPR5</b>	Peak frequency computed by the Read method of order 5. $f_{\text{pR5}} = \frac{\int_0^\infty f.S^5(f) df}{\int_0^\infty S^5(f) df}$	Hz	PEAK FREQ FPR5
23	<b>FPR8</b>	Peak frequency computed by the Read method of order 8. $f_{\text{pR8}} = \frac{\int_0^\infty f.S^8(f) df}{\int_0^\infty S^8(f) df}$	Hz	PEAK FREQ FPR8
24	<b>US</b>	Surface friction velocity $u^*$ .	m/s	USTAR
25	<b>CD</b>	Surface drag coefficient $C_D$ .	-	CD
26	<b>Z0</b>	Surface roughness length $z_0$ .	m	Z0
27	<b>WS</b>	Surface stress due to waves.	kg/(m.s <sup>2</sup> )	WAVE STRESS

N°	Symbol	Description of the variable	Unit	Output name
28	<b>TMOY</b>	Mean wave period, computed from the moments of order -1 and 0 of the wave spectrum. $T_{moy} = T_{-10} = \frac{m_{-1}}{m_0} = \frac{\int_0^{\infty} T.S(f) df}{\int_0^{\infty} S(f) df}$	s	MEAN PERIOD TMOY
29	<b>TM01</b>	Mean wave period, computed from the moments of order 0 and 1 of the wave spectrum. $T_{01} = \frac{1}{f_{01}}$	s	MEAN PERIOD TM01
30	<b>TM02</b>	Mean wave period, computed from the moments of order 0 and 2 of the wave spectrum. $T_{02} = \frac{1}{f_{02}}$	s	MEAN PERIOD TM02
31	<b>TPD</b>	Discrete peak period. $T_{pD} = \frac{1}{f_{pD}}$	s	PEAK PERIOD TPD
32	<b>TPR5</b>	Peak period computed by the Read method of order 5. $T_{pR5} = \frac{1}{f_{pR5}}$	s	PEAK PERIOD TPR5
33	<b>TPR8</b>	Peak period computed by the Read method of order 8. $T_{pR8} = \frac{1}{f_{pR8}}$	s	PEAK PERIOD TPR8
34	<b>POW</b>	Unit wave power rate (per meter of crest length).	kW/m	WAVE POWER
	<b>BETA</b>	Breaking wave coefficient	-	BETA



## APPENDIX 8: Description of the formats being used

### SERAFIN-formatted file

It is a binary file. This format is used for the *2D RESULTS FILE*, the *CURRENTS FILE FORMAT* (format 3) and the *WINDS FILE FORMAT* (format 3).

The list of records is as follows:

- a record including the study title (80 digits),
- a record including the pair of integers NBV( 1 ) and NBV( 2 ) (number of variables of linear and quadratic discretisations, NBV( 2 ) being 0),
- NBV( 1 ) + NBV( 2 ) records including (in 32 digits) each variable's name and unit,
- a record including the integers 1,0,0,0,0,0,0,0 (10 integers, only the first and the last one of which are presently used). If the last integer is equal to one, the record is followed by another record made of 6 integers indicating the date of computation beginning (year, month, day, hour, minute and second),
- a record including the integers NELEM, NPOIN, NDP, 1 (number of elements, number of points, number of points per element and the value 1),
- a record including the integer array IKLE ((NDP, NELEM)-dimensioned array), the connectivity table. WARNING: the dimensions of this array are (NELEM, NDP) in TOMAWAC),
- a record including the integer array IPOBO (NPOIN-dimensioned array). An item value is 0 for an inner point, and provides the edge point numbers for the others),
- a record including the X real array (NPOIN-dimensioned array of point abscissae),
- a record including the Y real array (NPOIN -dimensioned array of point ordinates),

The following can then be found for each time step:

- a record including time T (real),
- NBV( 1 ) + NBV( 2 ) records including the results arrays for each variable at time T.

### TOMAWAC-formatted file

It is a binary file. That format is used for the *PREVIOUS COMPUTATION FILE* and the *GLOBAL RESULT FILE*

The list of records is as follows:

- a record including the study title (80 digits).
- a record including the pair of integers NPLAN and NF corresponding respectively to the number of propagation directions and the number of frequencies.
- a record including the pair of integers NELEM2 and NPOIN2 corresponding respectively to the numbers of elements and 2D points.
- a record including end-of-computation time  $t$  (real).
- a record including the NPLAN-dimensioned real array TETA (directions of propagation, as expressed in radians).
- a record including the NF-dimensioned real array FREQ (propagation frequencies, as expressed in Hz).
- a record including the NPOIN\*NPLAN\*NF –dimensioned real area F (directional spectrum of wave action) at time  $t$ .

When a current is taken into account, then one can find:

- a record including the NPOIN–dimensioned real array UC (component of current along X) upon time  $t$ .
- a record including the NPOIN–dimensioned real array VC (component of current along Y) at time  $t$ .

When a wind is taken into account, then one can find:

- a record including the NPOIN–dimensioned real array UV (component of wind along X) at time  $t$ .
- a record including the NPOIN–dimensioned real array VV (component of wind along Y) at time  $t$ .

When the tide is taken into account, then one can find:

- a record including the NPOIN–dimensioned real array DEPTH at time  $t$ .

### **VENTS-WAM-Cycle 4-formatted file**

It is a formatted file. This format is used for the *WINDS FILE* when *WINDS FILE FORMAT* is set to 1.

The list of records is as follows:

#### **- 1- Winds grid input dimensions:**

KCOL, KROW, RLATS, RLATN, RLONL, RLONR, ICOORD, IWPER

Read with the format ( 2I4, 4F9.3, 2I2 )

KCOL: Number of longitudes in the winds grid

KROW: Number of latitudes in the winds grid

RLATS: Latitude of southern grid boundary (degrees)

RLATN: Latitude of northern grid boundary (degrees)

RLONL: Longitude of western grid boundary (degrees)

RLONR: Longitude of eastern grid boundary (degrees)

ICOORD: Code of coordinates (ICOORD=1 **mandatory**)

IWPER: Code of periodicity (IWPER=0 **mandatory**)

The latitude and longitude increments are respectively computed by:

$DPHI = (RLATN - RLATS) / (KROW - 1)$

$DLAM = (RLONR - RLONL) / (KCOL - 1)$

#### **Subsequently, for each wind field date:**

#### **- 2- Wind field date:**

IDTWIR read with format ( I10 )

WAM-formatted wind field date WAM (yyymmddhhmm)

#### **3- Horizontal (W-E) wind components at the grid points:**

ICODE read with format ( I2 )

Input field type flag

1: friction velocities

2: surface stresses

3: wind velocities at 10 m

( UWND( ILO, ILAT ), ( ILO=1, KCOL ), ILAT=1, KROW )

read with format ( 10F6.2 )

Horizontal (W-E) component value

#### **- 4- Vertical (S-N) wind components at the grid points:**

KCODE read with format ( I2 )

Input field type flag

KCODE should be equal to ICODE.

( VWND( ILO, ILAT ), ( ILO=1, KCOL ), ILAT=1, KROW )

read with format ( 10F6.2 )

Vertical (S-N) component value

The longitudes are scanned from the West eastwards and the latitudes from the South northwards

### **"finite differences" type- formatted file**

It is a formatted file. That file is possibly used for the *FORMATTED CURRENTS FILE*, the *FORMATTED WINDS FILE* or the *FORMATTED TIDAL WATER LEVEL FILE* when the option 1 is chosen for the format.

The list of records is as follows:

- a record including eight integers NCOL, NLIG, YMIN, YMAX, XMIN, XMAX, BID1 and BID. These variables respectively correspond to the number of columns, the lines of the mesh, the minimum and maximum ordinates, the minimum and maximum abscissae of the mesh, followed by 2 variables that are left unused by TOMAWAC.
- an empty record
- a record including the first component of the variable to be retrieved (for example Ux)
- a record including, if any, the second component of the variable to be retrieved (for example Uy)

### **SINUSX -formatted file**

This format is used for the *BOTTOM TOPOGRAPHY FILE* and possibly for the *CURRENTS FILE* when *CURRENTS FILE FORMAT* is set to 2.

It is a quite simple format, consisting in successive records of the X, Y, ZF type for the bottom topography file and of the X, Y, UC, VC type for the currents file.

## APPENDIX 9: File structure and processing

All files in the Serafin format may now be built in 3 different formats (given in 8 characters):

‘SERAFIN ‘: old format, understood by Rubens

‘SERAFIND’: the same in double precision, not understood by Rubens

‘MED ‘: understood by the Salomé Platform.

Consequently, for every previous Serafin file called “NAME-OF-FILE”, a key-word “NAME-OF-FILE FORMAT” has been added. In French “FORMAT DU FICHIER DE ...”.

For simplifying the implementation of this new possibility, as well as simplifying the coupling between programmes, a new file structure has been added to library BIEF. The goal is to store all the information related to a file in a single structure. The previous names of logical units and file names, such as NGE0, NRES,... and NOMGE0, NOMRES,... have been replaced by this new structure. It concerns ALL the files, not only the Serafin format. As a consequence, all the subroutines reading or writing to files have been modified.

More details are given here below.

### Structure of files

The new Fortran 90 structure for files is as follows:

```

C
C=====
=====
C
C  STRUCTURE OF FILE
C
C=====
=====
C
C      TYPE BIEF_FILE
C
C      LU: LOGICAL UNIT TO OPEN THE FILE
C      INTEGER LU
C
C      NAME: NAME OF FILE
C      CHARACTER(LEN=144) NAME
C
C      TELNAME: NAME OF FILE IN TEMPORARY DIRECTORY
C      CHARACTER(LEN=6) TELNAME
C
C      FMT: FORMAT (SERAFIN, MED, ETC.)
C      CHARACTER(LEN=8) FMT
C
C      ACTION: READ, WRITE OR READWRITE
C      CHARACTER(LEN=9) ACTION

```

```

C
C   BINASC: ASC FOR ASCII OR BIN FOR BINARY
C   CHARACTER(LEN=3) BINASC
C
C   TYPE: KIND OF FILE
C   CHARACTER(LEN=12) TYPE
C
C   END TYPE BIEF_FILE

```

### **Inputs and outputs: opening and closing files**

The various data and results files of TOMAWAC are described in its dictionary. The information relevant to files will be read with the subroutine READ\_SUBMIT, which is called in subroutine LECDON\_TOMAWAC, and stored in an array of file structures (called, WAC\_FILES). Hereafter is given an excerpt of TOMAWAC dictionary regarding the results file:

```

NOM = 'FICHER DES RESULTATS 2D'
NOM1 = '2D RESULTS FILE'
TYPE = CARACTERE
INDEX = 08
MNEMO = 'WAC_FILES(WACRES)%NAME'
SUBMIT = 'WACRES-READWRITE-08;WACRES;OBLIG;BIN;ECR;SELAFIN'
DEFAULT = ' '
DEFAULT1 = ' '

```

The character string called SUBMIT is used both by the perl scripts and, through Damocles, by the Fortran programme. It is composed of 6 character strings.

The first string, here WACRES-READWRITE-08, is made of:

- 1) the fortran integer for storing the file number: WACRES (which is declared in declarations\_telemac2d.f)
- 2) the argument ACTION in the Fortran Open statement that will be used to open the file. ACTION may be READ, WRITE, or READWRITE. Here it is READWRITE because the results file is written, and in case of validation it is read at the end of the computation. It will be stored into WAC\_FILES(WACRES) %ACTION
- 3) the logical unit to open the file. This a priori value may be changed in case of code coupling. It is stored into WAC\_FILES(WACRES) %LU

The **second** string, here WACRES, is the name of the file as it will appear in the temporary file where the computation is done.

The **third** string may be OBLIG (the name of the file must always be given), or FACUL (this file is not mandatory).

The **fourth** string (here BIN) says if it is a binary (BIN) or ASCII (ASC) file.

The **fifth** string is just like the READWRITE statement and is used by the perl scripts.

The **sixth** string is also used by the perl scripts and gives information on how the file must be treated. 'SELAFIN' means that the file is a Selafin format, it will have to be decomposed if parallelism is used. Other possibilities are:

SELAFIN-GEOM: this is the geometry file

FORTTRAN: this is the Fortran file for user subroutines

CAS: this is the parameter file

CONLIM: this is the boundary conditions file

PARAL: this file will have an extension added to its name, for distinguishing between processors

DICO: this is the dictionary

SCAL: this file will be the same for all processors

The following sequence of subroutines is used for opening, using and closing files:

Note: subroutine INIT\_FILES2 in BIEF version 5.9 has been renamed BIEF\_INIT in version 6.0 and has from now on nothing to see with files.

### 1) opening files

```
IFLOT=0
CALL
BIEF_OPEN_FILES( CODE , WAC_FILES , 44 , PATH , NCAR , COUPLAGE , IFLOT , ICODE )
```

CODE: name of calling program in 24 characters

WAC\_FILES: the array of BIEF\_FILE structures

44: the size of the previous array

PATH: full name of the path leading to the directory the case is

NCAR: number of characters of the string PATH

COUPLAGE: logical stating if there is a coupling between several programs.

IFLOT: in case of coupling, will be the last logical unit taken by a file

ICODE: code number in a coupling. For example in a coupling between Telemac-2D and Sisyphe, Telemac-2D will be code 1 and Sisyphe will be code 2.

### 2) using files:

Most operations on files consist on reading and writing, which always uses the logical unit. Every file has a name in the temporary folder where the program is executed, e.g. WACRES. The associated file number is an integer with the same name. The logical unit of this file will be equal to WACRES if there is no coupling, but more generally it is stored into WAC\_FILES(WACRES)%LU. The logical unit of the geometry file in Sisyphe will be SIS\_FILES(SISGEO)%LU.

Sometimes the real name of files in the original is also used, for example to know if it exists (= has been given in the parameter file). This name is retrieved in the component NAME. For example the name of the geometry file in Sisyphe will be SIS\_FILES(SISGEO)%NAME.

### 3) closing files:

```
CALL BIEF_CLOSE_FILES( CODE , WAC_FILES , 44 , PEXIT )
```

CODE: name of calling program in 24 characters

WAC\_FILES: the array of BIEF\_FILE structures

44: the size of the previous array

PEXIT: logical, if yes will stop parallelism (in a coupling the last program calling BIEF\_CLOSE\_FILES will also stop parallelism).



## APPENDIX 10: parallel computing in TOMAWAC

This document presents some basic concepts about the parallelism in TOMAWAC. It does not describe the parallel algorithm.

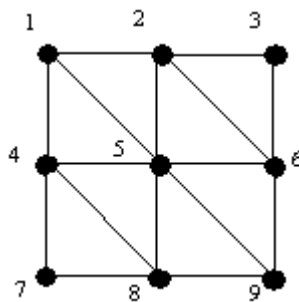
The parallelism in TOMAWAC is based on the message passing paradigm in order to run on a distributed memory architecture. The MPI library is used to manage the communication between parallel processors. Each MPI processor performs operations on its local memory independently from the other ones. The synchronisation and the data transfer between MPI processors are realized by sending or receiving messages.

Suppose that the parallel computing is performed on  $n$  MPI processus. The user has to add the following statement in the steering file:

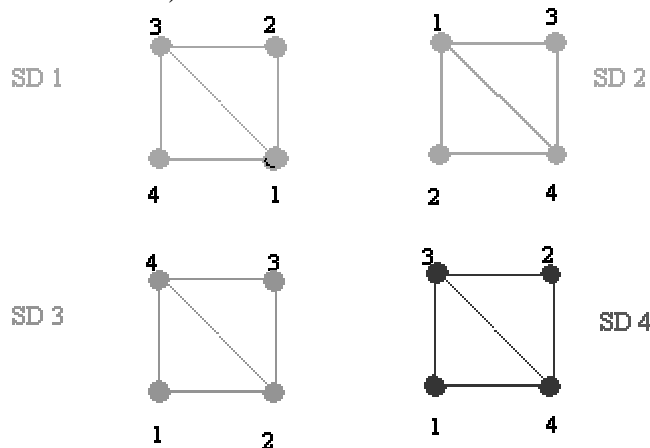
```
PARALLEL PROCESSORS = n
```

The domain (the finite element mesh) is split into  $n$  nonoverlapping subdomains. Each subdomain is assigned to a single MPI processor; in other words there is only one subdomain per MPI processor. The mesh partitioning is ensured by the PARTEL program included in the TELEMAC system. It generates the  $n$  local geometries and the boundary condition files required by the  $n$  MPI processus.

Let's consider a finite element mesh having 8 finite elements and 9 nodes



and suppose that the PARTEL program produces this following mesh partitionning (partition into 4 subdomains SD1 to SD4):



One could remark that a node does not have necessarily the same number in the global finite element mesh and in each subdomain. The node number in the global mesh is called global number whereas the node number in a subdomain is called local number.

Two arrays (knogl and knolg) are used to link the global numbering and the local numbering:

$knogl(k)=j$  indicates that the local number of the node having global number  $k$  is  $j$  ("gl" means global numbering to local numbering,  $knogl(k)=0$  indicates that the node having global number  $k$  does not belong to the subdomain);  
 $knolg(j)=k$  indicates that the global number of the node having local number  $j$  is  $k$  in the global mesh ("lg" means global numbering to local numbering) .

Note that these arrays are different among subdomains. For example, these arrays contain for subdomain SD 1:

j	1	2	3	4
knolg(j)	5	2	1	4

k	1	2	3	4	5	6	7	8	9
knogl(k)	3	2	0	4	1	0	0	0	0

and for subdomain SD 2 :

j	1	2	3	4
knolg(j)	2	5	3	6

k	1	2	3	4	5	6	7	8	9
knogl(k)	0	1	3	0	2	4	0	0	0

It is important to understand that the global numbering does not exist in parallel: the user files **need to be modified** if global node numbering is used. Suppose that in the user file there is the following instruction:

```
c The D-value is set to 0.0 for the node number 200
D(200)=0.0
```

This instruction needs to be rewritten as follows to be used both in sequential or in parallel:

```
IF (NCSIZE.GE.1) THEN
c NCSIZE is the number of MPI processus, so if NCSIZE > 1, the
c code runs in parallel
    IF (KNOGL(100) .NE. 0) THEN
c the node having global number 100 belongs to the subdomain
        D(KNOGL(100))=0.0
    END IF
ELSE
c here the code runs in sequential
    D(100)=0.0
END IF
```

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